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EXPERIMENTAL WAKE SURVEY BEHIND A 140°-INCLUDED-ANGLE CONE AT ANGLES OF ATTACK OF 0° AND 5°, MACH NUMBERS FROM 1.60 TO 3.95, AND LONGITUDINAL STATIONS VARYING FROM 1.0 TO 8.39 BODY DIAMETERS

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16. Abstract

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EXPERIMENTAL WAKE SURVEY BEHIND A 140°-INCLUDED-ANGLE CONE AT ANGLES OF ATTACK OF 0° AND 5°, MACH NUMBERS FROM 1.60 TO 3.95, AND LONGITUDINAL STATIONS VARYING FROM 1.0 TO 8.39 BODY DIAMETERS

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SUMMARY

An investigation has been conducted to obtain flow properties in the wake of a 140°-included-angle cone at Mach numbers from 1.60 to 3.95 and at angles of attack of 0° and 5°. The wake flow properties are calculated from total and static pressures measured with a pressure rake at longitudinal stations varying from 1.0 to 8.39 body diameters and at lateral stations varying from -0.42 to 3.0 body diameters. These measurements show a consistent trend throughout the range of Mach number and longitudinal distance and an increase in dynamic pressure with increasing longitudinal station.

INTRODUCTION

For problems of aerodynamic retardation, in which a drag-producing body is deployed in the wake of a forebody to reduce the speed by means of aerodynamic drag, the knowledge of the flow structure of the wake becomes an important problem. Investigations have shown that the velocity and the pressure distributions behind a body influence a secondary body placed in the wake. These flow structures are extremely difficult to predict and are generally dependent upon the shape of the leading body. Also, the effect of the flow generated by the leading body influences such parameters as the drag and the stability characteristics of the body submerged in the wake. Several investigations to define the flow field behind blunt bodies have been completed and the results can be found in references 1 to 6.

Presently an effort is underway to land an unmanned, instrumented spacecraft on the planet Mars. The thin Mars atmosphere requires the entry configuration to have a low ballistic coefficient and to utilize a parachute as the decelerator system where the parachute is partly submerged in the wake of the forebody. The drag of a decelerator system in free-stream conditions can be obtained readily in wind tunnels and in free flight; however, when a decelerator system is immersed, partially or totally, in the wake

of a forebody, the force exerted by the decelerator system differs from that measured in free stream. To help predict these forces, measurements of the flow behind the forebody have been undertaken.

An investigation has been conducted to obtain flow properties in the wake of a 140°-included-angle cone at Mach numbers from 1.60 to 3.95 and at angles of attack of 0° and 5°. The wake flow properties are calculated from total and static pressures measured with a pressure rake at longitudinal stations varying from 1.0 to 8.39 body diameters and at lateral stations varying from -0.42 to 3.0 body diameters. Free-stream Reynolds number was 5.42×10^{6} per meter (1.65×10^{6} per foot) for the tests.

Tests were run at Mach numbers from 1.60 to 3.95 on four different configurations, two 120°-included-angle cones, a 140°-included-angle cone, and the Viking '75 Entry Vehicle. Reference 5 presents the data for the two 120°-included-angle cones and reference 6 presents the data for the Viking Entry Vehicle. References 5 and 6 and the present paper are intended to make available to interested persons wake data in the form of curves and tables without analysis.

SYMBOLS

Measurements and calculations were made in the U.S. Customary Units. They are presented herein in the International System of Units (SI) with equivalent values given parenthetically in U.S. Customary Units.

D	cone base diameter, 12.192 cm (4.80 in.)
M_l	local Mach number
M_∞	free-stream Mach number
p_l	local static pressure, N/m^2 (psf)
p_∞	free-stream static pressure, N/m^2 (psf)
p_t	total pressure behind a normal shock wave, N/m^2 (psf)
$p_{t,\infty}$	free-stream total pressure, N/m^2 (psf)
q_l	local dynamic pressure, N/m^2 (psf)
q_∞	free-stream dynamic pressure, N/m^2 (psf)

R Reynolds number

T_o stagnation temperature, K (^{o}F)

V_l local velocity, m/sec (ft/sec)

V_∞ free-stream velocity, m/sec (ft/sec)

x longitudinal distance downstream from model base, cm (in.)

y lateral distance from model-rake plane, cm (in.)

z vertical distance measured in model-rake plane at zero angle of attack of model, cm (in.)

α angle of attack of model center line, deg

APPARATUS

Wind Tunnel

The tests were conducted in both the low and the high Mach number test sections of the Langley Unitary Plan wind tunnel (ref. 7). The test sections are of the variable-pressure, continuous-flow type. Each of the test sections is approximately 1.2 m (4 ft) square and 2.1 m (7 ft) long. The nozzle leading to each test section is of the asymmetric sliding-block type, which permits a continuous variation of Mach number from approximately 1.5 to 2.9 in the low Mach number test section and from approximately 2.3 to 4.7 in the high Mach number test section.

Models and Instrumentation

A sketch of the model used in the test program is shown in figure 1. The 140°-included-angle cone (fig. 1) was constructed of polished aluminum with a base diameter of 12.192 cm (4.80 in.).

The cone model was supported in the test section by a horizontal cantilevered strut (fig. 2) having a sharp leading edge and a maximum cross-sectional thickness of about 0.953 cm (0.375 in.). The use of the horizontal-cantilevered-strut support system eliminated the possibility of obtaining schlieren photographs during the tests.

A pressure rake, illustrated in figure 3, was used to perform the wake survey behind the body. The rake was 25.40 cm (10.00 in.) high and was composed of 41 total-pressure

tubes 0.635 cm (0.250 in.) apart and 21 static-pressure tubes tubes 1.270 cm (0.500 in.) apart. The rake was connected to a sting, which in turn was attached to a standard sting support system.

The pressures were recorded by using three 48-channel pressure-sampling gages. Two gages used to record total pressure had a maximum range of 57 711 N/m^2 (1080 psf) abs. The gage used to record the static pressure had a maximum range of 20 684 N/m^2 (432 psf) abs.

TESTS AND ACCURACY

The tests were performed at Mach numbers of 1.60, 2.30, 2.96, and 3.95. The Reynolds number was 5.42×10^6 per meter (1.65×10^6 per foot) for all Mach numbers tested. The stagnation dewpoint was maintained at 239 K (-30° F) in order to avoid condensation effects. The test conditions were as follows:

M_∞	T_o		$p_{t,\infty}$		q_∞	
	K	°F	N/m^2	psf	N/m^2	psf
$\alpha = 0^\circ$; $R = 5.42 \times 10^6$ per meter (1.65×10^6 per foot)						
1.60	339	150	45 184.60	943.7	19 050.12	397.87
2.30	339	150	60 621.19	1266.1	17 952.70	374.95
2.96	339	150	85 763.12	1791.2	15 206.29	317.59
3.95	353	175	152 517.77	3185.4	11 729.71	244.98
$\alpha = 5^\circ$; $R = 5.42 \times 10^6$ per meter (1.65×10^6 per foot)						
1.60	339	150	45 069.69	941.3	19 001.76	396.86
2.30	339	150	60 635.56	1266.4	17 956.53	375.03
2.96	339	150	85 878.03	1793.6	15 226.88	318.02
3.95	353	175	152 632.69	3187.8	11 738.32	245.16

The pressures in the wake of the cone were measured by means of electrically actuated pressure-scanning valves that record essentially instantaneous values. The rake was mounted vertically in the tunnel and was positioned in a longitudinal direction at various stations measured from the base of the cone. The rake was moved in a lateral direction (y-direction) at three selected longitudinal stations. At the remaining longitudinal stations, the rake was not traversed in a lateral direction (y-direction). A schematic representation of the stations, lateral and longitudinal, is presented in figure 4.

Accuracy of the pressure-scanning valves is within 1 percent of the full scale of the gage. This includes all errors of linearity, hysteresis, and repeatability. The free-

stream stagnation pressure was measured with a precision mercury manometer, the accuracy of which is ±23.94 N/m^2 (±0.50 psf).

The accuracy of the individual quantities is estimated to be within the following limits:

$p_{t,\infty}$	±526.68 N/m^2	(11.0 psf)
p	±335.16 N/m^2	(7.0 psf)
x	0.0254 cm	(0.01 in.)
y	0.0254 cm	(0.01 in.)
M_∞ at 1.60		±0.01
M_∞ at 2.30		±0.015
M_∞ at 2.96		±0.02
M_∞ at 3.95		±0.05

TABULATION OF EXPERIMENTAL DATA

Flow properties calculated from measured total and static pressures in the wake of the 140°-included-angle cone are presented in tables 1 to 8. The tabulations consist of the local flow properties for Mach number, velocity, static pressure, and dynamic pressure, each of which has been nondimensionalized by its respective free-stream value. The data are identified by the geometric information necessary to determine the longitudinal and lateral position in the flow field aft of the cone. The appropriate normal-shock expressions and isentropic-flow relations were used in conjunction with the measured total and static pressures to obtain the desired flow properties.

The pressure rake is designed with a displacement of about 1.270 cm (0.500 in.) between the total- and static-pressure tubes. In order to obtain static- and total-pressure data at identical locations, two sets of data were obtained. Total- and static-pressure data were taken at identical longitudinal and lateral positions by moving the sting to account for the offset between the total- and static-pressure tubes.

PRESENTATION OF DATA

The flow properties calculated from the measured total and static pressures in the wake of a 140°-included-angle cone are presented in figures 5 to 12 and tables 1 to 8 for Mach numbers of 1.60, 2.30, 2.96, and 3.95 and for cone angles of attack of 0° and 5°. These data consist of the local flow properties of Mach number, velocity, static pressure, and dynamic pressure that have been nondimensionalized by their respective free-stream values. The ratios are presented as a function of the vertical distance z/D measured from the model center line in the model-rake plane.

Presented in figure 5 and table 1 are plotted and tabulated flow ratios for a Mach number of 1.60, a cone angle of attack of 0°, longitudinal distances x/D varying from 1.0 to 8.39 at a lateral distance of $y/D = 0$, and for y/D varying from -0.42 to 3.0 at three values of x/D, 2.5, 5.0, and 8.39.

Figures 6, 7, and 8 and tables 2, 3, and 4 present plotted and tabulated flow ratios for Mach numbers of 2.30, 2.96, and 3.95, respectively, for the same cone angle of attack and the same combinations of x/D and y/D as figure 5 and table 1.

Figures 9, 10, 11, and 12 and tables 5, 6, 7, and 8 present plotted and tabulated flow ratios for Mach numbers of 1.60, 2.30, 2.96, and 3.95, respectively, for a cone angle of attack of 5° and x/D distances varying from 1.0 to 8.39. During these tests, no attempt was made to traverse the survey pressure rake in a lateral direction; therefore, the data presented are for cone-rake center-line locations ($y/D = 0$) at various x/D distances.

The consistent trends established by the static- and dynamic-pressure data throughout the range of Mach number and x/D result in well-defined data curves across the wake; this is particularly important in the wake-recompression region where large pressure gradients are predominant. It is believed that these consistent trends, along with the demonstrated repeatability of the data at all test conditions, make the present data a reliable information source for defining the wake structure and flow properties of the 140° cone.

Comparison of figures 5 to 8 shows that for x/D distances of 1.0 to 4.0, the center-line dynamic-pressure ratios $\left(q_l/q_\infty\right)$ are greater for the higher Mach numbers, and for x/D distances of 4.0 or greater, the center-line q_l/q_∞ ratios become greater for the lower Mach numbers tested. This trend is also evident for the 120° cone (ref. 5) and for the Viking Entry Vehicle (ref. 6). Comparing data at all Mach numbers for the various values of x/D when both y/D and x/D equal zero shows that the highest value of center-line dynamic-pressure ratio occurs when x/D is at the greatest value tested ($x/D = 8.39$). These center-line dynamic-pressure ratios vary from a maximum of 0.747 for $M_\infty = 1.60$ to 0.3946 for $M_\infty = 3.95$.

The effect of a 5° angle of attack on the 140° cone can be seen in figures 9 to 12. Comparison of figures 9 to 12 when $\alpha = 5^{\circ}$ with figures 5 to 8 when $\alpha = 0^{\circ}$ shows that, at the higher angle of attack, an unsymmetrical wake is produced and that the effect of the unsymmetrical wake appears to decrease when the survey rake is moved downstream.

Comparison of the wake data for all Mach numbers, x/D distances, and angles of attack for the 140° cone with the same type data for the 120° cone (ref. 5) indicates that the 120° cone has slightly lower dynamic pressures than the 140° cone. Comparison of the same type data for the 140° cone and the Viking Entry Vehicle (ref. 6) indicates almost no difference in dynamic pressures between the two configurations. The rake

used during the investigation covered a z/D distance of ± 1.04 body diameters from the wake (or body) center line. As would be expected, the closer the survey rake is to the base of the body the larger the variation in pressure that is noted for all Mach numbers. For all Mach numbers and all x/D distances tested, the dynamic-pressure ratio q_l/q_∞ approaches free-stream conditions at the outer edges of the wake. However, some pressure loss is shown in that free-stream conditions are not quite obtained within the distance covered by the rake. The exception to this is when the survey rake is placed at a large y/D distance and then the rake measures the free-stream conditions of the tunnel.

CONCLUDING REMARKS

An investigation has been conducted to obtain flow properties in the wake of a 140°-included-angle cone at Mach numbers from 1.60 to 3.95 and at angles of attack of 0° and 5°. The wake flow properties are calculated from total and static pressures measured with a pressure rake at longitudinal stations varying from 1.0 to 8.39 body diameters and at lateral stations varying from -0.42 to 3.0 body diameters. These measurements show a consistent trend throughout the range of Mach number and x/D distance and an increase in dynamic pressure with increasing longitudinal station.

Changing the cone angle from 120° (ref. 5) to 140° has only a slight effect on velocity, Mach number, static-pressure, and dynamic-pressure ratios. The 120° cone has slightly lower dynamic pressures than the 140° cone throughout the test Mach number range.

Langley Research Center,
National Aeronautics and Space Administration,
Hampton, Va., September 29, 1971.

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TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER)

(a) x/D = 1.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 221.93 psf (10626.13 N/m^2);
q_∞ = 397.70 psf (19042.02 N/m^2);
$p_{t,\infty}$ = 943.30 psf (45165.45 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7425	.8997	1.1008	1.0634
.988	.7272	.9006	1.1128	1.0705
.936	.7120	.8815	1.1127	1.0704
.884	.6902	.8784	1.1281	1.0794
.832	.6684	.8687	1.1400	1.0862
.780	.6565	.8474	1.1361	1.0840
.728	.6445	.8377	1.1401	1.0863
.676	.6107	.8315	1.1668	1.1014
.624	.5770	.6556	1.0659	1.0422
.572	.5683	.2065	.6028	.6806
.520	.5596	.0569	.3190	.3824
.468	.5563	.0167	.1735	.2117
.416	.5530	.0097	.1323	.1620
.364	.5498	.0085	.1244	.1523
.312	.5465	.0073	.1157	.1418
.260	.5476	.0067	.1107	.1357
.208	.5487	.0031	.0754	.0925
.156	.5520	.0013	.0486	.0597
.104	.5530	.0007	.0355	.0437
.052	.5520	0.0000	0.0000	0.0000
0.000	.5574	0.0000	0.0000	0.0000
-.052	.5563	.0079	.1192	.1460
-.104	.5552	.0085	.1237	.1515
-.156	.5509	.0138	.1584	.1935
-.208	.5465	.0162	.1720	.2099
-.260	.5465	.0162	.1720	.2099
-.312	.5465	.0162	.1720	.2099
-.364	.5465	.0162	.1720	.2099
-.416	.5465	.0191	.1868	.2277
-.468	.5541	.0237	.2068	.2515
-.520	.5618	.0505	.2998	.3604
-.572	.5694	.2370	.6451	.7202
-.624	.5770	.6689	1.0767	1.0488
-.676	.6009	.8348	1.1786	1.1079
-.728	.6249	.8525	1.1680	1.1020
-.780	.6521	.8481	1.1404	1.0865
-.832	.6793	.8636	1.1275	1.0790
-.884	.6968	.8723	1.1189	1.0740
-.936	.7142	.8828	1.1118	1.0699
-.988	.7349	.8927	1.1022	1.0641
-1.040	.7555	.9009	1.0920	1.0580

(b) x/D = 1.5; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 222.07 psf (10632.89 N/m^2);
q_∞ = 397.95 psf (19054.13 N/m^2);
$p_{t,\infty}$ = 943.90 psf (45194.18 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9498	.9447	.9973	.9982
.988	.9368	.9302	.9965	.9977
.936	.9238	.9174	.9965	.9977
.884	.8759	.9155	1.0224	1.0146
.832	.8281	.9103	1.0484	1.0313
.780	.7814	.8948	1.0701	1.0447
.728	.7347	.8942	1.1033	1.0648
.676	.7021	.8813	1.1204	1.0749
.624	.6694	.8600	1.1334	1.0825
.572	.6379	.7150	1.0587	1.0377
.520	.6064	.4118	.8240	.8728
.468	.6064	.1846	.5518	.6311
.416	.6064	.0614	.3183	.3816
.364	.6064	.0166	.1657	.2023
.312	.6064	.0018	.0538	.0661
.260	.6097	0.0000	0.0000	0.0000
.208	.6129	0.0000	0.0000	0.0000
.156	.6173	0.0000	0.0000	0.0000
.104	.6205	0.0000	0.0000	0.0000
.052	.6162	0.0000	0.0000	0.0000
0.000	.6282	0.0000	0.0000	0.0000
-.052	.6238	0.0000	0.0000	0.0000
-.104	.6195	0.0000	0.0000	0.0000
-.156	.6129	0.0000	0.0000	0.0000
-.208	.6064	0.0000	0.0000	0.0000
-.260	.6053	0.0000	0.0000	0.0000
-.312	.6042	.0086	.1191	.1460
-.364	.6075	.0157	.1606	.1962
-.416	.6108	.0748	.3500	.4175
-.468	.6151	.1959	.5644	.6435
-.520	.6195	.4258	.8290	.8768
-.572	.6477	.7709	1.0909	1.0574
-.624	.6760	.8662	1.1320	1.0816
-.676	.7303	.8772	1.0959	1.0604
-.728	.7846	.8864	1.0629	1.0403
-.780	.8281	.8974	1.0410	1.0266
-.832	.8716	.9067	1.0200	1.0131
-.884	.8738	.9164	1.0241	1.0157
-.936	.8759	.9344	1.0329	1.0214
-.988	.8303	.9505	1.0700	1.0447
-1.040	.7846	.9631	1.1079	1.0676

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(c) x/D = 2.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 221.98 psf (10628.38 N/m^2);
q_∞ = 397.79 psf (19046.06 N/m^2);
$p_{t,\infty}$ = 943.50 psf (45175.02 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7467	.9055	1.1012	1.0636
.988	.7325	.9079	1.1133	1.0707
.936	.7184	.8935	1.1153	1.0719
.884	.6999	.8849	1.1244	1.0772
.832	.6814	.8913	1.1437	1.0883
.780	.6955	.8789	1.1241	1.0771
.728	.7097	.8799	1.1135	1.0709
.676	.7238	.8842	1.1053	1.0660
.624	.7380	.8903	1.0983	1.0619
.572	.7499	.8883	1.0883	1.0558
.520	.7619	.8394	1.0496	1.0320
.468	.7630	.6253	.9053	.9343
.416	.7641	.3263	.6534	.7279
.364	.7652	.1754	.4788	.5569
.312	.7663	.0809	.3248	.3891
.260	.7695	.0349	.2131	.2590
.208	.7728	.0037	.0694	.0852
.156	.7739	0.0000	0.0000	0.0000
.104	.7771	0.0000	0.0000	0.0000
.052	.7706	0.0000	0.0000	0.0000
0.000	.7815	0.0000	0.0000	0.0000
-.052	.7750	0.0000	0.0000	0.0000
-.104	.7684	0.0000	0.0000	0.0000
-.156	.7663	.0064	.0912	.1119
-.208	.7641	.0194	.1595	.1949
-.260	.7576	.0374	.2221	.2698
-.312	.7510	.0872	.3406	.4070
-.364	.7586	.1488	.4429	.5192
-.416	.7663	.3649	.6901	.7608
-.468	.7597	.6360	.9149	.9413
-.520	.7532	.8454	1.0594	1.0381
-.572	.7347	.8835	1.0966	1.0608
-.624	.7162	.8916	1.1158	1.0722
-.676	.7086	.8862	1.1183	1.0737
-.728	.7010	.8841	1.1231	1.0765
-.780	.7053	.8767	1.1149	1.0717
-.832	.7097	.8843	1.1163	1.0725
-.884	.7195	.8861	1.1098	1.0686
-.936	.7293	.8994	1.1106	1.0691
-.988	.7532	.9021	1.0944	1.0595
-1.040	.7771	.9015	1.0770	1.0490

(d) x/D = 2.5; y/D = 3.0; $\alpha = 0^\circ$;

p_∞ = 221.06 psf (10584.45 N/m^2);
q_∞ = 396.14 psf (18967.33 N/m^2);
$p_{t,\infty}$ = 939.60 psf (44988.29 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1019	1.0134	.9590	.9723
.988	1.1083	1.0106	.9549	.9695
.936	1.1148	1.0111	.9524	.9677
.884	1.1094	1.0087	.9535	.9685
.832	1.1040	1.0080	.9555	.9699
.780	1.0889	1.0191	.9674	.9781
.728	1.0737	1.0201	.9747	.9831
.676	1.0748	1.0098	.9693	.9794
.624	1.0759	1.0147	.9711	.9806
.572	1.0770	1.0145	.9706	.9802
.520	1.0780	1.0093	.9676	.9782
.468	1.0824	1.0119	.9669	.9777
.416	1.0867	1.0111	.9646	.9762
.364	1.0824	1.0152	.9685	.9788
.312	1.0780	1.0093	.9676	.9782
.260	1.0715	1.0154	.9735	.9822
.208	1.0651	1.0082	.9729	.9819
.156	1.0845	1.0131	.9665	.9775
.104	1.0780	1.0126	.9692	.9793
.052	1.0824	1.0119	.9669	.9777
0.000	1.0910	1.0003	.9575	.9713
-.052	1.0954	1.0052	.9580	.9716
-.104	1.0997	.9961	.9517	.9673
-.156	1.0986	1.0063	.9571	.9710
-.208	1.0975	.9998	.9545	.9692
-.260	1.0975	1.0099	.9592	.9725
-.312	1.0975	1.0065	.9576	.9714
-.364	1.1040	1.0137	.9582	.9718
-.416	1.1105	1.0059	.9517	.9673
-.468	1.1094	1.0161	.9570	.9709
-.520	1.1083	1.0096	.9544	.9691
-.572	1.1138	1.0137	.9540	.9689
-.624	1.1192	1.0027	.9465	.9637
-.676	1.1170	1.0064	.9492	.9655
-.728	1.1148	1.0051	.9495	.9657
-.780	1.1235	1.0069	.9467	.9638
-.832	1.1322	1.0054	.9423	.9607
-.884	1.1322	1.0054	.9423	.9607
-.936	1.1322	1.0104	.9447	.9624
-.988	1.1311	1.0072	.9437	.9617
-1.040	1.1300	1.0074	.9442	.9620

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(e) x/D = 2.5; y/D = 2.0; $\alpha = 0^o$;

p_∞ = 221.13 psf (10587.83 N/m^2);
q_∞ = 396.27 psf (18973.39 N/m^2);
$p_{t,\infty}$ = 939.90 psf (45002.65 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8762	.9771	1.0560	1.0360
.988	.8806	.9863	1.0583	1.0375
.936	.8849	.9706	1.0473	1.0305
.884	.8773	.9752	1.0543	1.0349
.832	.8697	.9732	1.0578	1.0371
.780	.8697	.9582	1.0496	1.0320
.728	.8697	.9582	1.0496	1.0320
.676	.8546	.9591	1.0594	1.0381
.624	.8395	.9683	1.0740	1.0471
.572	.8416	.9563	1.0659	1.0422
.520	.8438	.9609	1.0672	1.0429
.468	.8470	.9537	1.0611	1.0392
.416	.8503	.9598	1.0625	1.0400
.364	.8427	.9544	1.0642	1.0411
.312	.8351	.9541	1.0688	1.0440
.260	.8330	.9544	1.0704	1.0449
.208	.8308	.9548	1.0720	1.0459
.156	.8308	.9548	1.0720	1.0459
.104	.8286	.9551	1.0736	1.0469
.052	.8297	.9550	1.0728	1.0464
0.000	.8265	.9655	1.0808	1.0513
-.052	.8276	.9491	1.0709	1.0453
-.104	.8286	.9589	1.0757	1.0482
-.156	.8308	.9486	1.0685	1.0438
-.208	.8330	.9515	1.0688	1.0439
-.260	.8297	.9521	1.0712	1.0454
-.312	.8265	.9526	1.0736	1.0469
-.364	.8330	.9515	1.0688	1.0439
-.416	.8395	.9521	1.0650	1.0416
-.468	.8416	.9534	1.0643	1.0412
-.520	.8438	.9547	1.0637	1.0408
-.572	.8524	.9549	1.0584	1.0375
-.624	.8611	.9684	1.0605	1.0388
-.676	.8676	.9573	1.0504	1.0325
-.728	.8741	.9679	1.0523	1.0337
-.780	.8784	.9588	1.0448	1.0289
-.832	.8827	.9697	1.0481	1.0311
-.884	.8881	.9771	1.0489	1.0316
-.936	.8935	.9712	1.0426	1.0275
-.988	.8990	.9770	1.0425	1.0275
-1.040	.9044	.9760	1.0389	1.0252

(f) x/D = 2.5; y/D = 1.5; $\alpha = 0^o$;

p_∞ = 221.13 psf (10587.83 N/m^2);
q_∞ = 396.27 psf (18973.39 N/m^2);
$p_{t,\infty}$ = 939.90 psf (45002.65 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7897	.9516	1.0977	1.0615
.988	.7940	.9409	1.0886	1.0560
.936	.7984	.9501	1.0909	1.0574
.884	.7929	.9361	1.0865	1.0548
.832	.7875	.9353	1.0898	1.0567
.780	.7929	.9294	1.0827	1.0524
.728	.7984	.9269	1.0775	1.0493
.676	.7800	.9283	1.0909	1.0574
.624	.7616	.9280	1.1039	1.0652
.572	.7594	.9267	1.1047	1.0656
.520	.7572	.9254	1.1055	1.0661
.468	.7637	.9243	1.1001	1.0629
.416	.7702	.9216	1.0939	1.0592
.364	.7594	.9234	1.1027	1.0645
.312	.7486	.9235	1.1107	1.0692
.260	.7443	.9226	1.1134	1.0708
.208	.7399	.9233	1.1171	1.0729
.156	.7453	.9208	1.1115	1.0697
.104	.7410	.9215	1.1151	1.0718
.052	.7389	.9218	1.1170	1.0729
0.000	.7421	.9229	1.1152	1.0719
-.052	.7399	.9188	1.1144	1.0714
-.104	.7378	.9192	1.1162	1.0724
-.156	.7378	.9192	1.1162	1.0724
-.208	.7378	.9208	1.1172	1.0730
-.260	.7389	.9207	1.1163	1.0725
-.312	.7399	.9205	1.1154	1.0719
-.364	.7432	.9200	1.1126	1.0703
-.416	.7464	.9211	1.1108	1.0693
-.468	.7529	.9200	1.1054	1.0661
-.520	.7594	.9222	1.1020	1.0641
-.572	.7627	.9217	1.0993	1.0625
-.624	.7659	.9245	1.0987	1.0621
-.676	.7702	.9254	1.0961	1.0605
-.728	.7746	.9264	1.0936	1.0590
-.780	.7789	.9273	1.0911	1.0575
-.832	.7832	.9266	1.0877	1.0555
-.884	.7875	.9308	1.0872	1.0552
-.936	.7919	.9351	1.0867	1.0549
-.988	.7984	.9340	1.0816	1.0518
-1.040	.8048	.9512	1.0871	1.0551

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(g) $x/D = 2.5$; $y/D = 1.0$; $\alpha = 0^\circ$;

p_∞ = 221.13 psf (10587.83 N/m^2);
q_∞ = 396.27 psf (18973.39 N/m^2);
$p_{t,\infty}$ = 939.90 psf (45002.65 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7321	.9224	1.1225	1.0761
.988	.7332	.9123	1.1155	1.0720
.936	.7343	.9121	1.1146	1.0715
.884	.7321	.9058	1.1123	1.0702
.832	.7299	.9045	1.1132	1.0707
.780	.7364	.8985	1.1045	1.0656
.728	.7429	.8974	1.0990	1.0623
.676	.7267	.8968	1.1109	1.0693
.624	.7104	.8994	1.1252	1.0777
.572	.7104	.8978	1.1241	1.0771
.520	.7104	.8994	1.1252	1.0777
.468	.7256	.8969	1.1118	1.0699
.416	.7408	.8977	1.1009	1.0634
.364	.7418	.9009	1.1020	1.0640
.312	.7429	.9040	1.1031	1.0647
.260	.7462	.9052	1.1014	1.0637
.208	.7494	.9079	1.1007	1.0633
.156	.7462	.9068	1.1024	1.0643
.104	.7494	.9096	1.1017	1.0639
.052	.7451	.9120	1.1063	1.0666
0.000	.7494	.9129	1.1037	1.0651
-.052	.7451	.9064	1.1029	1.0646
-.104	.7408	.9071	1.1066	1.0668
-.156	.7343	.9048	1.1101	1.0689
-.208	.7278	.9043	1.1147	1.0716
-.260	.7202	.9022	1.1193	1.0742
-.312	.7126	.8985	1.1229	1.0763
-.364	.7029	.8968	1.1296	1.0802
-.416	.6931	.8967	1.1374	1.0848
-.468	.7007	.8922	1.1284	1.0795
-.520	.7083	.8909	1.1216	1.0756
-.572	.7018	.8920	1.1274	1.0790
-.624	.6953	.8947	1.1344	1.0830
-.676	.6996	.8940	1.1304	1.0807
-.728	.7039	.8999	1.1307	1.0809
-.780	.7104	.8988	1.1248	1.0775
-.832	.7169	.9011	1.1211	1.0753
-.884	.7180	.9042	1.1222	1.0760
-.936	.7191	.9057	1.1223	1.0760
-.988	.7256	.9096	1.1196	1.0745
-1.040	.7321	.9118	1.1160	1.0723

(h) $x/D = 2.5$; $y/D = 0.83$; $\alpha = 0^\circ$;

p_∞ = 221.13 psf (10587.83 N/m^2);
q_∞ = 396.27 psf (18973.39 N/m^2);
$p_{t,\infty}$ = 939.90 psf (45002.65 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7183	.9141	1.1281	1.0794
.988	.7205	.9055	1.1211	1.0753
.936	.7226	.9068	1.1202	1.0748
.884	.7291	.9074	1.1156	1.0721
.832	.7356	.8980	1.1049	1.0658
.780	.7572	.8977	1.0888	1.0561
.728	.7789	.8991	1.0744	1.0474
.676	.7735	.9050	1.0817	1.0518
.624	.7681	.9125	1.0900	1.0568
.572	.7875	.9192	1.0804	1.0510
.520	.8070	.9226	1.0692	1.0442
.468	.8373	.9208	1.0487	1.0314
.416	.8676	.9273	1.0338	1.0220
.364	.8752	.9276	1.0296	1.0193
.312	.8827	.9313	1.0272	1.0177
.260	.8935	.9328	1.0217	1.0142
.208	.9044	.9360	1.0173	1.0114
.156	.9000	.9400	1.0220	1.0144
.104	.9109	.9348	1.0131	1.0086
.052	.9044	.9393	1.0191	1.0125
0.000	.9173	.9371	1.0107	1.0070
-.052	.9109	.9341	1.0127	1.0083
-.104	.9044	.9302	1.0142	1.0093
-.156	.8935	.9271	1.0186	1.0122
-.208	.8827	.9273	1.0249	1.0163
-.260	.8622	.9225	1.0344	1.0224
-.312	.8416	.9160	1.0433	1.0280
-.364	.8167	.9136	1.0576	1.0370
-.416	.7919	.9079	1.0707	1.0451
-.468	.7756	.9023	1.0786	1.0499
-.520	.7594	.8934	1.0847	1.0536
-.572	.7302	.8933	1.1061	1.0665
-.624	.7010	.8915	1.1278	1.0792
-.676	.6967	.8906	1.1307	1.0809
-.728	.6923	.8913	1.1346	1.0832
-.780	.6967	.8906	1.1307	1.0809
-.832	.7010	.8899	1.1267	1.0786
-.884	.6999	.8917	1.1287	1.0797
-.936	.6988	.8935	1.1308	1.0809
-.988	.7042	.8993	1.1300	1.0805
-1.040	.7096	.9017	1.1272	1.0789

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(i) x/D = 2.5; y/D = 0.63; $\alpha = 0^\circ$;

p_∞ = 221.15 psf (10588.95 N/m²);
q_∞ = 396.31 psf (18975.41 N/m²);
$p_{t,\infty}$ = 940.00 psf (45007.44 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8718	.9460	1.0417	1.0270
.988	.8783	.9499	1.0399	1.0259
.936	.8848	.9421	1.0319	1.0207
.884	.8891	.9430	1.0299	1.0194
.832	.8935	.9423	1.0270	1.0176
.780	.9108	.9393	1.0155	1.0102
.728	.9281	.9380	1.0053	1.0035
.676	.9475	.9413	.9967	.9978
.624	.9670	.9412	.9866	.9911
.572	.9930	.9451	.9756	.9836
.520	1.0189	.9388	.9599	.9729
.468	1.0341	.9428	.9549	.9695
.416	1.0492	.9401	.9466	.9637
.364	1.0568	.9405	.9434	.9614
.312	1.0644	.9324	.9360	.9562
.260	1.0687	.9282	.9320	.9534
.208	1.0730	.9191	.9255	.9488
.156	1.0741	.9121	.9215	.9460
.104	1.0784	.9063	.9167	.9426
.052	1.0730	.8972	.9144	.9409
0.000	1.0838	.8952	.9088	.9369
-.052	1.0784	.9000	.9136	.9403
-.104	1.0730	.9078	.9198	.9447
-.156	1.0752	.9158	.9229	.9470
-.208	1.0773	.9187	.9235	.9474
-.260	1.0622	.9315	.9365	.9566
-.312	1.0470	.9342	.9446	.9623
-.364	1.0395	.9373	.9496	.9658
-.416	1.0319	.9353	.9520	.9675
-.468	1.0070	.9330	.9625	.9747
-.520	.9821	.9307	.9734	.9822
-.572	.9540	.9356	.9903	.9935
-.624	.9259	.9338	1.0043	1.0028
-.676	.9194	.9349	1.0084	1.0055
-.728	.9129	.9327	1.0108	1.0071
-.780	.8999	.9333	1.0184	1.0120
-.832	.8870	.9305	1.0243	1.0158
-.884	.8805	.9383	1.0323	1.0210
-.936	.8740	.9427	1.0386	1.0250
-.988	.8805	.9466	1.0369	1.0239
-1.040	.8870	.9405	1.0297	1.0194

(j) x/D = 2.5; y/D = 0.42; $\alpha = 0^\circ$;

p_∞ = 220.38 psf (10551.78 N/m²);
q_∞ = 394.92 psf (18908.79 N/m²);
$p_{t,\infty}$ = 936.70 psf (44849.44 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8054	.9276	1.0732	1.0466
.988	.8152	.9277	1.0668	1.0427
.936	.8250	.9277	1.0604	1.0388
.884	.8423	.9264	1.0487	1.0314
.832	.8597	.9301	1.0402	1.0260
.780	.8955	.9290	1.0185	1.0122
.728	.9313	.9279	.9981	.9988
.676	.9606	.9345	.9863	.9909
.624	.9900	.9361	.9724	.9815
.572	1.0258	.9399	.9572	.9711
.520	1.0616	.9284	.9352	.9557
.468	1.0746	.9227	.9266	.9496
.416	1.0876	.8967	.9080	.9362
.364	1.0800	.8507	.8875	.9212
.312	1.0724	.7671	.8457	.8897
.260	1.0670	.6789	.7977	.8519
.208	1.0616	.5879	.7442	.8077
.156	1.0724	.4816	.6701	.7430
.104	1.0670	.4571	.6545	.7289
.052	1.0627	.4282	.6348	.7107
0.000	1.0724	.4043	.6140	.6912
-.052	1.0681	.4267	.6321	.7082
-.104	1.0638	.5019	.6869	.7580
-.156	1.0703	.5666	.7276	.7936
-.208	1.0768	.6701	.7888	.8447
-.260	1.0779	.7695	.8449	.8891
-.312	1.0790	.8407	.8827	.9177
-.364	1.0779	.8900	.9087	.9368
-.416	1.0768	.9172	.9229	.9470
-.468	1.0507	.9270	.9393	.9586
-.520	1.0247	.9300	.9527	.9679
-.572	.9791	.9330	.9762	.9840
-.624	.9335	.9325	.9995	.9997
-.676	.9096	.9316	1.0120	1.0079
-.728	.8857	.9257	1.0223	1.0146
-.780	.8597	.9235	1.0364	1.0236
-.832	.8336	.9229	1.0522	1.0336
-.884	.8184	.9238	1.0624	1.0400
-.936	.8032	.9313	1.0768	1.0488
-.988	.8076	.9273	1.0715	1.0456
-1.040	.8119	.9315	1.0711	1.0454

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(k) $x/D = 2.5$; $y/D = 0.21$; $\alpha = 0^\circ$;

p_∞ = 222.03 psf (10630.63 N/m^2);
q_∞ = 397.87 psf (19050.10 N/m^2);
$p_{t,\infty}$ = 943.70 psf (45184.60 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7356	.9120	1.1134	1.0708
.988	.7541	.9056	1.0958	1.0604
.936	.7726	.9175	1.0897	1.0567
.884	.8042	.9222	1.0709	1.0452
.832	.8357	.9252	1.0522	1.0336
.780	.8793	.9245	1.0254	1.0166
.728	.9228	.9254	1.0014	1.0009
.676	.9587	.9309	.9854	.9903
.624	.9946	.9313	.9676	.9782
.572	1.0294	.9318	.9514	.9671
.520	1.0643	.9104	.9249	.9484
.468	1.0632	.8684	.9038	.9332
.416	1.0621	.7207	.8237	.8726
.364	1.0425	.5652	.7363	.8010
.312	1.0229	.3948	.6212	.6980
.260	1.0327	.2266	.4684	.5461
.208	1.0425	.1291	.3519	.4196
.156	1.0501	.0604	.2398	.2906
.104	1.0599	.0467	.2100	.2553
.052	1.0512	.0369	.1874	.2284
0.000	1.0773	.0375	.1866	.2274
-.052	1.0686	.0427	.1998	.2432
-.104	1.0599	.0558	.2295	.2785
-.156	1.0534	.0872	.2877	.3464
-.208	1.0469	.1763	.4104	.4841
-.260	1.0436	.2782	.5163	.5956
-.312	1.0403	.4693	.6717	.7444
-.364	1.0436	.6396	.7828	.8398
-.416	1.0469	.8264	.8885	.9220
-.468	1.0392	.9059	.9336	.9546
-.520	1.0316	.9242	.9465	.9636
-.572	.9914	.9313	.9692	.9793
-.624	.9511	.9316	.9897	.9932
-.676	.9239	.9296	1.0031	1.0020
-.728	.8967	.9242	1.0152	1.0100
-.780	.8597	.9205	1.0347	1.0226
-.832	.8227	.9183	1.0565	1.0363
-.884	.7824	.9134	1.0805	1.0511
-.936	.7422	.9167	1.1114	1.0696
-.988	.7411	.9085	1.1072	1.0672
-1.040	.7400	.9154	1.1122	1.0701

(l) $x/D = 2.5$; $y/D = 0.0$; $\alpha = 0^\circ$;

p_∞ = 221.98 psf (10628.38 N/m^2);
q_∞ = 397.79 psf (19046.06 N/m^2);
$p_{t,\infty}$ = 943.50 psf (45175.02 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6705	.8930	1.1541	1.0942
.988	.7053	.8990	1.1290	1.0799
.936	.7401	.9049	1.1057	1.0663
.884	.7586	.9019	1.0903	1.0570
.832	.7771	.9121	1.0834	1.0529
.780	.8337	.9110	1.0453	1.0293
.728	.8903	.9147	1.0136	1.0089
.676	.9295	.9247	.9974	.9983
.624	.9687	.9246	.9770	.9846
.572	1.0133	.9302	.9581	.9717
.520	1.0580	.9189	.9320	.9534
.468	1.0667	.9156	.9265	.9495
.416	1.0754	.8598	.8942	.9262
.364	1.0689	.7536	.8397	.8850
.312	1.0623	.5761	.7364	.8011
.260	1.0667	.4062	.6171	.6941
.208	1.0710	.2976	.5272	.6065
.156	1.0874	.2762	.5040	.5829
.104	1.0917	.2989	.5233	.6026
.052	1.0743	.2586	.4906	.5692
0.000	1.1124	.2295	.4542	.5311
-.052	1.0950	.2896	.5143	.5934
-.104	1.0776	.2981	.5260	.6053
-.156	1.0819	.2632	.4932	.5719
-.208	1.0863	.3123	.5362	.6156
-.260	1.0765	.4288	.6311	.7073
-.312	1.0667	.5909	.7443	.8078
-.364	1.0656	.7538	.8411	.8861
-.416	1.0645	.8899	.9143	.9408
-.468	1.0471	.9234	.9391	.9585
-.520	1.0297	.9249	.9477	.9645
-.572	.9807	.9234	.9704	.9801
-.624	.9317	.9253	.9965	.9977
-.676	.8936	.9201	1.0147	1.0097
-.728	.8555	.9099	1.0313	1.0204
-.780	.8142	.9036	1.0535	1.0344
-.832	.7728	.8989	1.0785	1.0499
-.884	.7510	.8975	1.0932	1.0588
-.936	.7293	.9078	1.1157	1.0722
-.988	.7020	.8906	1.1263	1.0783
-1.040	.6748	.8984	1.1538	1.0941

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(m) $x/D = 2.5$; $y/D = -0.42$; $\alpha = 0^\circ$;

p_∞ = 221.98 psf (10628.38 N/m^2);
q_∞ = 397.79 psf (19046.06 N/m^2);
$p_{t,\infty}$ = 943.50 psf (45175.02 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.5943	.8915	1.2248	1.1326
.988	.6074	.8894	1.2101	1.1249
.936	.6204	.8806	1.1914	1.1149
.884	.5932	.8684	1.2099	1.1248
.832	.5660	.8661	1.2370	1.1390
.780	.6498	.8759	1.1610	1.0981
.728	.7336	.8920	1.1027	1.0645
.676	.7674	.9048	1.0859	1.0544
.624	.8011	.9024	1.0614	1.0393
.572	.8414	.9107	1.0404	1.0262
.520	.8816	.9004	1.0106	1.0070
.468	.9045	.9065	1.0011	1.0007
.416	.9274	.9025	.9865	.9910
.364	.9361	.9061	.9838	.9892
.312	.9448	.8995	.9757	.9838
.260	.9698	.9018	.9643	.9760
.208	.9948	.8873	.9444	.9622
.156	.9927	.8809	.9420	.9605
.104	1.0177	.8494	.9136	.9403
.052	1.0112	.7641	.8693	.9077
0.000	1.0406	.6746	.8052	.8579
-.052	1.0340	.7564	.8553	.8970
-.104	1.0275	.8476	.9083	.9364
-.156	1.0253	.8666	.9193	.9444
-.208	1.0231	.8737	.9241	.9478
-.260	.9959	.8938	.9473	.9642
-.312	.9687	.8953	.9613	.9739
-.364	.9546	.9045	.9734	.9822
-.416	.9404	.9003	.9784	.9856
-.468	.9012	.9071	1.0032	1.0021
-.520	.8620	.9038	1.0239	1.0156
-.572	.8196	.8976	1.0465	1.0301
-.624	.7771	.8998	1.0760	1.0484
-.676	.7401	.8943	1.0992	1.0624
-.728	.7031	.8871	1.1232	1.0765
-.780	.6509	.8490	1.1421	1.0874
-.832	.5986	.8576	1.1969	1.1178
-.884	.6128	.8669	1.1894	1.1138
-.936	.6269	.8896	1.1912	1.1147
-.988	.6302	.8940	1.1910	1.1147
-1.040	.6335	.8968	1.1898	1.1140

(n) $x/D = 3.0$; $y/D = 0.0$; $\alpha = 0^\circ$;

p_∞ = 221.23 psf (10592.33 N/m^2);
q_∞ = 396.44 psf (18981.46 N/m^2);
$p_{t,\infty}$ = 940.30 psf (45021.81 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8546	.9441	1.0510	1.0329
.988	.9217	.9526	1.0166	1.0109
.936	.9888	.9410	.9755	.9836
.884	1.0126	.9451	.9661	.9772
.832	1.0364	.9376	.9511	.9669
.780	1.0429	.9398	.9493	.9656
.728	1.0494	.9420	.9474	.9643
.676	1.0818	.9311	.9277	.9504
.624	1.1143	.9252	.9112	.9386
.572	1.1424	.9251	.8999	.9303
.520	1.1705	.9132	.8832	.9181
.468	1.1965	.9032	.8689	.9073
.416	1.2225	.8644	.8409	.8860
.364	1.2387	.7997	.8035	.8565
.312	1.2549	.7135	.7540	.8160
.260	1.2549	.6023	.6928	.7633
.208	1.2549	.5050	.6344	.7103
.156	1.2744	.4469	.5922	.6705
.104	1.2744	.4509	.5948	.6730
.052	1.2603	.4292	.5836	.6622
0.000	1.2939	.4164	.5673	.6463
-.052	1.2798	.4443	.5892	.6676
-.104	1.2657	.4486	.5954	.6735
-.156	1.2701	.4373	.5868	.6653
-.208	1.2744	.5195	.6385	.7141
-.260	1.2517	.6164	.7018	.7711
-.312	1.2289	.7387	.7753	.8336
-.364	1.2051	.8342	.8320	.8791
-.416	1.1813	.8862	.8661	.9053
-.468	1.1586	.9158	.8891	.9224
-.520	1.1359	.9200	.9000	.9304
-.572	1.1132	.9258	.9120	.9391
-.624	1.0905	.9266	.9218	.9462
-.676	1.0786	.9304	.9288	.9512
-.728	1.0667	.9242	.9308	.9526
-.780	1.0450	.9331	.9449	.9625
-.832	1.0234	.9319	.9543	.9690
-.884	.9812	.9411	.9793	.9862
-.936	.9390	.9367	.9988	.9992
-.988	.8763	.9409	1.0362	1.0235
-1.040	.8135	.9299	1.0691	1.0441

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(o) x/D = 4.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 221.46 psf (10603.60 N/m^2);
q_∞ = 396.86 psf (19001.65 N/m^2);
$p_{t,\infty}$ = 941.30 psf (45069.69 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1507	.9585	.9127	.9396
.988	1.1540	.9495	.9071	.9356
.936	1.1572	.9522	.9071	.9356
.884	1.1583	.9436	.9026	.9323
.832	1.1594	.9434	.9021	.9319
.780	1.1388	.9438	.9104	.9380
.728	1.1183	.9459	.9197	.9447
.676	1.1367	.9341	.9065	.9352
.624	1.1550	.9240	.8944	.9263
.572	1.1540	.9191	.8925	.9249
.520	1.1529	.9075	.8872	.9210
.468	1.1367	.8970	.8883	.9219
.416	1.1205	.8713	.8818	.9170
.364	1.1183	.8395	.8664	.9055
.312	1.1162	.7992	.8462	.8901
.260	1.1108	.7662	.8305	.8779
.208	1.1054	.7399	.8182	.8682
.156	1.1205	.7026	.7919	.8472
.104	1.1151	.6813	.7816	.8389
.052	1.1021	.6337	.7583	.8195
0.000	1.1248	.6167	.7404	.8045
-.052	1.1119	.6436	.7609	.8217
-.104	1.0989	.6809	.7871	.8433
-.156	1.1162	.7031	.7937	.8486
-.208	1.1334	.7288	.8019	.8552
-.260	1.1291	.7553	.8179	.8680
-.312	1.1248	.8123	.8498	.8928
-.364	1.1291	.8538	.8696	.9079
-.416	1.1334	.8817	.8820	.9171
-.468	1.1399	.9041	.8906	.9235
-.520	1.1464	.9146	.8932	.9255
-.572	1.1475	.9245	.8976	.9287
-.624	1.1486	.9277	.8987	.9295
-.676	1.1496	.9275	.8982	.9291
-.728	1.1507	.9340	.9009	.9311
-.780	1.1496	.9342	.9015	.9315
-.832	1.1486	.9428	.9060	.9348
-.884	1.1486	.9428	.9060	.9348
-.936	1.1486	.9479	.9085	.9366
-.988	1.1464	.9500	.9103	.9379
-1.040	1.1442	.9554	.9138	.9404

(p) x/D = 5.0; y/D = 3.0; $\alpha = 0^\circ$;

p_∞ = 221.32 psf (10596.84 N/m^2);
q_∞ = 396.60 psf (18989.54 N/m^2);
$p_{t,\infty}$ = 940.70 psf (45040.96 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8480	.9755	1.0725	1.0462
.988	.8556	.9676	1.0634	1.0406
.936	.8631	.9762	1.0635	1.0407
.884	.8599	.9652	1.0595	1.0382
.832	.8566	.9674	1.0627	1.0402
.780	.8620	.9631	1.0570	1.0366
.728	.8674	.9639	1.0541	1.0348
.676	.8534	.9646	1.0632	1.0405
.624	.8393	.9670	1.0733	1.0467
.572	.8415	.9666	1.0718	1.0458
.520	.8437	.9696	1.0720	1.0459
.468	.8501	.9651	1.0655	1.0419
.416	.8566	.9674	1.0627	1.0402
.364	.8501	.9651	1.0655	1.0419
.312	.8437	.9662	1.0702	1.0448
.260	.8415	.9666	1.0718	1.0458
.208	.8393	.9670	1.0733	1.0467
.156	.8415	.9666	1.0718	1.0458
.104	.8393	.9670	1.0733	1.0467
.052	.8382	.9671	1.0741	1.0472
0.000	.8393	.9802	1.0807	1.0512
-.052	.8382	.9630	1.0719	1.0458
-.104	.8372	.9632	1.0726	1.0463
-.156	.8372	.9632	1.0726	1.0463
-.208	.8372	.9632	1.0726	1.0463
-.260	.8328	.9623	1.0749	1.0477
-.312	.8285	.9630	1.0781	1.0497
-.364	.8328	.9623	1.0749	1.0477
-.416	.8372	.9616	1.0717	1.0457
-.468	.8372	.9616	1.0717	1.0457
-.520	.8372	.9632	1.0726	1.0463
-.572	.8415	.9625	1.0695	1.0444
-.624	.8458	.9618	1.0663	1.0424
-.676	.8491	.9612	1.0640	1.0410
-.728	.8523	.9673	1.0653	1.0418
-.780	.8523	.9623	1.0626	1.0401
-.832	.8523	.9656	1.0644	1.0412
-.884	.8534	.9621	1.0618	1.0396
-.936	.8545	.9736	1.0674	1.0431
-.988	.8566	.9616	1.0595	1.0382
-1.040	.8588	.9745	1.0652	1.0417

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(q) x/D = 5.0; y/D = 2.0; $\alpha = 0^\circ$;

p_∞ = 221,37 psf (10599.09 N/m^2);
q_∞ = 396.69 psf (18993.57 N/m^2);
$p_{t,\infty}$ = 940.90 psf (45050.53 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0879	1.0027	.9600	.9730
.988	1.1008	.9987	.9525	.9678
.936	1.1138	1.0014	.9482	.9648
.884	1.1084	.9990	.9494	.9656
.832	1.1030	.9966	.9506	.9665
.780	1.0944	1.0099	.9606	.9734
.728	1.0857	1.0081	.9636	.9755
.676	1.0922	.9985	.9562	.9704
.624	1.0987	1.0007	.9544	.9691
.572	1.1041	1.0031	.9532	.9683
.520	1.1095	.9955	.9472	.9641
.468	1.1117	1.0018	.9493	.9656
.416	1.1138	1.0014	.9482	.9648
.364	1.1127	1.0016	.9487	.9652
.312	1.1117	.9968	.9469	.9639
.260	1.1106	1.0036	.9506	.9665
.208	1.1095	1.0022	.9504	.9664
.156	1.1235	1.0030	.9448	.9625
.104	1.1225	1.0015	.9446	.9623
.052	1.1257	.9993	.9422	.9606
0.000	1.1354	.9908	.9341	.9550
-.052	1.1387	.9936	.9341	.9549
-.104	1.1419	.9913	.9317	.9533
-.156	1.1376	.9955	.9354	.9559
-.208	1.1333	.9929	.9360	.9563
-.260	1.1300	.9968	.9392	.9585
-.312	1.1268	.9991	.9416	.9602
-.364	1.1300	1.0018	.9416	.9602
-.416	1.1333	.9962	.9376	.9574
-.468	1.1290	1.0054	.9437	.9617
-.520	1.1246	.9995	.9427	.9610
-.572	1.1257	1.0043	.9445	.9623
-.624	1.1268	.9924	.9385	.9580
-.676	1.1203	.9969	.9433	.9614
-.728	1.1138	.9930	.9442	.9620
-.780	1.1138	.9980	.9466	.9637
-.832	1.1138	.9930	.9442	.9620
-.884	1.1117	.9968	.9469	.9639
-.936	1.1095	.9988	.9488	.9653
-.988	1.1041	.9981	.9508	.9666
-1.040	1.0987	.9924	.9504	.9664

(r) x/D = 5.0; y/D = 1.5; $\alpha = 0^\circ$;

p_∞ = 221.39 psf (10600.22 N/m^2);
q_∞ = 396.73 psf (18995.59 N/m^2);
$p_{t,\infty}$ = 941.00 psf (45055.32 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1146	.9979	.9462	.9634
.988	1.1243	.9928	.9397	.9589
.936	1.1341	.9927	.9356	.9560
.884	1.1297	.9902	.9362	.9564
.832	1.1254	.9893	.9375	.9574
.780	1.1125	.9983	.9473	.9642
.728	1.0995	1.0006	.9539	.9688
.676	1.1081	.9890	.9447	.9624
.624	1.1168	.9891	.9411	.9599
.572	1.1200	.9902	.9403	.9593
.520	1.1233	.9863	.9370	.9570
.468	1.1243	.9878	.9373	.9572
.416	1.1254	.9876	.9368	.9568
.364	1.1243	.9878	.9373	.9572
.312	1.1233	.9846	.9362	.9565
.260	1.1189	.9921	.9416	.9602
.208	1.1146	.9878	.9414	.9601
.156	1.1308	.9866	.9341	.9549
.104	1.1265	.9857	.9354	.9559
.052	1.1297	.9834	.9330	.9542
0.000	1.1384	.9769	.9263	.9494
-.052	1.1416	.9809	.9270	.9499
-.104	1.1449	.9804	.9254	.9487
-.156	1.1416	.9826	.9278	.9504
-.208	1.1384	.9815	.9286	.9510
-.260	1.1362	.9870	.9320	.9534
-.312	1.1341	.9890	.9339	.9548
-.364	1.1351	.9888	.9333	.9544
-.416	1.1362	.9886	.9328	.9540
-.468	1.1351	.9939	.9357	.9561
-.520	1.1341	.9873	.9331	.9542
-.572	1.1341	.9907	.9347	.9553
-.624	1.1341	.9840	.9315	.9531
-.676	1.1297	.9848	.9336	.9546
-.728	1.1254	.9855	.9358	.9561
-.780	1.1297	.9864	.9344	.9552
-.832	1.1341	.9873	.9331	.9542
-.884	1.1297	.9881	.9352	.9557
-.936	1.1254	.9939	.9398	.9589
-.988	1.1200	.9932	.9417	.9603
-1.040	1.1146	.9925	.9436	.9616

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(s) x/D = 5.0; y/D = 1.0; $\alpha = 0^o$;

p_∞ = 221.32 psf (10596.84 N/m^2);
q_∞ = 396.60 psf (18989.54 N/m^2);
$p_{t,\infty}$ = 940.70 psf (45040.96 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1119	.9833	.9404	.9594
.988	1.1173	.9790	.9361	.9563
.936	1.1227	.9797	.9341	.9550
.884	1.1195	.9769	.9342	.9550
.832	1.1162	.9741	.9342	.9550
.780	1.1011	.9819	.9443	.9621
.728	1.0859	.9829	.9514	.9670
.676	1.0913	.9685	.9421	.9605
.624	1.0967	.9693	.9401	.9591
.572	1.0989	.9689	.9390	.9584
.520	1.1011	.9618	.9346	.9553
.468	1.0989	.9638	.9365	.9566
.416	1.0967	.9592	.9352	.9557
.364	1.0967	.9575	.9344	.9551
.312	1.0967	.9491	.9303	.9522
.260	1.0913	.9534	.9347	.9554
.208	1.0859	.9460	.9334	.9544
.156	1.1043	.9427	.9239	.9477
.104	1.0989	.9386	.9242	.9479
.052	1.1000	.9385	.9237	.9475
0.000	1.1119	.9296	.9143	.9408
-.052	1.1130	.9315	.9148	.9412
-.104	1.1141	.9380	.9176	.9432
-.156	1.1151	.9378	.9170	.9428
-.208	1.1162	.9376	.9165	.9424
-.260	1.1130	.9483	.9230	.9471
-.312	1.1097	.9522	.9263	.9494
-.364	1.1108	.9587	.9290	.9513
-.416	1.1119	.9585	.9285	.9510
-.468	1.1130	.9650	.9312	.9529
-.520	1.1141	.9632	.9298	.9519
-.572	1.1151	.9663	.9309	.9527
-.624	1.1162	.9594	.9271	.9500
-.676	1.1141	.9632	.9298	.9519
-.728	1.1119	.9636	.9309	.9527
-.780	1.1141	.9665	.9314	.9531
-.832	1.1162	.9712	.9328	.9540
-.884	1.1162	.9728	.9336	.9546
-.936	1.1162	.9779	.9360	.9563
-.988	1.1119	.9787	.9382	.9578
-1.040	1.1076	.9778	.9396	.9588

(t) x/D = 5.0; y/D = 0.83; $\alpha = 0^o$;

p_∞ = 221.32 psf (10596.84 N/m^2);
q_∞ = 396.60 psf (18989.54 N/m^2);
$p_{t,\infty}$ = 940.70 psf (45040.96 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1150	.9778	.9365	.9566
.988	1.1204	.9718	.9313	.9530
.936	1.1258	.9725	.9294	.9516
.884	1.1225	.9681	.9287	.9511
.832	1.1193	.9636	.9279	.9505
.780	1.1009	.9736	.9404	.9594
.728	1.0826	.9719	.9475	.9643
.676	1.0901	.9588	.9378	.9576
.624	1.0977	.9574	.9339	.9548
.572	1.0988	.9556	.9326	.9538
.520	1.0999	.9436	.9263	.9494
.468	1.0955	.9427	.9276	.9504
.416	1.0912	.9284	.9224	.9466
.364	1.0891	.9187	.9185	.9438
.312	1.0869	.9073	.9137	.9403
.260	1.0793	.8969	.9116	.9388
.208	1.0718	.8932	.9129	.9398
.156	1.0912	.8745	.8952	.9269
.104	1.0837	.8658	.8938	.9259
.052	1.0793	.8683	.8969	.9282
0.000	1.0955	.8552	.8835	.9183
-.052	1.0912	.8491	.8821	.9172
-.104	1.0869	.8650	.8921	.9246
-.156	1.0945	.8788	.8961	.9275
-.208	1.1020	.8774	.8923	.9248
-.260	1.0988	.9082	.9091	.9371
-.312	1.0955	.9172	.9150	.9413
-.364	1.0988	.9350	.9225	.9467
-.416	1.1020	.9378	.9225	.9467
-.468	1.1074	.9485	.9255	.9488
-.520	1.1128	.9492	.9236	.9475
-.572	1.1150	.9572	.9265	.9496
-.624	1.1171	.9518	.9230	.9471
-.676	1.1150	.9572	.9265	.9496
-.728	1.1128	.9576	.9276	.9503
-.780	1.1139	.9607	.9287	.9511
-.832	1.1150	.9622	.9290	.9513
-.884	1.1161	.9670	.9308	.9526
-.936	1.1171	.9719	.9327	.9540
-.988	1.1150	.9723	.9338	.9547
-1.040	1.1128	.9726	.9349	.9555

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(u) x/D = 5.0; y/D = 0.63; $\alpha = 0^\circ$;

p_∞ = 221.32 psf (10596.84 N/m^2);
q_∞ = 396.60 psf (18989.54 N/m^2);
$p_{t,\infty}$ = 940.70 psf (45040.96 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0869	.9698	.9446	.9623
.988	1.0923	.9638	.9394	.9586
.936	1.0977	.9629	.9366	.9567
.884	1.0945	.9584	.9358	.9561
.832	1.0912	.9557	.9358	.9562
.780	1.0750	.9619	.9459	.9632
.728	1.0588	.9598	.9521	.9675
.676	1.0664	.9434	.9406	.9595
.624	1.0739	.9353	.9332	.9543
.572	1.0728	.9221	.9271	.9499
.520	1.0718	.9038	.9183	.9437
.468	1.0620	.8921	.9165	.9424
.416	1.0523	.8519	.8997	.9302
.364	1.0491	.8306	.8898	.9229
.312	1.0458	.7974	.8732	.9106
.260	1.0426	.7727	.8609	.9013
.208	1.0394	.7377	.8425	.8872
.156	1.0523	.7181	.8261	.8744
.104	1.0491	.6949	.8139	.8648
.052	1.0415	.6981	.8187	.8686
0.000	1.0588	.6861	.8050	.8577
-.052	1.0512	.6993	.8156	.8662
-.104	1.0437	.7161	.8283	.8762
-.156	1.0534	.7481	.8427	.8874
-.208	1.0631	.7768	.8548	.8966
-.260	1.0588	.8063	.8726	.9102
-.312	1.0545	.8307	.8876	.9213
-.364	1.0620	.8746	.9075	.9359
-.416	1.0696	.8900	.9122	.9393
-.468	1.0772	.9054	.9168	.9426
-.520	1.0847	.9292	.9255	.9488
-.572	1.0891	.9384	.9283	.9508
-.624	1.0934	.9377	.9261	.9492
-.676	1.0923	.9446	.9299	.9520
-.728	1.0912	.9447	.9305	.9524
-.780	1.0923	.9529	.9340	.9549
-.832	1.0934	.9527	.9335	.9545
-.884	1.0945	.9559	.9345	.9553
-.936	1.0955	.9624	.9373	.9572
-.988	1.0934	.9628	.9384	.9579
-1.040	1.0912	.9631	.9395	.9587

(v) x/D = 5.0; y/D = 0.42; $\alpha = 0^\circ$;

p_∞ = 221.37 psf (10599.09 N/m^2);
q_∞ = 396.69 psf (18993.57 N/m^2);
$p_{t,\infty}$ = 940.90 psf (45050.53 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0780	.9596	.9435	.9615
.988	1.0834	.9552	.9390	.9584
.936	1.0888	.9543	.9362	.9564
.884	1.0845	.9483	.9351	.9557
.832	1.0802	.9441	.9349	.9555
.780	1.0640	.9520	.9459	.9632
.728	1.0478	.9482	.9513	.9670
.676	1.0575	.9281	.9368	.9568
.624	1.0672	.9179	.9274	.9502
.572	1.0640	.9084	.9240	.9478
.520	1.0607	.8805	.9111	.9385
.468	1.0499	.8488	.8991	.9298
.416	1.0391	.8019	.8785	.9145
.364	1.0348	.7639	.8592	.9000
.312	1.0305	.7206	.8362	.8823
.260	1.0251	.6807	.8149	.8656
.208	1.0197	.6493	.7980	.8521
.156	1.0327	.6260	.7786	.8363
.104	1.0273	.6150	.7738	.8324
.052	1.0165	.6121	.7760	.8342
0.000	1.0348	.6082	.7667	.8265
-.052	1.0240	.6173	.7764	.8346
-.104	1.0132	.6281	.7874	.8435
-.156	1.0273	.6458	.7929	.8480
-.208	1.0413	.6738	.8044	.8573
-.260	1.0381	.7154	.8301	.8776
-.312	1.0348	.7567	.8551	.8969
-.364	1.0435	.8040	.8778	.9140
-.416	1.0521	.8461	.8968	.9281
-.468	1.0618	.8829	.9119	.9391
-.520	1.0715	.9063	.9197	.9447
-.572	1.0769	.9204	.9245	.9481
-.624	1.0823	.9244	.9242	.9479
-.676	1.0823	.9345	.9292	.9515
-.728	1.0823	.9345	.9292	.9515
-.780	1.0834	.9443	.9336	.9546
-.832	1.0845	.9441	.9330	.9542
-.884	1.0877	.9519	.9355	.9559
-.936	1.0910	.9530	.9346	.9553
-.988	1.0877	.9553	.9371	.9571
-1.040	1.0845	.9558	.9388	.9583

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(w) x/D = 5.0; y/D = 0.21; $\alpha = 0^o$;

p_∞ = 221.34 psf (10597.97 N/m^2);
q_∞ = 396.65 psf (18991.56 N/m^2);
$p_{t,\infty}$ = 940.80 psf (45045.75 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0695	.9574	.9462	.9634
.988	1.0771	.9527	.9405	.9595
.936	1.0846	.9514	.9366	.9567
.884	1.0825	.9467	.9352	.9557
.832	1.0803	.9438	.9347	.9553
.780	1.0663	.9496	.9437	.9617
.728	1.0522	.9471	.9488	.9652
.676	1.0652	.9297	.9343	.9550
.624	1.0781	.9173	.9224	.9466
.572	1.0738	.9063	.9187	.9440
.520	1.0695	.8819	.9081	.9363
.468	1.0554	.8592	.9022	.9321
.416	1.0414	.8264	.8908	.9237
.364	1.0338	.7906	.8745	.9116
.312	1.0263	.7582	.8595	.9002
.260	1.0176	.7208	.8416	.8865
.208	1.0090	.6918	.8280	.8760
.156	1.0230	.6668	.8073	.8596
.104	1.0144	.6634	.8087	.8607
.052	1.0058	.6531	.8058	.8584
0.000	1.0198	.6503	.7985	.8525
−.052	1.0112	.6467	.7997	.8535
−.104	1.0025	.6655	.8148	.8655
−.156	1.0209	.6807	.8165	.8669
−.208	1.0392	.6907	.8152	.8659
−.260	1.0371	.7337	.8411	.8861
−.312	1.0349	.7696	.8624	.9024
−.364	1.0446	.8100	.8806	.9161
−.416	1.0544	.8537	.8998	.9303
−.468	1.0619	.8809	.9108	.9383
−.520	1.0695	.8979	.9163	.9422
−.572	1.0717	.9210	.9271	.9499
−.624	1.0738	.9206	.9259	.9491
−.676	1.0727	.9292	.9307	.9525
−.728	1.0717	.9294	.9313	.9529
−.780	1.0727	.9359	.9341	.9549
−.832	1.0738	.9357	.9335	.9545
−.884	1.0749	.9456	.9379	.9576
−.936	1.0760	.9454	.9374	.9572
−.988	1.0738	.9491	.9401	.9592
−1.040	1.0717	.9495	.9413	.9600

(x) x/D = 5.0; y/D = 0.0; $\alpha = 0^o$;

p_∞ = 221.34 psf (10597.97 N/m^2);
q_∞ = 396.65 psf (18991.56 N/m^2);
$p_{t,\infty}$ = 940.80 psf (45045.75 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0476	.9516	.9531	.9682
.988	1.0541	.9488	.9487	.9652
.936	1.0606	.9409	.9419	.9604
.884	1.0541	.9404	.9445	.9623
.832	1.0476	.9349	.9446	.9623
.780	1.0304	.9379	.9541	.9689
.728	1.0131	.9410	.9638	.9756
.676	1.0260	.9253	.9496	.9658
.624	1.0390	.9180	.9400	.9591
.572	1.0401	.9161	.9385	.9580
.520	1.0412	.9008	.9302	.9521
.468	1.0336	.8904	.9282	.9507
.416	1.0260	.8717	.9217	.9461
.364	1.0228	.8538	.9137	.9403
.312	1.0196	.8241	.8991	.9297
.260	1.0174	.8077	.8910	.9238
.208	1.0152	.7828	.8781	.9142
.156	1.0196	.7634	.8653	.9046
.104	1.0174	.7350	.8499	.8930
.052	1.0120	.6952	.8288	.8766
0.000	1.0196	.6886	.8218	.8711
−.052	1.0142	.7006	.8312	.8784
−.104	1.0088	.7356	.8539	.8960
−.156	1.0282	.7539	.8563	.8978
−.208	1.0476	.7807	.8632	.9031
−.260	1.0422	.8104	.8818	.9170
−.312	1.0368	.8400	.9001	.9305
−.364	1.0422	.8592	.9079	.9362
−.416	1.0476	.8750	.9139	.9405
−.468	1.0498	.9014	.9266	.9496
−.520	1.0520	.9077	.9289	.9513
−.572	1.0574	.9202	.9329	.9541
−.624	1.0628	.9158	.9283	.9508
−.676	1.0649	.9255	.9322	.9536
−.728	1.0671	.9234	.9303	.9522
−.780	1.0682	.9333	.9347	.9554
−.832	1.0692	.9314	.9333	.9544
−.884	1.0703	.9396	.9369	.9569
−.936	1.0714	.9427	.9380	.9577
−.988	1.0682	.9500	.9431	.9613
−1.040	1.0649	.9489	.9440	.9619

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(y) $x/D = 5.0$; $y/D = -0.42$; $\alpha = 0^\circ$;

p_∞ = 221.34 psf (10597.97 N/m^2);
q_∞ = 396.65 psf (18991.56 N/m^2);
$p_{t,\infty}$ = 940.80 psf (45045.75 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0131	.9557	.9713	.9807
.988	1.0217	.9609	.9698	.9797
.936	1.0304	.9510	.9607	.9735
.884	1.0250	.9570	.9663	.9773
.832	1.0196	.9512	.9659	.9771
.780	1.0066	.9468	.9699	.9798
.728	.9936	.9458	.9756	.9837
.676	1.0034	.9374	.9666	.9775
.624	1.0131	.9323	.9593	.9725
.572	1.0152	.9319	.9581	.9717
.520	1.0174	.9198	.9508	.9667
.468	1.0142	.9221	.9535	.9685
.416	1.0109	.9143	.9510	.9668
.364	1.0077	.9132	.9519	.9674
.312	1.0044	.9054	.9494	.9657
.260	1.0012	.9009	.9486	.9651
.208	.9980	.8814	.9398	.9589
.156	1.0098	.8624	.9241	.9479
.104	1.0066	.8210	.9031	.9327
.052	1.0077	.7752	.8771	.9135
0.000	1.0152	.7331	.8498	.8928
-.052	1.0163	.7681	.8693	.9077
-.104	1.0174	.8168	.8960	.9275
-.156	1.0217	.8546	.9146	.9410
-.208	1.0260	.8740	.9229	.9470
-.260	1.0228	.8963	.9361	.9564
-.312	1.0196	.8986	.9388	.9582
-.364	1.0206	.9118	.9452	.9627
-.416	1.0217	.9099	.9437	.9617
-.468	1.0206	.9235	.9512	.9669
-.520	1.0196	.9237	.9518	.9673
-.572	1.0250	.9311	.9531	.9682
-.624	1.0304	.9284	.9493	.9656
-.676	1.0282	.9355	.9539	.9688
-.728	1.0260	.9359	.9551	.9696
-.780	1.0293	.9453	.9584	.9719
-.832	1.0325	.9431	.9557	.9700
-.884	1.0336	.9529	.9602	.9731
-.936	1.0347	.9511	.9587	.9721
-.988	1.0379	.9639	.9637	.9755
-1.040	1.0412	.9566	.9585	.9720

(z) $x/D = 6.0$; $y/D = 0.0$; $\alpha = 0^\circ$;

p_∞ = 221.37 psf (10599.09 N/m^2);
q_∞ = 396.69 psf (18993.57 N/m^2);
$p_{t,\infty}$ = 940.90 psf (45050.53 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1010	.9575	.9325	.9538
.988	1.1086	.9561	.9287	.9511
.936	1.1161	.9514	.9232	.9472
.884	1.1075	.9512	.9268	.9497
.832	1.0989	.9511	.9304	.9523
.780	1.0891	.9478	.9329	.9541
.728	1.0794	.9513	.9388	.9582
.676	1.1107	.9372	.9186	.9439
.624	1.1420	.9180	.8966	.9279
.572	1.1334	.9179	.8999	.9304
.520	1.1248	.9043	.8967	.9280
.468	1.0740	.8884	.9095	.9373
.416	1.0233	.8774	.9260	.9492
.364	.9974	.8518	.9241	.9479
.312	.9715	.8363	.9278	.9505
.260	.9661	.8154	.9187	.9440
.208	.9607	.7962	.9104	.9380
.156	.9704	.7725	.8922	.9247
.104	.9650	.7516	.8825	.9175
.052	.9834	.7227	.8573	.8986
0.000	.9693	.7186	.8610	.9014
-.052	.9877	.7314	.8605	.9010
-.104	1.0060	.7636	.8712	.9091
-.156	1.0524	.7718	.8563	.8978
-.208	1.0989	.7986	.8525	.8949
-.260	1.1032	.8114	.8576	.8988
-.312	1.1075	.8445	.8732	.9106
-.364	1.1097	.8644	.8826	.9176
-.416	1.1118	.8826	.8910	.9238
-.468	1.1129	.9061	.9023	.9321
-.520	1.1140	.9177	.9076	.9360
-.572	1.1129	.9246	.9115	.9388
-.624	1.1118	.9282	.9137	.9404
-.676	1.1194	.9319	.9124	.9394
-.728	1.1269	.9305	.9087	.9367
-.780	1.1194	.9403	.9165	.9424
-.832	1.1118	.9450	.9219	.9463
-.884	1.1075	.9458	.9241	.9478
-.936	1.1032	.9516	.9288	.9512
-.988	1.0999	.9589	.9337	.9547
-1.040	1.0967	.9545	.9329	.9541

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(aa) x/D = 7.0; y/D = 0.0; $\alpha = 0^o$;

p_∞ = 221.37 psf (10599.09 N/m^2);
q_∞ = 396.69 psf (18993.57 N/m^2);
$p_{t,\infty}$ = 940.90 psf (45050.53 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0363	.9588	.9619	.9743
.988	1.0654	.9620	.9503	.9663
.936	1.0945	.9535	.9333	.9544
.884	1.1226	.9535	.9216	.9460
.832	1.1507	.9500	.9086	.9367
.780	1.1604	.9516	.9056	.9345
.728	1.1701	.9448	.8986	.9294
.676	1.1895	.9344	.8863	.9204
.624	1.2090	.9308	.8775	.9138
.572	1.2500	.9197	.8578	.8989
.520	1.2910	.9050	.8373	.8832
.468	1.2910	.8914	.8310	.8782
.416	1.2910	.8692	.8205	.8701
.364	1.2932	.8448	.8083	.8604
.312	1.2953	.8255	.7983	.8524
.260	1.2813	.7974	.7889	.8447
.208	1.2673	.7778	.7834	.8403
.156	1.2770	.7568	.7698	.8291
.104	1.2629	.7320	.7613	.8221
.052	1.2521	.7168	.7566	.8182
0.000	1.2586	.7102	.7512	.8136
-.052	1.2478	.7291	.7644	.8246
-.104	1.2370	.7557	.7816	.8388
-.156	1.2554	.7710	.7837	.8405
-.208	1.2737	.7915	.7883	.8443
-.260	1.2489	.8258	.8132	.8642
-.312	1.2241	.8427	.8297	.8773
-.364	1.2025	.8742	.8527	.8950
-.416	1.1809	.8919	.8691	.9075
-.468	1.1518	.9127	.8902	.9232
-.520	1.1226	.9231	.9068	.9354
-.572	1.0773	.9263	.9273	.9501
-.624	1.0319	.9344	.9516	.9672
-.676	1.0114	.9397	.9639	.9757
-.728	.9909	.9349	.9713	.9808
-.780	.9834	.9447	.9801	.9867
-.832	.9758	.9393	.9811	.9874
-.884	.9736	.9514	.9885	.9924
-.936	.9715	.9484	.9881	.9921
-.988	.9715	.9602	.9942	.9961
-1.040	.9715	.9585	.9933	.9955

(bb) x/D = 8.0; y/D = 0.0; $\alpha = 0^o$;

p_∞ = 221.41 psf (10601.35 N/m^2);
q_∞ = 396.77 psf (18997.61 N/m^2);
$p_{t,\infty}$ = 941.10 psf (45060.11 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2128	.9661	.8925	.9249
.988	1.2117	.9545	.8875	.9213
.936	1.2106	.9580	.8896	.9228
.884	1.2084	.9467	.8851	.9194
.832	1.2063	.9454	.8853	.9196
.780	1.1836	.9462	.8941	.9261
.728	1.1609	.9504	.9048	.9339
.676	1.1857	.9323	.8867	.9207
.624	1.2106	.9176	.8706	.9086
.572	1.2074	.9097	.8680	.9067
.520	1.2041	.9002	.8646	.9041
.468	1.1836	.8889	.8666	.9056
.416	1.1630	.8809	.8703	.9084
.364	1.1684	.8613	.8586	.8995
.312	1.1739	.8484	.8502	.8931
.260	1.1684	.8308	.8432	.8878
.208	1.1630	.8132	.8362	.8823
.156	1.1814	.7874	.8164	.8668
.104	1.1760	.7697	.8090	.8609
.052	1.1771	.7472	.7967	.8511
0.000	1.1890	.7414	.7897	.8454
-.052	1.1901	.7502	.7939	.8488
-.104	1.1911	.7761	.8072	.8595
-.156	1.2225	.7733	.7953	.8500
-.208	1.2538	.7984	.7980	.8521
-.260	1.2398	.8239	.8152	.8658
-.312	1.2257	.8422	.8289	.8767
-.364	1.2193	.8694	.8444	.8887
-.416	1.2128	.8948	.8590	.8998
-.468	1.2182	.9041	.8615	.9018
-.520	1.2236	.9203	.8673	.9061
-.572	1.2225	.9291	.8718	.9095
-.624	1.2214	.9379	.8763	.9129
-.676	1.2279	.9367	.8734	.9107
-.728	1.2344	.9492	.8769	.9134
-.780	1.2290	.9502	.8793	.9152
-.832	1.2236	.9615	.8865	.9205
-.884	1.2301	.9552	.8812	.9166
-.936	1.2365	.9694	.8854	.9197
-.988	1.2409	.9669	.8827	.9177
-1.040	1.2452	.9695	.8824	.9175

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(cc) $x/D = 8.39$; $y/D = 3.0$; $\alpha = 0^\circ$;

$p_\infty = 221.63$ psf (10611.48 N/m^2);
$q_\infty = 397.15$ psf (19015.78 N/m^2);
$p_{t,\infty} = 942.00$ psf (45103.20 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2483	1.0163	.9023	.9321
.988	1.2526	1.0105	.8982	.9291
.936	1.2569	1.0181	.9000	.9304
.884	1.2601	1.0091	.8949	.9267
.832	1.2634	1.0152	.8964	.9278
.780	1.2418	1.0192	.9060	.9348
.728	1.2202	1.0248	.9165	.9424
.676	1.2331	1.0191	.9091	.9370
.624	1.2461	1.0134	.9018	.9317
.572	1.2483	1.0147	.9016	.9316
.520	1.2504	1.0143	.9006	.9309
.468	1.2450	1.0153	.9030	.9326
.416	1.2396	1.0179	.9062	.9349
.364	1.2450	1.0169	.9038	.9332
.312	1.2504	1.0159	.9014	.9314
.260	1.2439	1.0205	.9057	.9346
.208	1.2375	1.0150	.9056	.9345
.156	1.2504	1.0126	.8999	.9303
.104	1.2439	1.0121	.9020	.9319
.052	1.2418	1.0108	.9022	.9320
0.000	1.2504	1.0092	.8984	.9293
-.052	1.2483	1.0049	.8972	.9284
-.104	1.2461	1.0103	.9004	.9307
-.156	1.2461	1.0086	.8997	.9302
-.208	1.2461	1.0053	.8982	.9291
-.260	1.2396	1.0115	.9033	.9329
-.312	1.2331	1.0127	.9062	.9350
-.364	1.2299	1.0150	.9084	.9366
-.416	1.2267	1.0156	.9099	.9376
-.468	1.2299	1.0166	.9092	.9371
-.520	1.2331	1.0127	.9062	.9350
-.572	1.2331	1.0144	.9070	.9355
-.624	1.2331	1.0127	.9062	.9350
-.676	1.2310	1.0081	.9049	.9340
-.728	1.2288	1.0101	.9067	.9353
-.780	1.2277	1.0103	.9071	.9356
-.832	1.2267	1.0156	.9099	.9376
-.884	1.2267	1.0105	.9076	.9360
-.936	1.2267	1.0139	.9091	.9371
-.988	1.2191	1.0102	.9103	.9379
-1.040	1.2115	1.0116	.9138	.9404

(dd) $x/D = 8.39$; $y/D = 2.0$; $\alpha = 0^\circ$;

$p_\infty = 221.58$ psf (10609.23 N/m^2);
$q_\infty = 397.07$ psf (19011.74 N/m^2);
$p_{t,\infty} = 941.80$ psf (45093.63 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1429	1.0042	.9373	.9572
.988	1.1462	1.0019	.9350	.9555
.936	1.1494	1.0030	.9341	.9550
.884	1.1462	1.0019	.9350	.9555
.832	1.1429	.9992	.9350	.9556
.780	1.1257	1.0089	.9467	.9638
.728	1.1084	1.0137	.9563	.9705
.676	1.1224	.9995	.9437	.9617
.624	1.1365	.9986	.9374	.9573
.572	1.1397	.9997	.9366	.9567
.520	1.1429	.9958	.9334	.9545
.468	1.1408	1.0012	.9368	.9569
.416	1.1386	1.0033	.9387	.9582
.364	1.1375	1.0051	.9400	.9591
.312	1.1365	1.0003	.9382	.9578
.260	1.1354	1.0055	.9411	.9598
.208	1.1343	.9990	.9385	.9580
.156	1.1473	1.0034	.9352	.9557
.104	1.1462	.9969	.9326	.9539
.052	1.1483	1.0015	.9339	.9548
0.000	1.1581	.9881	.9237	.9475
-.052	1.1602	.9977	.9273	.9501
-.104	1.1624	.9940	.9247	.9483
-.156	1.1635	1.0005	.9273	.9501
-.208	1.1646	.9969	.9252	.9486
-.260	1.1602	1.0027	.9297	.9518
-.312	1.1559	1.0018	.9310	.9527
-.364	1.1527	1.0074	.9349	.9555
-.416	1.1494	1.0013	.9334	.9544
-.468	1.1505	1.0129	.9383	.9579
-.520	1.1516	1.0060	.9346	.9553
-.572	1.1537	1.0073	.9344	.9551
-.624	1.1559	.9952	.9279	.9505
-.676	1.1494	1.0030	.9341	.9550
-.728	1.1429	.9975	.9342	.9550
-.780	1.1419	1.0044	.9379	.9576
-.832	1.1408	.9979	.9353	.9558
-.884	1.1451	1.0004	.9347	.9554
-.936	1.1494	.9997	.9326	.9539
-.988	1.1494	1.0030	.9341	.9550
-1.040	1.1494	.9997	.9326	.9539

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(ee) x/D = 8.39; y/D = 1.5; $\alpha = 0^o$;

p_∞ = 221.58 psf (10609.23 N/m^2);
q_∞ = 397.07 psf (19011.74 N/m^2);
$p_{t,\infty}$ = 941.80 psf (45093.63 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1213	.9995	.9441	.9620
.988	1.1311	.9977	.9392	.9585
.936	1.1408	.9960	.9344	.9551
.884	1.1440	.9954	.9328	.9540
.832	1.1473	.9948	.9312	.9529
.780	1.1386	1.0031	.9386	.9581
.728	1.1300	1.0029	.9421	.9606
.676	1.1440	.9920	.9312	.9529
.624	1.1581	.9929	.9259	.9491
.572	1.1570	.9947	.9272	.9501
.520	1.1559	.9865	.9238	.9476
.468	1.1505	.9942	.9296	.9517
.416	1.1451	.9918	.9307	.9525
.364	1.1451	.9952	.9322	.9536
.312	1.1451	.9868	.9283	.9508
.260	1.1429	.9922	.9317	.9533
.208	1.1408	.9876	.9304	.9523
.156	1.1505	.9909	.9280	.9506
.104	1.1483	.9879	.9275	.9503
.052	1.1527	.9871	.9254	.9488
0.000	1.1559	.9782	.9199	.9448
-.052	1.1602	.9858	.9217	.9462
-.104	1.1646	.9816	.9181	.9435
-.156	1.1646	.9883	.9212	.9458
-.208	1.1646	.9816	.9181	.9435
-.260	1.1581	.9895	.9244	.9480
-.312	1.1516	.9907	.9275	.9503
-.364	1.1451	.9969	.9330	.9542
-.416	1.1386	.9930	.9339	.9548
-.468	1.1375	.9982	.9368	.9568
-.520	1.1365	.9934	.9349	.9555
-.572	1.1343	.9955	.9368	.9568
-.624	1.1321	.9858	.9331	.9543
-.676	1.1192	.9915	.9412	.9599
-.728	1.1062	.9904	.9462	.9635
-.780	1.1051	.9957	.9492	.9655
-.832	1.1041	.9908	.9473	.9642
-.884	1.1062	.9971	.9494	.9657
-.936	1.1084	.9901	.9451	.9627
-.988	1.1062	.9988	.9502	.9662
-1.040	1.1041	.9925	.9481	.9648

(ff) x/D = 8.39; y/D = 1.0; $\alpha = 0^o$;

p_∞ = 221.55 psf (10608.10 N/m^2);
q_∞ = 397.03 psf (19009.72 N/m^2);
$p_{t,\infty}$ = 941.70 psf (45088.84 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1866	.9878	.9124	.9394
.988	1.1898	.9805	.9078	.9361
.936	1.1930	.9849	.9086	.9367
.884	1.1930	.9765	.9047	.9339
.832	1.1930	.9782	.9055	.9344
.780	1.1693	.9809	.9159	.9420
.728	1.1455	.9835	.9266	.9496
.676	1.1628	.9703	.9135	.9402
.624	1.1801	.9587	.9014	.9314
.572	1.1768	.9560	.9013	.9314
.520	1.1736	.9465	.8980	.9290
.468	1.1628	.9417	.8999	.9304
.416	1.1520	.9336	.9003	.9306
.364	1.1574	.9293	.8961	.9275
.312	1.1628	.9165	.8878	.9215
.260	1.1639	.9096	.8840	.9187
.208	1.1649	.8942	.8761	.9128
.156	1.1779	.8833	.8660	.9051
.104	1.1790	.8814	.8646	.9041
.052	1.1736	.8892	.8704	.9085
0.000	1.1930	.8838	.8607	.9012
-.052	1.1876	.8827	.8621	.9022
-.104	1.1822	.8888	.8671	.9060
-.156	1.1952	.8982	.8669	.9058
-.208	1.2082	.9042	.8651	.9045
-.260	1.2071	.9162	.8712	.9091
-.312	1.2060	.9300	.8781	.9143
-.364	1.2093	.9310	.8775	.9138
-.416	1.2125	.9490	.8847	.9192
-.468	1.2244	.9451	.8786	.9146
-.520	1.2363	.9615	.8819	.9171
-.572	1.2373	.9663	.8837	.9184
-.624	1.2384	.9712	.8856	.9198
-.676	1.2428	.9687	.8829	.9178
-.728	1.2471	.9746	.8840	.9187
-.780	1.2428	.9754	.8859	.9201
-.832	1.2384	.9830	.8909	.9238
-.884	1.2428	.9822	.8890	.9224
-.936	1.2471	.9848	.8886	.9221
-.988	1.2449	.9852	.8896	.9228
-1.040	1.2428	.9906	.8928	.9252

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(gg) $x/D = 8.39$; $y/D = 0.83$; $\alpha = 0^\circ$;

p_∞ = 221.41 psf (10601.35 N/m^2);
q_∞ = 396.77 psf (18997.61 N/m^2);
$p_{t,\infty}$ = 941.10 psf (45060.11 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1798	.9845	.9135	.9402
.988	1.1809	.9776	.9099	.9376
.936	1.1820	.9791	.9101	.9378
.884	1.1830	.9738	.9073	.9357
.832	1.1841	.9703	.9052	.9342
.780	1.1614	.9727	.9152	.9414
.728	1.1387	.9735	.9246	.9482
.676	1.1549	.9554	.9095	.9374
.624	1.1711	.9440	.8978	.9288
.572	1.1690	.9343	.8940	.9260
.520	1.1668	.9145	.8853	.9196
.468	1.1560	.9046	.8846	.9191
.416	1.1452	.8999	.8864	.9205
.364	1.1528	.8647	.8661	.9052
.312	1.1603	.8598	.8608	.9013
.260	1.1625	.8391	.8496	.8927
.208	1.1647	.8353	.8469	.8906
.156	1.1776	.8175	.8332	.8800
.104	1.1798	.8051	.8261	.8744
.052	1.1776	.8089	.8288	.8766
0.000	1.1949	.7953	.8158	.8663
-.052	1.1928	.8123	.8253	.8738
-.104	1.1906	.8264	.8332	.8800
-.156	1.2122	.8171	.8210	.8704
-.208	1.2338	.8283	.8193	.8691
-.260	1.2273	.8518	.8331	.8799
-.312	1.2208	.8582	.8384	.8841
-.364	1.2219	.8785	.8479	.8914
-.416	1.2230	.9158	.8653	.9047
-.468	1.2295	.9197	.8649	.9043
-.520	1.2360	.9269	.8660	.9052
-.572	1.2327	.9411	.8738	.9110
-.624	1.2295	.9621	.8846	.9191
-.676	1.2360	.9592	.8810	.9164
-.728	1.2425	.9699	.8835	.9183
-.780	1.2349	.9713	.8869	.9208
-.832	1.2273	.9795	.8933	.9255
-.884	1.2306	.9755	.8903	.9233
-.936	1.2338	.9817	.8920	.9245
-.988	1.2317	.9838	.8937	.9258
-1.040	1.2295	.9875	.8962	.9277

(hh) $x/D = 8.39$; $y/D = 0.63$; $\alpha = 0^\circ$;

p_∞ = 221.39 psf (10600.22 N/m^2);
q_∞ = 396.73 psf (18995.59 N/m^2);
$p_{t,\infty}$ = 941.00 psf (45055.32 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1713	.9748	.9123	.9393
.988	1.1702	.9683	.9096	.9374
.936	1.1691	.9685	.9102	.9378
.884	1.1670	.9621	.9080	.9363
.832	1.1648	.9609	.9082	.9364
.780	1.1464	.9625	.9163	.9422
.728	1.1281	.9575	.9213	.9458
.676	1.1464	.9373	.9042	.9335
.624	1.1648	.9171	.8873	.9211
.572	1.1648	.9069	.8824	.9175
.520	1.1648	.8833	.8708	.9088
.468	1.1551	.8513	.8585	.8995
.416	1.1453	.8379	.8553	.8971
.364	1.1540	.8244	.8452	.8893
.312	1.1626	.7989	.8289	.8767
.260	1.1670	.7810	.8181	.8681
.208	1.1713	.7596	.8053	.8580
.156	1.1853	.7379	.7890	.8448
.104	1.1896	.7336	.7853	.8418
.052	1.1799	.7338	.7886	.8445
0.000	1.2080	.7212	.7726	.8315
-.052	1.1983	.7264	.7786	.8364
-.104	1.1886	.7440	.7912	.8466
-.156	1.2069	.7385	.7822	.8393
-.208	1.2253	.7589	.7870	.8432
-.260	1.2113	.7876	.8064	.8588
-.312	1.1972	.8075	.8213	.8707
-.364	1.2015	.8255	.8289	.8766
-.416	1.2059	.8605	.8447	.8890
-.468	1.2167	.8737	.8474	.8910
-.520	1.2275	.8955	.8541	.8962
-.572	1.2253	.8993	.8567	.8981
-.624	1.2231	.9439	.8784	.9145
-.676	1.2275	.9498	.8797	.9154
-.728	1.2318	.9541	.8801	.9157
-.780	1.2210	.9578	.8857	.9199
-.832	1.2102	.9716	.8960	.9275
-.884	1.2123	.9679	.8935	.9257
-.936	1.2145	.9759	.8964	.9278
-.988	1.2134	.9761	.8969	.9282
-1.040	1.2123	.9780	.8982	.9291

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(ii) $x/D = 8.39$; $y/D = 0.42$; $\alpha = 0^\circ$;

$p_\infty = 221.37$ psf (10599.09 N/m^2);
$q_\infty = 396.69$ psf (18993.57 N/m^2);
$p_{t,\infty} = 940.90$ psf (45050.53 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1687	.9687	.9104	.9380
.988	1.1687	.9636	.9080	.9363
.936	1.1687	.9636	.9080	.9363
.884	1.1665	.9556	.9051	.9341
.832	1.1644	.9526	.9045	.9337
.780	1.1428	.9515	.9125	.9395
.728	1.1212	.9471	.9191	.9442
.676	1.1417	.9332	.9041	.9334
.624	1.1622	.9109	.8853	.9196
.572	1.1633	.8972	.8782	.9143
.520	1.1644	.8683	.8635	.9033
.468	1.1557	.8513	.8582	.8993
.416	1.1471	.8292	.8502	.8932
.364	1.1601	.8114	.8363	.8824
.312	1.1730	.7679	.8091	.8610
.260	1.1773	.7654	.8063	.8588
.208	1.1817	.7387	.7907	.8462
.156	1.1903	.7266	.7813	.8386
.104	1.1946	.7240	.7785	.8363
.052	1.1827	.7179	.7791	.8367
0.000	1.2076	.7127	.7682	.8278
-.052	1.1957	.7139	.7727	.8315
-.104	1.1838	.7267	.7835	.8403
-.156	1.2022	.7281	.7782	.8361
-.208	1.2205	.7330	.7749	.8333
-.260	1.2076	.7632	.7950	.8497
-.312	1.1946	.7796	.8078	.8600
-.364	1.1989	.8113	.8226	.8717
-.416	1.2033	.8224	.8267	.8749
-.468	1.2162	.8523	.8371	.8830
-.520	1.2292	.8566	.8348	.8812
-.572	1.2292	.9059	.8585	.8995
-.624	1.2292	.9212	.8657	.9049
-.676	1.2313	.9225	.8656	.9048
-.728	1.2335	.9272	.8670	.9059
-.780	1.2205	.9415	.8783	.9144
-.832	1.2076	.9320	.8785	.9146
-.884	1.2076	.9574	.8904	.9234
-.936	1.2076	.9625	.8928	.9251
-.988	1.2097	.9604	.8910	.9238
-1.040	1.2119	.9634	.8916	.9243

(jj) $x/D = 8.39$; $y/D = 0.21$; $\alpha = 0^\circ$;

$p_\infty = 221.39$ psf (10600.22 N/m^2);
$q_\infty = 396.73$ psf (18995.59 N/m^2);
$p_{t,\infty} = 941.00$ psf (45055.32 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1434	.9665	.9194	.9445
.988	1.1521	.9582	.9120	.9391
.936	1.1607	.9567	.9078	.9361
.884	1.1597	.9501	.9052	.9342
.832	1.1586	.9486	.9049	.9340
.780	1.1402	.9503	.9129	.9398
.728	1.1218	.9469	.9187	.9440
.676	1.1434	.9329	.9033	.9328
.624	1.1651	.9104	.8840	.9186
.572	1.1694	.9028	.8787	.9147
.520	1.1737	.8851	.8684	.9070
.468	1.1694	.8741	.8646	.9041
.416	1.1651	.8512	.8548	.8966
.364	1.1802	.8279	.8376	.8834
.312	1.1953	.8079	.8221	.8713
.260	1.1953	.7926	.8143	.8651
.208	1.1953	.7789	.8072	.8595
.156	1.2018	.7621	.7963	.8508
.104	1.2018	.7484	.7891	.8449
.052	1.1899	.7422	.7898	.8455
0.000	1.2083	.7367	.7809	.8382
-.052	1.1964	.7379	.7853	.8419
-.104	1.1845	.7472	.7942	.8491
-.156	1.2061	.7566	.7920	.8473
-.208	1.2277	.7660	.7899	.8456
-.260	1.2169	.7906	.8060	.8585
-.312	1.2061	.7996	.8142	.8651
-.364	1.2094	.8246	.8257	.8742
-.416	1.2126	.8530	.8387	.8843
-.468	1.2245	.8711	.8434	.8880
-.520	1.2364	.8893	.8481	.8915
-.572	1.2310	.9056	.8577	.8989
-.624	1.2256	.9253	.8689	.9073
-.676	1.2267	.9301	.8708	.9088
-.728	1.2277	.9384	.8743	.9114
-.780	1.2180	.9419	.8794	.9152
-.832	1.2083	.9522	.8877	.9214
-.884	1.2040	.9530	.8897	.9229
-.936	1.1996	.9555	.8924	.9249
-.988	1.1953	.9546	.8936	.9258
-1.040	1.1910	.9621	.8988	.9296

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Concluded

(kk) $x/D = 8.39$; $y/D = 0.0$; $\alpha = 0°$;

$p_\infty = 221.39$ psf (10600.22 N/m^2);
$q_\infty = 396.73$ psf (18995.59 N/m^2);
$p_{t,\infty} = 941.00$ psf (45055.32 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1413	.9652	.9196	.9446
.988	1.1456	.9561	.9135	.9403
.936	1.1499	.9569	.9122	.9393
.884	1.1467	.9475	.9090	.9370
.832	1.1434	.9464	.9097	.9375
.780	1.1229	.9484	.9190	.9442
.728	1.1024	.9471	.9269	.9498
.676	1.1272	.9342	.9104	.9380
.624	1.1521	.9212	.8942	.9262
.572	1.1607	.9112	.8860	.9201
.520	1.1694	.9028	.8787	.9147
.468	1.1661	.8950	.8761	.9127
.416	1.1629	.8922	.8759	.9126
.364	1.1813	.8600	.8532	.8955
.312	1.1996	.8514	.8424	.8872
.260	1.1996	.8361	.8348	.8813
.208	1.1996	.8105	.8220	.8712
.156	1.2040	.7926	.8114	.8628
.104	1.2040	.7772	.8034	.8565
.052	1.1921	.7572	.7970	.8513
0.000	1.2083	.7471	.7863	.8427
-.052	1.1964	.7506	.7921	.8473
-.104	1.1845	.7667	.8045	.8574
-.156	1.2105	.7684	.7967	.8511
-.208	1.2364	.7907	.7997	.8535
-.260	1.2245	.8119	.8143	.8651
-.312	1.2126	.8364	.8305	.8779
-.364	1.2148	.8428	.8330	.8798
-.416	1.2169	.8713	.8462	.8901
-.468	1.2277	.8812	.8472	.8908
-.520	1.2386	.8995	.8522	.8947
-.572	1.2342	.9071	.8573	.8986
-.624	1.2299	.9113	.8608	.9012
-.676	1.2299	.9198	.8648	.9042
-.728	1.2299	.9282	.8688	.9072
-.780	1.2191	.9303	.8735	.9108
-.832	1.2083	.9255	.8752	.9121
-.884	1.2061	.9445	.8849	.9193
-.936	1.2040	.9517	.8891	.9224
-.988	1.1996	.9508	.8903	.9233
-1.040	1.1953	.9499	.8915	.9242

(ll) $x/D = 8.39$; $y/D = -0.42$; $\alpha = 0°$;

$p_\infty = 221.37$ psf (10599.09 N/m^2);
$q_\infty = 396.69$ psf (18993.57 N/m^2);
$p_{t,\infty} = 940.90$ psf (45050.53 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1414	.9722	.9229	.9470
.988	1.1468	.9661	.9179	.9434
.936	1.1522	.9668	.9160	.9421
.884	1.1501	.9622	.9147	.9411
.832	1.1479	.9626	.9157	.9418
.780	1.1317	.9655	.9237	.9475
.728	1.1155	.9617	.9285	.9510
.676	1.1446	.9481	.9101	.9378
.624	1.1738	.9343	.8921	.9247
.572	1.1911	.9294	.8833	.9181
.520	1.2084	.9228	.8739	.9111
.468	1.2041	.9236	.8758	.9125
.416	1.1998	.9210	.8762	.9128
.364	1.2138	.9099	.8658	.9050
.312	1.2279	.8988	.8556	.8972
.260	1.2225	.8896	.8531	.8953
.208	1.2171	.8754	.8481	.8915
.156	1.2181	.8446	.8327	.8796
.104	1.2127	.8064	.8154	.8661
.052	1.2030	.7758	.8031	.8562
0.000	1.2084	.7524	.7891	.8449
-.052	1.1987	.7594	.7960	.8505
-.104	1.1890	.7872	.8137	.8646
-.156	1.2160	.8110	.8167	.8670
-.208	1.2430	.8399	.8220	.8713
-.260	1.2279	.8583	.8361	.8822
-.312	1.2127	.8833	.8534	.8956
-.364	1.2117	.8954	.8597	.9004
-.416	1.2106	.9092	.8666	.9057
-.468	1.2225	.9155	.8654	.9047
-.520	1.2344	.9166	.8617	.9019
-.572	1.2300	.9259	.8676	.9064
-.624	1.2257	.9386	.8751	.9120
-.676	1.2279	.9382	.8741	.9113
-.728	1.2300	.9480	.8779	.9141
-.780	1.2203	.9498	.8822	.9173
-.832	1.2106	.9516	.8866	.9206
-.884	1.2052	.9560	.8906	.9236
-.936	1.1998	.9553	.8923	.9248
-.988	1.1922	.9533	.8942	.9262
-1.040	1.1846	.9682	.9041	.9334

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0.0$; $\alpha = 0^\circ$;

p_∞ = 101.29 psf (4849.95 N/m^2);
q_∞ = 375.09 psf (17959.36 N/m^2);
$p_{t,\infty}$ = 1266.60 psf (60645.13 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8178	.7250	.9415	.9703
.988	.7492	.6987	.9657	.9829
.936	.6807	.6759	.9964	.9983
.884	.6453	.6506	1.0041	1.0020
.832	.6098	.6322	1.0182	1.0087
.780	.5838	.6115	1.0234	1.0112
.728	.5578	.5942	1.0321	1.0152
.676	.5294	.5736	1.0409	1.0192
.624	.5011	.5582	1.0555	1.0258
.572	.4585	.5474	1.0926	1.0419
.520	.4160	.5383	1.1375	1.0602
.468	.4302	.5285	1.1085	1.0485
.416	.4443	.3248	.8549	.9210
.364	.4585	.1153	.5015	.6393
.312	.4727	.0378	.2830	.3898
.260	.4751	.0091	.1387	.1970
.208	.4774	.0023	.0697	.0997
.156	.4869	0.0000	0.0000	0.0000
.104	.4963	0.0000	0.0000	0.0000
.052	.4822	0.0000	0.0000	0.0000
0.000	.4680	0.0000	0.0000	0.0000
-.104	.4774	0.0000	0.0000	0.0000
-.156	.4774	0.0000	0.0000	0.0000
-.208	.4774	0.0000	0.0000	0.0000
-.260	.4774	0.0000	0.0000	0.0000
-.312	.4774	.0056	.1083	.1544
-.364	.4656	.0638	.3701	.4962
-.416	.4774	.2786	.7639	.8617
-.468	.4656	.5073	1.0438	1.0206
-.520	.4538	.5257	1.0763	1.0350
-.572	.4585	.5393	1.0845	1.0385
-.624	.4633	.5547	1.0942	1.0426
-.676	.5058	.5690	1.0607	1.0281
-.728	.5483	.5886	1.0361	1.0170
-.780	.5791	.6073	1.0241	1.0115
-.832	.6098	.6260	1.0132	1.0063
-.884	.6358	.6503	1.0113	1.0055
-.936	.6618	.6763	1.0109	1.0053
-.988	.7256	.6960	.9794	.9898
-1.040	.7894	.7227	.9568	.9783

(b) $x/D = 1.5$; $y/D = 0.0$; $\alpha = 0^\circ$;

p_∞ = 101.34 psf (4852.25 N/m^2);
q_∞ = 375.27 psf (17967.87 N/m^2);
$p_{t,\infty}$ = 1267.20 psf (60673.86 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6993	.6872	.9913	.9957
.988	.6497	.6681	1.0141	1.0068
.936	.6001	.6526	1.0429	1.0202
.884	.5717	.6355	1.0543	1.0253
.832	.5434	.6236	1.0713	1.0328
.780	.5268	.6074	1.0737	1.0339
.728	.5103	.5981	1.0826	1.0377
.676	.4985	.5885	1.0865	1.0394
.624	.4867	.5859	1.0972	1.0439
.572	.5032	.5899	1.0827	1.0377
.520	.5197	.6026	1.0768	1.0352
.468	.5953	.6372	1.0346	1.0164
.416	.6709	.6491	.9836	.9919
.364	.6946	.5072	.8546	.9208
.312	.7182	.2578	.5992	.7318
.260	.7300	.0840	.3393	.4595
.208	.7418	.0230	.1760	.2484
.156	.7465	.0002	.0175	.0251
.104	.7513	0.0000	0.0000	0.0000
.052	.7418	0.0000	0.0000	0.0000
0.000	.7324	.0009	.0341	.0489
-.104	.7371	0.0000	0.0000	0.0000
-.156	.7347	0.0000	0.0000	0.0000
-.208	.7324	.0042	.0762	.1089
-.260	.7111	.0528	.2724	.3762
-.312	.7087	.1597	.4746	.6119
-.364	.6379	.3928	.7847	.8760
-.416	.6851	.6383	.9652	.9826
-.468	.6142	.6138	.9997	.9998
-.520	.5434	.5876	1.0399	1.0188
-.572	.4961	.5789	1.0802	1.0367
-.624	.4489	.5806	1.1373	1.0601
-.676	.4748	.5822	1.1073	1.0480
-.728	.5008	.5908	1.0861	1.0392
-.780	.5245	.6013	1.0707	1.0326
-.832	.5481	.6153	1.0595	1.0276
-.884	.5552	.6305	1.0657	1.0303
-.936	.5623	.6509	1.0760	1.0348
-.988	.6071	.6651	1.0466	1.0219
-1.040	.6520	.6863	1.0259	1.0123

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(c) x/D = 2.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 101.41 psf (4855.31 N/m^2);
q_∞ = 375.50 psf (17979.21 N/m^2);
$p_{t,\infty}$ = 1268.00 psf (60712.17 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6233	.6731	1.0392	1.0185
.988	.5808	.6588	1.0651	1.0301
.936	.5383	.6462	1.0957	1.0432
.884	.5194	.6319	1.1030	1.0463
.832	.5005	.6228	1.1155	1.0514
.780	.5572	.6396	1.0714	1.0329
.728	.6138	.6861	1.0572	1.0266
.676	.6563	.6829	1.0200	1.0096
.624	.6988	.6815	.9875	.9939
.572	.7390	.6820	.9607	.9803
.520	.7791	.6964	.9455	.9723
.468	.8594	.7183	.9143	.9555
.416	.9397	.7332	.8833	.9379
.364	.9940	.7448	.8656	.9274
.312	1.0483	.7318	.8355	.9090
.260	1.0766	.5678	.7262	.8347
.208	1.1049	.3532	.5654	.7011
.156	1.1191	.1830	.4044	.5356
.104	1.1333	.1234	.3300	.4482
.052	1.1238	.1442	.3582	.4822
0.000	1.1144	.1707	.3914	.5208
-.104	1.1191	.1216	.3296	.4479
-.156	1.1167	.1388	.3526	.4755
-.208	1.1144	.2696	.4919	.6296
-.260	1.0247	.5039	.7012	.8159
-.312	1.0223	.6908	.8221	.9005
-.364	.9515	.7419	.8831	.9377
-.416	.9302	.7243	.8824	.9373
-.468	.8594	.7104	.9092	.9527
-.520	.7886	.6826	.9304	.9643
-.572	.7295	.6765	.9630	.9815
-.624	.6705	.6792	1.0064	1.0031
-.676	.6587	.6783	1.0148	1.0071
-.728	.6469	.6704	1.0180	1.0086
-.780	.5832	.6018	1.0158	1.0076
-.832	.5194	.6135	1.0868	1.0395
-.884	.5076	.6248	1.1094	1.0489
-.936	.4958	.6414	1.1374	1.0602
-.988	.5312	.6528	1.1085	1.0486
-1.040	.5666	.6676	1.0855	1.0389

(d) x/D = 2.5; y/D = 3.0; $\alpha = 0^\circ$;

p_∞ = 101.30 psf (4850.33 N/m^2);
q_∞ = 375.12 psf (17960.78 N/m^2);
$p_{t,\infty}$ = 1266.70 psf (60649.92 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0259	1.0011	.9878	.9940
.988	1.0685	1.0311	.9824	.9913
.936	1.1110	1.1589	1.0213	1.0102
.884	1.2387	1.2315	.9971	.9986
.832	1.3663	1.2219	.9457	.9725
.780	1.3994	1.2177	.9328	.9656
.728	1.4325	1.2117	.9197	.9585
.676	1.4609	1.2060	.9086	.9523
.624	1.4893	1.2038	.8991	.9469
.572	1.5129	1.1985	.8901	.9418
.520	1.5365	1.1967	.8825	.9374
.468	1.5507	1.1939	.8774	.9344
.416	1.5649	1.1893	.8718	.9311
.364	1.5295	1.1955	.8841	.9383
.312	1.4940	1.1982	.8956	.9449
.260	1.4751	1.1944	.8999	.9474
.208	1.4562	1.1941	.9056	.9506
.156	1.4964	1.1910	.8922	.9430
.104	1.5365	1.1862	.8786	.9351
.052	1.5176	1.1894	.8853	.9390
0.000	1.4987	1.1909	.8914	.9426
-.104	1.4940	1.1860	.8910	.9423
-.156	1.5011	1.1872	.8893	.9414
-.208	1.5082	1.1866	.8870	.9400
-.260	1.4420	1.1934	.9097	.9529
-.312	1.4491	1.1964	.9086	.9523
-.364	1.4231	1.1984	.9177	.9573
-.416	1.3900	1.2044	.9309	.9645
-.468	1.3640	1.2099	.9418	.9704
-.520	1.3380	1.2136	.9524	.9760
-.572	1.3829	1.2102	.9355	.9670
-.624	1.4278	1.2068	.9193	.9583
-.676	1.3309	1.2141	.9551	.9774
-.728	1.2340	1.1864	.9806	.9904
-.780	1.1323	1.1294	.9987	.9994
-.832	1.0307	1.0112	.9905	.9954
-.884	1.0023	.9941	.9959	.9980
-.936	.9739	.9945	1.0105	1.0051
-.988	.9810	.9940	1.0066	1.0032
-1.040	.9881	.9934	1.0027	1.0013

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(e) $x/D = 2.5$; $y/D = 2.0$; $\alpha = 0^\circ$;

p_∞ = 101.47 psf (4858.37 N/m^2);
q_∞ = 375.74 psf (17990.56 N/m^2);
$p_{t,\infty}$ = 1268.80 psf (60750.47 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1246	1.0193	.9520	.9758
.988	1.0868	1.0152	.9665	.9833
.936	1.0490	1.0128	.9826	.9914
.884	1.0396	1.0065	.9840	.9921
.832	1.0301	1.0037	.9871	.9937
.780	1.0207	.9974	.9886	.9944
.728	1.0112	.9894	.9892	.9947
.676	.9994	.9868	.9937	.9969
.624	.9876	.9807	.9965	.9983
.572	.9876	.9772	.9947	.9974
.520	.9876	.9737	.9930	.9966
.468	.9781	.9727	.9972	.9986
.416	.9687	.9681	.9997	.9999
.364	.9640	.9650	1.0005	1.0003
.312	.9592	.9619	1.0014	1.0007
.260	.9569	.9603	1.0018	1.0009
.208	.9545	.9605	1.0031	1.0015
.156	.9521	.9589	1.0035	1.0017
.104	.9498	.9573	1.0040	1.0019
.052	.9521	.9554	1.0017	1.0008
0.000	.9545	.9552	1.0004	1.0002
-.104	.9403	.9504	1.0054	1.0026
-.156	.9474	.9534	1.0032	1.0015
-.208	.9545	.9546	1.0001	1.0000
-.260	.9450	.9553	1.0054	1.0026
-.312	.9521	.9583	1.0032	1.0016
-.364	.9616	.9593	.9988	.9994
-.416	.9498	.9672	1.0091	1.0044
-.468	.9592	.9700	1.0056	1.0027
-.520	.9687	.9745	1.0030	1.0015
-.572	.9805	.9754	.9974	.9987
-.624	.9923	.9815	.9945	.9973
-.676	1.0088	.9855	.9884	.9943
-.728	1.0254	.9895	.9824	.9913
-.780	1.0254	.9965	.9858	.9930
-.832	1.0254	1.0000	.9876	.9939
-.884	1.0466	1.0072	.9810	.9906
-.936	1.0679	1.0143	.9746	.9874
-.988	1.0868	1.0181	.9679	.9840
-1.040	1.1057	1.0237	.9622	.9811

(f) $x/D = 2.5$; $y/D = 1.5$; $\alpha = 0^\circ$;

p_∞ = 101.42 psf (4856.08 N/m^2);
q_∞ = 375.56 psf (17982.05 N/m^2);
$p_{t,\infty}$ = 1268.20 psf (60721.74 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8980	.9005	1.0014	1.0007
.988	.8626	.8910	1.0163	1.0078
.936	.8271	.8849	1.0343	1.0162
.884	.8129	.8772	1.0388	1.0183
.832	.7988	.8730	1.0454	1.0213
.780	.7964	.8644	1.0418	1.0197
.728	.7940	.8559	1.0382	1.0180
.676	.7775	.8484	1.0446	1.0209
.624	.7609	.8444	1.0534	1.0249
.572	.7491	.8383	1.0578	1.0269
.520	.7373	.8339	1.0635	1.0294
.468	.7231	.8297	1.0712	1.0327
.416	.7090	.8238	1.0779	1.0357
.364	.7090	.8185	1.0745	1.0342
.312	.7090	.8168	1.0734	1.0337
.260	.7090	.8133	1.0711	1.0327
.208	.7090	.8116	1.0699	1.0322
.156	.7042	.8102	1.0726	1.0334
.104	.6995	.8070	1.0741	1.0340
.052	.7019	.8034	1.0699	1.0322
0.000	.7042	.8049	1.0691	1.0319
-.104	.6995	.8035	1.0718	1.0330
-.156	.7137	.8042	1.0615	1.0285
-.208	.7279	.8049	1.0516	1.0241
-.260	.7184	.8074	1.0601	1.0279
-.312	.7326	.8098	1.0514	1.0240
-.364	.7373	.8112	1.0489	1.0229
-.416	.7373	.8182	1.0534	1.0249
-.468	.7420	.8248	1.0543	1.0253
-.520	.7468	.8280	1.0530	1.0247
-.572	.7515	.8329	1.0527	1.0246
-.624	.7562	.8412	1.0547	1.0255
-.676	.7657	.8458	1.0510	1.0238
-.728	.7751	.8538	1.0495	1.0232
-.780	.7869	.8599	1.0453	1.0213
-.832	.7988	.8660	1.0412	1.0194
-.884	.8129	.8754	1.0377	1.0178
-.936	.8271	.8849	1.0343	1.0162
-.988	.8460	.8904	1.0259	1.0123
-1.040	.8649	.8978	1.0188	1.0090

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(g) $x/D = 2.5$; $y/D = 1.0$; $\alpha = 0^\circ$;

p_∞ = 101.30 psf (4850.33 N/m^2);
q_∞ = 375.12 psf (17960.78 N/m^2);
$p_{t,\infty}$ = 1266.70 psf (60649.92 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7186	.7979	1.0537	1.0250
.988	.6903	.7773	1.0612	1.0284
.936	.6619	.7689	1.0778	1.0356
.884	.6453	.7596	1.0849	1.0387
.832	.6288	.7503	1.0924	1.0418
.780	.6312	.7397	1.0826	1.0377
.728	.6335	.7290	1.0727	1.0334
.676	.6217	.7212	1.0770	1.0353
.624	.6099	.7133	1.0815	1.0372
.572	.5910	.7060	1.0930	1.0421
.520	.5721	.7004	1.1065	1.0477
.468	.5532	.6948	1.1207	1.0535
.416	.5342	.6891	1.1358	1.0595
.364	.5366	.6855	1.1302	1.0573
.312	.5390	.6905	1.1319	1.0580
.260	.5413	.6764	1.1178	1.0524
.208	.5437	.6727	1.1124	1.0501
.156	.5413	.6712	1.1135	1.0506
.104	.5390	.6696	1.1146	1.0511
.052	.5437	.6623	1.1037	1.0466
0.000	.5484	.6794	1.1130	1.0504
-.104	.5484	.6759	1.1101	1.0492
-.156	.5602	.6611	1.0862	1.0392
-.208	.5721	.6724	1.0842	1.0384
-.260	.5673	.6693	1.0861	1.0392
-.312	.5792	.6719	1.0771	1.0353
-.364	.5839	.6733	1.0738	1.0339
-.416	.5863	.6801	1.0771	1.0353
-.468	.5910	.6867	1.0780	1.0357
-.520	.5957	.6916	1.0775	1.0355
-.572	.5981	.6967	1.0793	1.0363
-.624	.6004	.7053	1.0838	1.0382
-.676	.6052	.7154	1.0873	1.0397
-.728	.6099	.7220	1.0881	1.0400
-.780	.6193	.7318	1.0870	1.0396
-.832	.6288	.7416	1.0860	1.0391
-.884	.6359	.7551	1.0897	1.0407
-.936	.6430	.7650	1.0908	1.0412
-.988	.6619	.7724	1.0802	1.0367
-1.040	.6808	.7832	1.0726	1.0334

(h) $x/D = 2.5$; $y/D = 0.83$; $\alpha = 0^\circ$;

p_∞ = 101.30 psf (4850.33 N/m^2);
q_∞ = 375.12 psf (17960.78 N/m^2);
$p_{t,\infty}$ = 1266.70 psf (60649.92 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6808	.7710	1.0642	1.0297
.988	.6501	.7453	1.0707	1.0326
.936	.6193	.7388	1.0922	1.0418
.884	.6052	.7276	1.0965	1.0436
.832	.5910	.7164	1.1010	1.0455
.780	.5933	.7058	1.0906	1.0411
.728	.5957	.6951	1.0802	1.0367
.676	.5886	.6869	1.0803	1.0367
.624	.5815	.6805	1.0817	1.0373
.572	.5650	.6747	1.0928	1.0420
.520	.5484	.6689	1.1044	1.0469
.468	.5272	.6652	1.1233	1.0546
.416	.5059	.6598	1.1420	1.0620
.364	.5130	.6575	1.1322	1.0581
.312	.5201	.6588	1.1255	1.0554
.260	.5272	.6547	1.1145	1.0510
.208	.5342	.6507	1.1036	1.0466
.156	.5390	.6504	1.0985	1.0444
.104	.5437	.6623	1.1037	1.0466
.052	.5508	.6460	1.0830	1.0379
0.000	.5579	.6595	1.0872	1.0397
-.104	.5484	.6497	1.0884	1.0402
-.156	.5579	.6403	1.0713	1.0328
-.208	.5673	.6570	1.0762	1.0349
-.260	.5532	.6476	1.0820	1.0374
-.312	.5626	.6469	1.0723	1.0332
-.364	.5673	.6466	1.0675	1.0312
-.416	.5579	.6507	1.0800	1.0366
-.468	.5626	.6556	1.0795	1.0364
-.520	.5673	.6588	1.0776	1.0355
-.572	.5673	.6675	1.0847	1.0386
-.624	.5673	.6728	1.0889	1.0404
-.676	.5721	.6811	1.0912	1.0413
-.728	.5768	.6895	1.0934	1.0423
-.780	.5863	.6976	1.0908	1.0412
-.832	.5957	.7074	1.0897	1.0407
-.884	.5957	.7196	1.0991	1.0446
-.936	.5957	.7318	1.1084	1.0485
-.988	.6170	.7425	1.0970	1.0438
-1.040	.6383	.7531	1.0863	1.0393

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(i) $x/D = 2.5$; $y/D = 0.63$; $\alpha = 0^o$;

p_∞ = 101.38 psf (4854.16 N/m^2);
q_∞ = 375.41 psf (17974.96 N/m^2);
$p_{t,\infty}$ = 1267.70 psf (60697.80 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6337	.7336	1.0759	1.0348
.988	.6054	.7130	1.0853	1.0388
.936	.5770	.7029	1.1037	1.0466
.884	.5604	.6919	1.1111	1.0496
.832	.5439	.6844	1.1218	1.0540
.780	.5486	.6736	1.1081	1.0484
.728	.5533	.6645	1.0959	1.0433
.676	.5557	.6573	1.0876	1.0398
.624	.5581	.6537	1.0823	1.0376
.572	.5888	.6514	1.0518	1.0242
.520	.6195	.6561	1.0291	1.0138
.468	.7520	.7336	.9877	.9940
.416	.8844	.7708	.9336	.9660
.364	.9246	.7800	.9185	.9578
.312	.9648	.7910	.9055	.9505
.260	.9790	.7829	.8943	.9442
.208	.9932	.7836	.8882	.9407
.156	1.0050	.7809	.8815	.9368
.104	1.0168	.7782	.8749	.9329
.052	1.0192	.7781	.8737	.9323
0.000	1.0215	.7779	.8726	.9316
-.104	1.0074	.7790	.8794	.9356
-.156	1.0097	.7753	.8763	.9338
-.208	1.0121	.7751	.8751	.9331
-.260	.9435	.7804	.9094	.9528
-.312	.9459	.7784	.9072	.9515
-.364	.7993	.7860	.9917	.9959
-.416	.8797	.7625	.9310	.9646
-.468	.7330	.7071	.9821	.9912
-.520	.5864	.6481	1.0513	1.0239
-.572	.5628	.6429	1.0688	1.0317
-.624	.5391	.6463	1.0949	1.0429
-.676	.5415	.6497	1.0953	1.0431
-.728	.5439	.6582	1.1001	1.0451
-.780	.5486	.6648	1.1009	1.0454
-.832	.5533	.6732	1.1030	1.0463
-.884	.5486	.6840	1.1166	1.0519
-.936	.5439	.6966	1.1317	1.0579
-.988	.5652	.7073	1.1187	1.0527
-1.040	.5864	.7179	1.1064	1.0477

(j) $x/D = 2.5$; $y/D = 0.42$; $\alpha = 0^o$;

p_∞ = 101.29 psf (4849.95 N/m^2);
q_∞ = 375.09 psf (17959.36 N/m^2);
$p_{t,\infty}$ = 1266.60 psf (60645.13 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6099	.7003	1.0715	1.0329
.988	.5839	.6883	1.0857	1.0390
.936	.5579	.6797	1.1037	1.0466
.884	.5437	.6703	1.1103	1.0493
.832	.5296	.6643	1.1200	1.0533
.780	.5390	.6566	1.1037	1.0466
.728	.5485	.6577	1.0951	1.0430
.676	.7400	.7762	1.0242	1.0115
.624	.9315	.7916	.9219	.9596
.572	.9787	.7880	.8973	.9459
.520	1.0260	.7826	.8733	.9320
.468	1.0449	.7794	.8636	.9263
.416	1.0638	.7779	.8551	.9211
.364	1.0638	.7761	.8541	.9205
.312	1.0638	.7761	.8541	.9205
.260	1.0662	.7725	.8512	.9187
.208	1.0686	.7705	.8492	.9175
.156	1.0804	.7678	.8430	.9137
.104	1.0922	.7617	.8351	.9088
.052	1.0922	.7599	.8341	.9082
0.000	1.0922	.7599	.8341	.9082
-.104	1.0828	.7616	.8387	.9110
-.156	1.0851	.7614	.8377	.9104
-.208	1.0875	.7647	.8386	.9109
-.260	1.0615	.7668	.8499	.9179
-.312	1.0638	.7683	.8498	.9179
-.364	1.0473	.7714	.8582	.9230
-.416	1.0402	.7719	.8614	.9249
-.468	1.0237	.7749	.8701	.9301
-.520	1.0071	.7762	.8779	.9347
-.572	.9716	.7772	.8944	.9442
-.624	.9362	.7799	.9127	.9546
-.676	.7471	.6769	.9519	.9757
-.728	.5579	.6421	1.0728	1.0334
-.780	.5532	.6442	1.0791	1.0362
-.832	.5485	.6515	1.0899	1.0408
-.884	.5319	.6597	1.1136	1.0507
-.936	.5154	.6731	1.1428	1.0623
-.988	.5390	.6819	1.1247	1.0551
-1.040	.5627	.6941	1.1107	1.0495

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(k) $x/D = 2.5$; $y/D = 0.21$; $\alpha = 0^\circ$;

p_∞ = 101.40 psf (4854.93 N/m^2);
q_∞ = 375.47 psf (17977.79 N/m^2);
$p_{t,\infty}$ = 1267.90 psf (60707.38 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6045	.6816	1.0619	1.0287
.988	.5738	.6734	1.0833	1.0380
.936	.5431	.6651	1.1067	1.0478
.884	.5879	.6549	1.0554	1.0258
.832	.6328	.7301	1.0741	1.0340
.780	.7626	.7694	1.0044	1.0021
.728	.8925	.7579	.9215	.9594
.676	.9256	.7623	.9076	.9517
.624	.9586	.7651	.8934	.9437
.572	.9964	.7674	.8776	.9345
.520	1.0342	.7663	.8608	.9245
.468	1.0578	.7662	.8511	.9187
.416	1.0814	.7643	.8407	.9123
.364	1.0790	.7610	.8398	.9117
.312	1.0767	.7577	.8389	.9111
.260	1.0743	.7123	.8142	.8955
.208	1.0720	.6422	.7740	.8687
.156	1.0838	.5319	.7006	.8154
.104	1.0956	.4278	.6249	.7541
.052	1.0932	.3724	.5837	.7179
0.000	1.0908	.3473	.5642	.7001
-.104	1.0814	.4058	.6126	.7435
-.156	1.0861	.4856	.6687	.7904
-.208	1.0908	.6090	.7472	.8499
-.260	1.0696	.6933	.8051	.8896
-.312	1.0743	.7368	.8282	.9044
-.364	1.0554	.7558	.8463	.9157
-.416	1.0578	.7609	.8481	.9169
-.468	1.0389	.7624	.8566	.9220
-.520	1.0200	.7603	.8634	.9261
-.572	.9870	.7576	.8762	.9337
-.624	.9539	.7549	.8896	.9415
-.676	.9232	.7503	.9015	.9483
-.728	.8925	.7509	.9172	.9571
-.780	.7508	.7633	1.0082	1.0040
-.832	.6092	.6603	1.0411	1.0194
-.884	.5525	.6453	1.0807	1.0369
-.936	.4958	.6599	1.1536	1.0665
-.988	.5194	.6669	1.1330	1.0585
-1.040	.5431	.6773	1.1168	1.0520

(l) $x/D = 2.5$; $y/D = 0.0$; $\alpha = 0^\circ$;

p_∞ = 101.24 psf (4847.27 N/m^2);
q_∞ = 374.88 psf (17949.44 N/m^2);
$p_{t,\infty}$ = 1265.90 psf (60611.62 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7106	.7510	1.0280	1.0133
.988	.6987	.7361	1.0264	1.0126
.936	.6869	.7196	1.0235	1.0112
.884	.6774	.7063	1.0211	1.0101
.832	.6679	.7035	1.0263	1.0125
.780	.7106	.7073	.9977	.9989
.728	.7532	.7251	.9812	.9907
.676	.8456	.7549	.9448	.9720
.624	.9380	.7706	.9064	.9511
.572	1.0019	.7745	.8792	.9355
.520	1.0659	.7713	.8507	.9184
.468	1.0872	.7696	.8414	.9127
.416	1.1085	.7645	.8304	.9058
.364	1.0967	.7531	.8287	.9047
.312	1.0848	.7242	.8170	.8973
.260	1.0730	.6073	.7523	.8535
.208	1.0611	.4792	.6720	.7930
.156	1.0682	.3497	.5722	.7074
.104	1.0753	.3034	.5312	.6687
.052	1.0682	.3096	.5384	.6756
0.000	1.0611	.3213	.5503	.6870
-.104	1.0564	.2984	.5315	.6690
-.156	1.0682	.3119	.5404	.6776
-.208	1.0801	.4140	.6191	.7491
-.260	1.0706	.5694	.7293	.8369
-.312	1.0824	.6919	.7995	.8859
-.364	1.0635	.7461	.8376	.9103
-.416	1.0848	.7585	.8362	.9094
-.468	1.0659	.7617	.8454	.9151
-.520	1.0469	.7632	.8538	.9203
-.572	.9877	.7642	.8796	.9357
-.624	.9285	.7530	.9005	.9478
-.676	.8337	.7357	.9393	.9691
-.728	.7390	.7060	.9774	.9888
-.780	.7153	.6973	.9873	.9938
-.832	.6916	.6921	1.0003	1.0002
-.884	.6798	.7017	1.0160	1.0077
-.936	.6679	.7183	1.0370	1.0175
-.988	.6395	.7379	1.0742	1.0341
-1.040	.6111	.7155	1.0821	1.0375

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(m) x/D = 2.5; y/D = -0.42; $\alpha = 0^\circ$;

p_∞ = 101.28 psf (4849.18 N/m^2);
q_∞ = 375.03 psf (17956.53 N/m^2);
$p_{t,\infty}$ = 1266.40 psf (60635.56 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7100	.7175	1.0053	1.0026
.988	.6437	.6963	1.0400	1.0189
.936	.5774	.6784	1.0839	1.0383
.884	.5609	.6605	1.0852	1.0388
.832	.5443	.6495	1.0923	1.0418
.780	.5277	.6402	1.1014	1.0456
.728	.5112	.6309	1.1110	1.0496
.676	.4899	.6150	1.1205	1.0534
.624	.4686	.5939	1.1258	1.0556
.572	.7029	.6079	.9300	.9641
.520	.9372	.7528	.8963	.9453
.468	.9679	.7435	.8764	.9338
.416	.9987	.7341	.8574	.9225
.364	1.0034	.7250	.8500	.9180
.312	1.0082	.7316	.8519	.9191
.260	1.0176	.7361	.8505	.9183
.208	1.0271	.7354	.8462	.9156
.156	1.0366	.7276	.8378	.9105
.104	1.0460	.7322	.8366	.9097
.052	1.0507	.7178	.8265	.9033
0.000	1.0555	.6383	.7777	.8712
-.104	1.0413	.7369	.8413	.9126
-.156	1.0437	.7227	.8322	.9069
-.208	1.0460	.7296	.8351	.9088
-.260	1.0129	.7321	.8502	.9181
-.312	1.0153	.7214	.8430	.9137
-.364	.9466	.7232	.8741	.9325
-.416	.9845	.7291	.8606	.9244
-.468	.9159	.7414	.8997	.9473
-.520	.8472	.7343	.9310	.9646
-.572	.6366	.5629	.9403	.9696
-.624	.4260	.5960	1.1828	1.0774
-.676	.4709	.6154	1.1431	1.0624
-.728	.5159	.6278	1.1032	1.0463
-.780	.5325	.6319	1.0893	1.0406
-.832	.5490	.6446	1.0836	1.0381
-.884	.5514	.6584	1.0928	1.0420
-.936	.5538	.6810	1.1089	1.0487
-.988	.6058	.6981	1.0735	1.0338
-1.040	.6579	.7222	1.0478	1.0224

(n) x/D = 3.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 101.34 psf (4852.25 N/m^2);
q_∞ = 375.27 psf (17967.87 N/m^2);
$p_{t,\infty}$ = 1267.20 psf (60673.86 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7237	.7396	1.0109	1.0053
.988	.7521	.7427	.9938	.9970
.936	.7805	.7878	1.0047	1.0023
.884	.8916	.8319	.9659	.9830
.832	1.0028	.8235	.9062	.9510
.780	1.0170	.8137	.8945	.9443
.728	1.0312	.8003	.8810	.9365
.676	1.0264	.7884	.8764	.9339
.624	1.0217	.7800	.8738	.9323
.572	1.0241	.7711	.8677	.9287
.520	1.0264	.7639	.8627	.9257
.468	1.0264	.7551	.8577	.9227
.416	1.0264	.7428	.8507	.9184
.364	1.0170	.7208	.8419	.9130
.312	1.0075	.6882	.8265	.9033
.260	1.0028	.5919	.7683	.8647
.208	.9981	.5005	.7082	.8212
.156	1.0052	.4183	.6451	.7711
.104	1.0122	.3819	.6143	.7450
.052	1.0099	.3750	.6094	.7407
0.000	1.0075	.3788	.6132	.7440
-.104	.9981	.3748	.6128	.7437
-.156	1.0052	.3849	.6188	.7489
-.208	1.0122	.4521	.6683	.7901
-.260	1.0052	.5607	.7469	.8497
-.312	1.0122	.6517	.8024	.8878
-.364	1.0170	.7094	.8352	.9088
-.416	1.0122	.7361	.8528	.9197
-.468	1.0170	.7463	.8566	.9220
-.520	1.0217	.7582	.8614	.9249
-.572	1.0217	.7652	.8654	.9273
-.624	1.0217	.7740	.8704	.9303
-.676	1.0264	.7841	.8740	.9324
-.728	1.0312	.7943	.8777	.9346
-.780	1.0146	.8043	.8904	.9420
-.832	.9981	.8109	.9014	.9482
-.884	.8727	.8099	.9633	.9817
-.936	.7474	.7597	1.0082	1.0040
-.988	.7095	.7398	1.0211	1.0101
-1.040	.6717	.7391	1.0490	1.0229

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(o) $x/D = 4.0$; $y/D = 0.0$; $\alpha = 0^\circ$;

p_∞ = 101.29 psf (4849.95 N/m^2);
q_∞ = 375.09 psf (17959.36 N/m^2);
$p_{t,\infty}$ = 1266.60 psf (60645.13 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0369	.8852	.9240	.9608
.988	1.0321	.8680	.9171	.9570
.936	1.0274	.8579	.9138	.9552
.884	1.0298	.8402	.9033	.9493
.832	1.0321	.8295	.8965	.9455
.780	1.0321	.8155	.8889	.9411
.728	1.0321	.8015	.8812	.9367
.676	1.0250	.7881	.8768	.9341
.624	1.0179	.7781	.8743	.9326
.572	1.0156	.7713	.8715	.9309
.520	1.0132	.7609	.8666	.9280
.468	1.0132	.7469	.8586	.9232
.416	1.0132	.7277	.8475	.9164
.364	1.0014	.6953	.8333	.9076
.312	.9895	.6576	.8152	.8961
.260	.9848	.5912	.7748	.8692
.208	.9801	.5352	.7390	.8440
.156	.9848	.4854	.7021	.8165
.104	.9895	.4585	.6807	.7999
.052	.9943	.4439	.6682	.7899
0.000	.9990	.4399	.6636	.7863
-.104	.9895	.4484	.6732	.7940
-.156	.9895	.4644	.6851	.8034
-.208	.9895	.5086	.7170	.8278
-.260	.9895	.5634	.7545	.8551
-.312	.9895	.6215	.7925	.8812
-.364	.9943	.6756	.8243	.9020
-.416	.9895	.7181	.8519	.9192
-.468	.9943	.7370	.8610	.9247
-.520	.9990	.7507	.8669	.9282
-.572	1.0037	.7626	.8717	.9310
-.624	1.0085	.7710	.8744	.9327
-.676	1.0132	.7812	.8781	.9348
-.728	1.0179	.7931	.8827	.9375
-.780	1.0156	.8055	.8906	.9421
-.832	1.0132	.8145	.8966	.9455
-.884	1.0132	.8250	.9024	.9488
-.936	1.0132	.8390	.9100	.9531
-.988	1.0014	.8469	.9197	.9584
-1.040	.9895	.8531	.9285	.9633

(p) $x/D = 5.0$; $y/D = 3.0$; $\alpha = 0^\circ$;

p_∞ = 101.29 psf (4849.95 N/m^2);
q_∞ = 375.09 psf (17959.36 N/m^2);
$p_{t,\infty}$ = 1266.60 psf (60645.13 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9888	.9785	.9948	.9975
.988	.9652	.9785	1.0069	1.0033
.936	.9415	.9786	1.0195	1.0093
.884	.9368	.9772	1.0213	1.0102
.832	.9321	.9775	1.0241	1.0115
.780	.9321	.9775	1.0241	1.0115
.728	.9321	.9740	1.0223	1.0106
.676	.9273	.9726	1.0241	1.0115
.624	.9226	.9712	1.0260	1.0124
.572	.9226	.9695	1.0251	1.0120
.520	.9226	.9695	1.0251	1.0120
.468	.9131	.9667	1.0289	1.0137
.416	.9037	.9657	1.0337	1.0160
.364	.9037	.9639	1.0328	1.0155
.312	.9037	.9622	1.0319	1.0151
.260	.9013	.9606	1.0324	1.0153
.208	.8989	.9608	1.0338	1.0160
.156	.8989	.9590	1.0329	1.0156
.104	.8989	.9573	1.0319	1.0151
.052	.9013	.9571	1.0305	1.0145
0.000	.9037	.9569	1.0291	1.0138
-.104	.8942	.9529	1.0323	1.0153
-.156	.9060	.9521	1.0251	1.0120
-.208	.9179	.9512	1.0180	1.0086
-.260	.8989	.9543	1.0303	1.0144
-.312	.9108	.9535	1.0232	1.0111
-.364	.9108	.9535	1.0232	1.0111
-.416	.9037	.9540	1.0275	1.0131
-.468	.9037	.9575	1.0293	1.0139
-.520	.9037	.9592	1.0303	1.0144
-.572	.9084	.9589	1.0274	1.0130
-.624	.9131	.9585	1.0246	1.0117
-.676	.9155	.9601	1.0241	1.0115
-.728	.9179	.9617	1.0236	1.0113
-.780	.9179	.9617	1.0236	1.0113
-.832	.9179	.9634	1.0245	1.0117
-.884	.9250	.9664	1.0221	1.0106
-.936	.9321	.9711	1.0207	1.0099
-.988	.9439	.9702	1.0139	1.0067
-1.040	.9557	.9711	1.0080	1.0039

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(q) $x/D = 5.0$; $y/D = 2.0$; $\alpha = 0°$;

p_∞ = 101.31 psf (4850.71 N/m^2);
q_∞ = 375.15 psf (17962.20 N/m^2);
$p_{t,\infty}$ = 1266.80 psf (60654.71 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7572	.8790	1.0774	1.0355
.988	.7407	.8645	1.0804	1.0367
.936	.7241	.8640	1.0923	1.0418
.884	.7146	.8629	1.0989	1.0446
.832	.7052	.8636	1.1066	1.0478
.780	.7146	.8594	1.0966	1.0436
.728	.7241	.8552	1.0868	1.0395
.676	.7146	.8542	1.0933	1.0422
.624	.7052	.8531	1.0999	1.0450
.572	.7028	.8516	1.1007	1.0453
.520	.7004	.8482	1.1005	1.0452
.468	.6862	.8493	1.1125	1.0502
.416	.6720	.8486	1.1237	1.0547
.364	.6744	.8449	1.1193	1.0530
.312	.6768	.8447	1.1172	1.0521
.260	.6815	.8426	1.1119	1.0500
.208	.6862	.8423	1.1079	1.0483
.156	.6815	.8409	1.1108	1.0495
.104	.6768	.8412	1.1149	1.0512
.052	.6791	.8358	1.1094	1.0489
0.000	.6815	.8391	1.1096	1.0490
-.104	.6815	.8339	1.1062	1.0476
-.156	.6981	.8327	1.0922	1.0418
-.208	.7146	.8332	1.0798	1.0365
-.260	.6957	.8346	1.0953	1.0431
-.312	.7123	.8351	1.0828	1.0378
-.364	.7099	.8353	1.0847	1.0386
-.416	.7099	.8371	1.0859	1.0391
-.468	.7075	.8372	1.0878	1.0399
-.520	.7052	.8392	1.0909	1.0412
-.572	.7028	.8393	1.0928	1.0420
-.624	.7004	.8395	1.0948	1.0428
-.676	.6957	.8433	1.1010	1.0455
-.728	.6910	.8454	1.1061	1.0476
-.780	.6933	.8453	1.1041	1.0468
-.832	.6957	.8486	1.1044	1.0469
-.884	.7004	.8482	1.1005	1.0452
-.936	.7052	.8514	1.0988	1.0445
-.988	.7123	.8526	1.0941	1.0426
-1.040	.7194	.8538	1.0895	1.0406

(r) $x/D = 5.0$; $y/D = 1.5$; $\alpha = 0°$;

p_∞ = 101.36 psf (4853.01 N/m^2);
q_∞ = 375.33 psf (17970.70 N/m^2);
$p_{t,\infty}$ = 1267.40 psf (60683.44 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9304	.9968	1.0350	1.0166
.988	.9753	.9882	1.0066	1.0032
.936	1.0202	.9849	.9825	.9914
.884	1.0225	.9829	.9804	.9904
.832	1.0249	.9828	.9792	.9897
.780	1.0249	.9793	.9775	.9889
.728	1.0249	.9758	.9757	.9880
.676	1.0225	.9724	.9752	.9877
.624	1.0202	.9709	.9755	.9879
.572	1.0249	.9670	.9714	.9858
.520	1.0296	.9649	.9681	.9841
.468	1.0225	.9637	.9708	.9855
.416	1.0155	.9625	.9736	.9869
.364	1.0131	.9592	.9730	.9866
.312	1.0107	.9558	.9725	.9863
.260	1.0036	.9529	.9744	.9873
.208	.9966	.9499	.9763	.9883
.156	1.0013	.9478	.9729	.9866
.104	1.0060	.9474	.9705	.9853
.052	1.0084	.9473	.9692	.9847
0.000	1.0107	.9471	.9680	.9841
-.104	.9966	.9429	.9727	.9865
-.156	1.0036	.9424	.9690	.9846
-.208	1.0107	.9453	.9671	.9836
-.260	.9966	.9464	.9745	.9874
-.312	1.0036	.9494	.9726	.9864
-.364	1.0013	.9496	.9738	.9870
-.416	.9966	.9517	.9772	.9887
-.468	.9942	.9536	.9794	.9898
-.520	.9918	.9538	.9806	.9904
-.572	.9942	.9536	.9794	.9898
-.624	.9966	.9552	.9790	.9896
-.676	1.0013	.9565	.9774	.9888
-.728	1.0060	.9632	.9785	.9894
-.780	1.0013	.9635	.9810	.9906
-.832	.9966	.9639	.9835	.9919
-.884	1.0013	.9653	.9819	.9911
-.936	1.0060	.9684	.9811	.9907
-.988	.9422	.9749	1.0172	1.0082
-1.040	.8785	.9552	1.0428	1.0201

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(s) x/D = 5.0; y/D = 1.0; $\alpha = 0^\circ$;

p_∞ = 101.19 psf (4844.97 N/m^2);
q_∞ = 374.70 psf (17940.93 N/m^2);
$p_{t,\infty}$ = 1265.30 psf (60582.89 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0467	.9379	.9466	.9730
.988	1.0230	.9310	.9540	.9768
.936	.9993	.9293	.9643	.9822
.884	.9970	.9207	.9610	.9805
.832	.9946	.9156	.9595	.9797
.780	.9946	.9086	.9558	.9778
.728	.9946	.9034	.9530	.9763
.676	.9946	.8964	.9493	.9744
.624	.9946	.8911	.9466	.9729
.572	.9970	.8857	.9425	.9708
.520	.9993	.8803	.9385	.9687
.468	.9970	.8752	.9369	.9678
.416	.9946	.8684	.9344	.9665
.364	.9922	.8615	.9318	.9651
.312	.9899	.8565	.9302	.9642
.260	.9875	.8531	.9295	.9638
.208	.9851	.8516	.9298	.9639
.156	.9875	.8461	.9257	.9617
.104	.9899	.8442	.9235	.9605
.052	.9922	.8423	.9213	.9594
0.000	.9946	.8421	.9202	.9587
-.104	.9804	.8407	.9260	.9619
-.156	.9851	.8403	.9236	.9606
-.208	.9899	.8452	.9241	.9609
-.260	.9780	.8479	.9311	.9647
-.312	.9827	.8493	.9296	.9639
-.364	.9804	.8512	.9318	.9651
-.416	.9756	.8586	.9381	.9684
-.468	.9733	.8640	.9422	.9706
-.520	.9709	.8712	.9473	.9733
-.572	.9733	.8745	.9479	.9736
-.624	.9756	.8796	.9495	.9745
-.676	.9756	.8849	.9523	.9760
-.728	.9756	.8901	.9552	.9774
-.780	.9733	.8956	.9592	.9796
-.832	.9709	.9010	.9633	.9817
-.884	.9733	.9061	.9649	.9825
-.936	.9756	.9146	.9682	.9842
-.988	.9875	.9173	.9638	.9819
-1.040	.9993	.9234	.9612	.9806

(t) x/D = 5.0; y/D = 0.83; $\alpha = 0^\circ$;

p_∞ = 101.25 psf (4848.03 N/m^2);
q_∞ = 374.94 psf (17952.27 N/m^2);
$p_{t,\infty}$ = 1266.10 psf (60621.19 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0271	.9171	.9450	.9721
.988	1.0105	.9114	.9497	.9746
.936	.9940	.9074	.9555	.9776
.884	.9963	.9002	.9505	.9750
.832	.9987	.8948	.9465	.9729
.780	.9987	.8860	.9419	.9705
.728	.9987	.8773	.9372	.9680
.676	.9987	.8685	.9325	.9655
.624	.9987	.8597	.9278	.9629
.572	1.0034	.8524	.9217	.9595
.520	1.0082	.8450	.9155	.9562
.468	1.0034	.8384	.9141	.9553
.416	.9987	.8300	.9116	.9540
.364	.9963	.8249	.9099	.9530
.312	.9940	.8181	.9072	.9515
.260	.9892	.8114	.9057	.9507
.208	.9845	.8100	.9071	.9514
.156	.9869	.8046	.9029	.9491
.104	.9892	.8026	.9008	.9479
.052	.9916	.8007	.8986	.9467
0.000	.9940	.8005	.8974	.9460
-.104	.9798	.7981	.9025	.9489
-.156	.9869	.7993	.9000	.9474
-.208	.9940	.8023	.8984	.9466
-.260	.9774	.8070	.9087	.9524
-.312	.9845	.8100	.9071	.9514
-.364	.9845	.8135	.9090	.9525
-.416	.9750	.8177	.9158	.9563
-.468	.9750	.8248	.9197	.9585
-.520	.9750	.8318	.9236	.9606
-.572	.9774	.8386	.9263	.9621
-.624	.9798	.8472	.9299	.9640
-.676	.9798	.8524	.9328	.9656
-.728	.9798	.8629	.9385	.9686
-.780	.9750	.8703	.9448	.9720
-.832	.9703	.8759	.9501	.9748
-.884	.9703	.8829	.9539	.9768
-.936	.9703	.8899	.9577	.9788
-.988	.9774	.8964	.9577	.9787
-1.040	.9845	.9011	.9567	.9782

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(u) x/D = 5.0; y/D = 0.63; $\alpha = 0^\circ$;

p_∞ = 101.29 psf (4849.95 N/m^2);
q_∞ = 375.09 psf (17959.36 N/m^2);
$p_{t,\infty}$ = 1266.60 psf (60645.13 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0452	.9038	.9299	.9640
.988	1.0286	.8946	.9326	.9655
.936	1.0121	.8853	.9353	.9669
.884	1.0121	.8748	.9297	.9639
.832	1.0121	.8626	.9232	.9604
.780	1.0121	.8521	.9176	.9573
.728	1.0121	.8398	.9109	.9536
.676	1.0097	.8278	.9054	.9505
.624	1.0073	.8192	.9018	.9485
.572	1.0073	.8104	.8970	.9457
.520	1.0073	.8052	.8940	.9441
.468	1.0097	.7980	.8890	.9412
.416	1.0121	.7908	.8840	.9383
.364	1.0097	.7857	.8821	.9372
.312	1.0073	.7807	.8803	.9361
.260	1.0050	.7756	.8785	.9351
.208	1.0026	.7758	.8796	.9357
.156	1.0121	.7733	.8741	.9325
.104	1.0215	.7708	.8687	.9293
.052	1.0239	.7689	.8666	.9280
0.000	1.0263	.7687	.8655	.9274
-.104	1.0121	.7672	.8707	.9305
-.156	1.0121	.7672	.8707	.9305
-.208	1.0121	.7672	.8707	.9305
-.260	.9955	.7720	.8806	.9363
-.312	.9955	.7738	.8816	.9369
-.364	.9932	.7739	.8828	.9376
-.416	.9790	.7820	.8938	.9439
-.468	.9766	.7875	.8980	.9463
-.520	.9742	.7929	.9022	.9487
-.572	.9790	.7996	.9037	.9496
-.624	.9837	.8080	.9063	.9510
-.676	.9884	.8146	.9078	.9519
-.728	.9932	.8283	.9132	.9549
-.780	.9884	.8374	.9204	.9589
-.832	.9837	.8483	.9286	.9633
-.884	.9884	.8584	.9319	.9651
-.936	.9932	.8721	.9371	.9679
-.988	.9955	.8771	.9387	.9687
-1.040	.9979	.8857	.9421	.9706

(v) x/D = 5.0; y/D = 0.42; $\alpha = 0^\circ$;

p_∞ = 101.25 psf (4848.03 N/m^2);
q_∞ = 374.94 psf (17952.27 N/m^2);
$p_{t,\infty}$ = 1266.10 psf (60621.19 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0704	.8954	.9146	.9556
.988	1.0467	.8761	.9149	.9558
.936	1.0231	.8622	.9180	.9575
.884	1.0207	.8484	.9117	.9540
.832	1.0183	.8415	.9091	.9526
.780	1.0207	.8274	.9003	.9476
.728	1.0231	.8167	.8935	.9437
.676	1.0302	.8074	.8853	.9390
.624	1.0373	.8051	.8810	.9365
.572	1.0610	.7962	.8663	.9279
.520	1.0846	.7926	.8549	.9210
.468	1.1012	.7914	.8477	.9166
.416	1.1178	.7866	.8389	.9111
.364	1.1107	.7783	.8371	.9100
.312	1.1036	.7666	.8335	.9077
.260	1.0965	.7496	.8268	.9036
.208	1.0894	.7309	.8191	.8986
.156	1.0965	.7092	.8043	.8890
.104	1.1036	.6911	.7913	.8804
.052	1.1036	.6735	.7812	.8736
0.000	1.1036	.6700	.7792	.8722
-.104	1.0894	.6825	.7915	.8806
-.156	1.0846	.6970	.8016	.8873
-.208	1.0799	.7185	.8157	.8964
-.260	1.0681	.7317	.8277	.9041
-.312	1.0633	.7514	.8406	.9122
-.364	1.0444	.7651	.8559	.9216
-.416	1.0467	.7720	.8588	.9233
-.468	1.0278	.7787	.8704	.9303
-.520	1.0089	.7802	.8794	.9356
-.572	1.0041	.7805	.8817	.9369
-.624	.9994	.7844	.8859	.9394
-.676	.9946	.7918	.8922	.9430
-.728	.9899	.7974	.8975	.9461
-.780	.9875	.8064	.9036	.9495
-.832	.9852	.8171	.9107	.9535
-.884	.9899	.8307	.9161	.9565
-.936	.9946	.8461	.9223	.9599
-.988	1.0041	.8559	.9233	.9604
-1.040	1.0136	.8692	.9260	.9619

TABLE 2.- *VARIATION OF* p_1/p_∞, q_1/q_∞, M_1/M_∞, *AND* V_1/V_∞ *WITH* z/D *IN THE WAKE OF A* 140°*-INCLUDED-ANGLE CONE AT A* MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(w) $x/D = 5.0$; $y/D = 0.21$; $\alpha = 0^{\circ}$;

$p_\infty = 101.27$ psf (4848.80 N/m^2);
$q_\infty = 375.00$ psf (17955.11 N/m^2);
$p_{t,\infty} = 1266.30$ psf (60630.77 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1253	.9085	.8985	.9466
.988	1.1182	.9003	.8973	.9459
.936	1.1111	.8903	.8951	.9447
.884	1.1300	.8766	.8808	.9364
.832	1.1490	.8664	.8684	.9291
.780	1.1608	.8532	.8573	.9225
.728	1.1726	.8400	.8464	.9158
.676	1.1726	.8278	.8402	.9119
.624	1.1726	.8172	.8348	.9086
.572	1.1797	.8097	.8284	.9046
.520	1.1868	.7986	.8203	.8994
.468	1.1868	.7810	.8112	.8936
.416	1.1868	.7564	.7984	.8851
.364	1.1679	.7263	.7886	.8786
.312	1.1490	.6909	.7754	.8697
.260	1.1395	.6300	.7435	.8473
.208	1.1300	.5867	.7205	.8304
.156	1.1324	.5334	.6863	.8043
.104	1.1348	.4995	.6634	.7862
.052	1.1324	.4819	.6523	.7771
0.000	1.1300	.4714	.6459	.7718
-.104	1.1206	.4853	.6581	.7818
-.156	1.1206	.5085	.6736	.7943
-.208	1.1206	.5510	.7012	.8159
-.260	1.1182	.5972	.7308	.8380
-.312	1.1182	.6484	.7615	.8600
-.364	1.1182	.6942	.7879	.8781
-.416	1.1159	.7419	.8154	.8962
-.468	1.1159	.7682	.8297	.9054
-.520	1.1159	.7840	.8382	.9107
-.572	1.1206	.7960	.8428	.9136
-.624	1.1253	.8009	.8436	.9141
-.676	1.1135	.8053	.8504	.9183
-.728	1.1017	.8132	.8592	.9236
-.780	1.0757	.8240	.8752	.9332
-.832	1.0497	.8365	.8927	.9433
-.884	1.0402	.8390	.8981	.9464
-.936	1.0308	.8502	.9082	.9521
-.988	1.0260	.8488	.9096	.9528
-1.040	1.0213	.8667	.9212	.9593

(x) $x/D = 5.0$; $y/D = 0.0$; $\alpha = 0^{\circ}$;

$p_\infty = 101.28$ psf (4849.18 N/m^2);
$q_\infty = 375.03$ psf (17956.53 N/m^2);
$p_{t,\infty} = 1266.40$ psf (60635.56 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2069	.9231	.8745	.9327
.988	1.1927	.9101	.8735	.9321
.936	1.1785	.8971	.8725	.9315
.884	1.1809	.8811	.8638	.9264
.832	1.1833	.8704	.8577	.9227
.780	1.1880	.8524	.8471	.9162
.728	1.1927	.8397	.8391	.9113
.676	1.1856	.8262	.8348	.9086
.624	1.1785	.8162	.8322	.9070
.572	1.1785	.8057	.8268	.9035
.520	1.1785	.7933	.8205	.8995
.468	1.1809	.7755	.8104	.8930
.416	1.1833	.7489	.7956	.8832
.364	1.1691	.7165	.7829	.8747
.312	1.1549	.6806	.7677	.8643
.260	1.1454	.6301	.7417	.8459
.208	1.1359	.5937	.7229	.8322
.156	1.1383	.5616	.7024	.8168
.104	1.1407	.5401	.6881	.8057
.052	1.1430	.5221	.6758	.7961
0.000	1.1454	.5094	.6669	.7889
-.104	1.1359	.5249	.6797	.7992
-.156	1.1336	.5446	.6931	.8096
-.208	1.1312	.5696	.7096	.8222
-.260	1.1288	.6016	.7300	.8375
-.312	1.1265	.6441	.7562	.8563
-.364	1.1288	.6933	.7837	.8753
-.416	1.1217	.7361	.8100	.8928
-.468	1.1241	.7622	.8235	.9014
-.520	1.1265	.7814	.8329	.9074
-.572	1.1383	.7963	.8364	.9096
-.624	1.1501	.8041	.8361	.9094
-.676	1.1572	.8176	.8405	.9122
-.728	1.1643	.8294	.8440	.9143
-.780	1.1572	.8404	.8522	.9193
-.832	1.1501	.8533	.8613	.9249
-.884	1.1572	.8685	.8663	.9279
-.936	1.1643	.8820	.8703	.9303
-.988	1.1620	.8927	.8765	.9339
-1.040	1.1596	.9034	.8826	.9375

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(y) $x/D = 5.0$; $y/D = -0.42$; $\alpha = 0^o$;

$p_\infty = 101.31$ psf (4850.71 N/m^2);
$q_\infty = 375.15$ psf (17962.20 N/m^2);
$p_{t,\infty} = 1266.80$ psf (60654.71 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2294	.9398	.8743	.9326
.988	1.2034	.9278	.8780	.9348
.936	1.1774	.9122	.8802	.9361
.884	1.1727	.8951	.8737	.9322
.832	1.1680	.8814	.8687	.9293
.780	1.1656	.8641	.8610	.9247
.728	1.1632	.8449	.8523	.9194
.676	1.1561	.8262	.8453	.9151
.624	1.1490	.8127	.8410	.9125
.572	1.1538	.7965	.8309	.9061
.520	1.1585	.7804	.8207	.8997
.468	1.1656	.7622	.8087	.8919
.416	1.1727	.7546	.8022	.8876
.364	1.1538	.7737	.8189	.8985
.312	1.1349	.7752	.8265	.9033
.260	1.1278	.7687	.8256	.9028
.208	1.1207	.7640	.8257	.9028
.156	1.1254	.7548	.8190	.8986
.104	1.1301	.7457	.8123	.8942
.052	1.1325	.7191	.7969	.8841
0.000	1.1349	.6873	.7782	.8716
-.104	1.1254	.7373	.8094	.8924
-.156	1.1183	.7501	.8190	.8986
-.208	1.1112	.7577	.8258	.9029
-.260	1.1159	.7626	.8267	.9035
-.312	1.1088	.7684	.8325	.9071
-.364	1.1112	.7718	.8334	.9077
-.416	1.1065	.7493	.8229	.9011
-.468	1.1088	.7544	.8248	.9023
-.520	1.1112	.7718	.8334	.9077
-.572	1.1207	.7903	.8398	.9117
-.624	1.1301	.8036	.8433	.9139
-.676	1.1396	.8205	.8485	.9171
-.728	1.1490	.8355	.8527	.9197
-.780	1.1443	.8499	.8618	.9252
-.832	1.1396	.8661	.8718	.9311
-.884	1.1538	.8825	.8746	.9328
-.936	1.1680	.8954	.8756	.9334
-.988	1.1798	.9121	.8793	.9355
-1.040	1.1916	.9234	.8803	.9361

(z) $x/D = 6.0$; $y/D = 0.0$; $\alpha = 0^o$;

$p_\infty = 101.29$ psf (4849.57 N/m^2);
$q_\infty = 375.06$ psf (17957.94 N/m^2);
$p_{t,\infty} = 1266.50$ psf (60640.35 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1540	.8975	.8819	.9370
.988	1.1304	.8853	.8850	.9388
.936	1.1067	.8731	.8882	.9407
.884	1.1044	.8558	.8803	.9361
.832	1.1020	.8454	.8759	.9335
.780	1.1044	.8312	.8676	.9286
.728	1.1067	.8188	.8601	.9241
.676	1.0996	.8071	.8567	.9221
.624	1.0926	.8006	.8560	.9217
.572	1.0973	.7915	.8493	.9176
.520	1.1020	.7823	.8426	.9134
.468	1.1091	.7642	.8301	.9056
.416	1.1162	.7444	.8166	.8970
.364	1.1044	.7190	.8069	.8907
.312	1.0926	.6935	.7967	.8840
.260	1.0902	.6603	.7783	.8716
.208	1.0878	.6359	.7646	.8622
.156	1.0902	.6163	.7519	.8532
.104	1.0926	.5915	.7358	.8417
.052	1.1044	.5711	.7191	.8294
0.000	1.1162	.5524	.7035	.8176
-.104	1.1020	.5702	.7193	.8296
-.156	1.0949	.5920	.7353	.8413
-.208	1.0878	.6173	.7533	.8542
-.260	1.0878	.6367	.7650	.8625
-.312	1.0807	.6619	.7826	.8746
-.364	1.0831	.6899	.7981	.8849
-.416	1.0736	.7223	.8202	.8993
-.468	1.0760	.7467	.8330	.9075
-.520	1.0784	.7641	.8418	.9129
-.572	1.0831	.7777	.8474	.9164
-.624	1.0878	.7862	.8501	.9181
-.676	1.0949	.7961	.8527	.9197
-.728	1.1020	.8061	.8553	.9212
-.780	1.0973	.8188	.8638	.9264
-.832	1.0926	.8297	.8714	.9309
-.884	1.0996	.8449	.8765	.9339
-.936	1.1067	.8601	.8816	.9369
-.988	1.1186	.8715	.8827	.9375
-1.040	1.1304	.8881	.8864	.9397

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(aa) x/D = 7.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 101.34 psf (4852.25 N/m^2);
q_∞ = 375.27 psf (17967.87 N/m^2);
$p_{t,\infty}$ = 1267.20 psf (60673.86 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0683	.8738	.9044	.9499
.988	1.0447	.8581	.9063	.9510
.936	1.0210	.8459	.9102	.9532
.884	1.0187	.8321	.9038	.9496
.832	1.0163	.8235	.9001	.9475
.780	1.0210	.8091	.8902	.9419
.728	1.0258	.7965	.8812	.9366
.676	1.0210	.7881	.8786	.9351
.624	1.0163	.7780	.8749	.9330
.572	1.0187	.7690	.8689	.9294
.520	1.0210	.7583	.8618	.9252
.468	1.0234	.7477	.8547	.9209
.416	1.0258	.7317	.8446	.9147
.364	1.0210	.7145	.8365	.9097
.312	1.0163	.6974	.8284	.9045
.260	1.0140	.6712	.8136	.8951
.208	1.0116	.6504	.8018	.8874
.156	1.0163	.6272	.7855	.8765
.104	1.0210	.6057	.7702	.8661
.052	1.0305	.5820	.7515	.8530
0.000	1.0400	.5672	.7385	.8436
-.104	1.0258	.5779	.7506	.8523
-.156	1.0234	.6027	.7674	.8641
-.208	1.0210	.6258	.7829	.8747
-.260	1.0210	.6434	.7938	.8821
-.312	1.0187	.6576	.8035	.8885
-.364	1.0187	.6822	.8184	.8982
-.416	1.0163	.7088	.8351	.9088
-.468	1.0163	.7281	.8464	.9158
-.520	1.0163	.7439	.8555	.9214
-.572	1.0187	.7577	.8624	.9255
-.624	1.0210	.7680	.8673	.9285
-.676	1.0234	.7766	.8711	.9307
-.728	1.0258	.7887	.8769	.9341
-.780	1.0234	.7977	.8828	.9376
-.832	1.0210	.8066	.8888	.9411
-.884	1.0234	.8204	.8954	.9448
-.936	1.0258	.8325	.9009	.9480
-.988	1.0352	.8441	.9030	.9491
-1.040	1.0447	.8574	.9059	.9508

(bb) x/D = 8.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 101.37 psf (4853.40 N/m^2);
q_∞ = 375.36 psf (17972.12 N/m^2);
$p_{t,\infty}$ = 1267.50 psf (60688.23 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9965	.8602	.9291	.9636
.988	.9776	.8388	.9263	.9621
.936	.9587	.8298	.9303	.9643
.884	.9563	.8159	.9237	.9606
.832	.9540	.8056	.9189	.9580
.780	.9587	.7947	.9105	.9533
.728	.9634	.7821	.9010	.9480
.676	.9611	.7700	.8951	.9447
.624	.9587	.7614	.8912	.9424
.572	.9587	.7561	.8881	.9406
.520	.9587	.7438	.8808	.9364
.468	.9611	.7314	.8724	.9315
.416	.9634	.7154	.8617	.9251
.364	.9587	.7000	.8545	.9207
.312	.9540	.6828	.8460	.9155
.260	.9516	.6601	.8329	.9074
.208	.9493	.6445	.8240	.9017
.156	.9540	.6265	.8104	.8930
.104	.9587	.6086	.7967	.8840
.052	.9658	.5886	.7807	.8733
0.000	.9729	.5740	.7681	.8646
-.104	.9587	.5814	.7788	.8719
-.156	.9611	.5953	.7870	.8775
-.208	.9634	.6145	.7986	.8853
-.260	.9587	.6342	.8133	.8949
-.312	.9611	.6498	.8223	.9007
-.364	.9611	.6673	.8333	.9076
-.416	.9587	.6921	.8496	.9178
-.468	.9587	.7096	.8603	.9243
-.520	.9587	.7254	.8699	.9300
-.572	.9587	.7394	.8782	.9349
-.624	.9587	.7517	.8855	.9391
-.676	.9611	.7603	.8894	.9414
-.728	.9634	.7706	.8943	.9442
-.780	.9634	.7829	.9014	.9483
-.832	.9634	.7916	.9065	.9511
-.884	.9658	.8037	.9122	.9543
-.936	.9681	.8158	.9179	.9575
-.988	.9729	.8277	.9224	.9599
-1.040	.9776	.8396	.9267	.9623

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(cc) x/D = 8.39; y/D = 3.0; $\alpha = 0^\circ$;

p_∞ = 101.37 psf (4853.40 N/m^2);
q_∞ = 375.36 psf (17972.12 N/m^2);
$p_{t,\infty}$ = 1267.50 psf (60688.23 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0440	1.0013	.9794	.9898
.988	1.0203	1.0031	.9915	.9958
.936	.9967	1.0048	1.0041	1.0020
.884	.9967	1.0031	1.0032	1.0016
.832	.9967	1.0031	1.0032	1.0016
.780	.9944	1.0015	1.0036	1.0017
.728	.9920	1.0017	1.0049	1.0024
.676	.9920	1.0000	1.0040	1.0019
.624	.9920	1.0000	1.0040	1.0019
.572	.9991	1.0012	1.0011	1.0005
.520	1.0062	1.0007	.9973	.9987
.468	1.0014	1.0010	.9998	.9999
.416	.9967	1.0014	1.0023	1.0011
.364	.9991	1.0012	1.0011	1.0005
.312	1.0014	1.0010	.9998	.9999
.260	.9991	1.0012	1.0011	1.0005
.208	.9967	1.0031	1.0032	1.0016
.156	.9991	1.0029	1.0019	1.0009
.104	1.0014	1.0027	1.0007	1.0003
.052	1.0062	1.0024	.9981	.9991
0.000	1.0109	1.0038	.9965	.9983
-.104	.9967	.9996	1.0015	1.0007
-.156	1.0038	.9991	.9976	.9989
-.208	1.0109	.9986	.9939	.9970
-.260	.9944	1.0015	1.0036	1.0017
-.312	1.0014	.9993	.9989	.9995
-.364	.9991	.9994	1.0002	1.0001
-.416	.9920	1.0000	1.0040	1.0019
-.468	.9896	1.0001	1.0053	1.0026
-.520	.9873	1.0003	1.0066	1.0032
-.572	.9920	.9982	1.0031	1.0015
-.624	.9967	.9996	1.0015	1.0007
-.676	.9991	.9994	1.0002	1.0001
-.728	1.0014	.9993	.9989	.9995
-.780	.9991	.9994	1.0002	1.0001
-.832	.9967	.9996	1.0015	1.0007
-.884	1.0014	.9993	.9989	.9995
-.936	1.0062	1.0007	.9973	.9987
-.988	1.0132	1.0001	.9935	.9968
-1.040	1.0203	.9996	.9898	.9950

(dd) x/D = 8.39; y/D = 2.0; $\alpha = 0^\circ$;

p_∞ = 101.42 psf (4856.08 N/m^2);
q_∞ = 375.56 psf (17982.05 N/m^2);
$p_{t,\infty}$ = 1268.20 psf (60721.74 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1661	1.0387	.9438	.9715
.988	1.1449	1.0403	.9532	.9764
.936	1.1236	1.0384	.9613	.9806
.884	1.1213	1.0386	.9624	.9812
.832	1.1189	1.0387	.9635	.9818
.780	1.1142	1.0374	.9649	.9825
.728	1.1095	1.0360	.9663	.9832
.676	1.1118	1.0323	.9636	.9818
.624	1.1142	1.0304	.9617	.9808
.572	1.1189	1.0300	.9595	.9797
.520	1.1236	1.0297	.9573	.9785
.468	1.1213	1.0281	.9575	.9787
.416	1.1189	1.0265	.9578	.9788
.364	1.1166	1.0267	.9589	.9794
.312	1.1142	1.0269	.9600	.9800
.260	1.1118	1.0271	.9611	.9805
.208	1.1095	1.0272	.9622	.9811
.156	1.1142	1.0269	.9600	.9800
.104	1.1189	1.0265	.9578	.9788
.052	1.1213	1.0263	.9567	.9783
0.000	1.1236	1.0262	.9556	.9777
-.104	1.1095	1.0215	.9595	.9797
-.156	1.1047	1.0218	.9617	.9809
-.208	1.1000	1.0257	.9656	.9828
-.260	1.1000	1.0257	.9656	.9828
-.312	1.0953	1.0278	.9687	.9844
-.364	1.0953	1.0278	.9687	.9844
-.416	1.0906	1.0281	.9709	.9856
-.468	1.0906	1.0316	.9726	.9864
-.520	1.0906	1.0316	.9726	.9864
-.572	1.1024	1.0308	.9670	.9835
-.624	1.1142	1.0299	.9614	.9807
-.676	1.1213	1.0293	.9581	.9790
-.728	1.1284	1.0340	.9573	.9786
-.780	1.1189	1.0348	.9617	.9808
-.832	1.1095	1.0355	.9661	.9831
-.884	1.1213	1.0363	.9614	.9807
-.936	1.1331	1.0407	.9584	.9791
-.988	1.1449	1.0398	.9530	.9763
-1.040	1.1567	1.0389	.9477	.9735

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(ee) $x/D = 8.39$; $y/D = 1.5$; $\alpha = 0^\circ$;

p_∞ = 101.45 psf (4857.22 N/m^2);
q_∞ = 375.65 psf (17986.30 N/m^2);
$p_{t,\infty}$ = 1268.50 psf (60736.11 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1286	.9993	.9410	.9700
.988	1.1050	1.0011	.9518	.9757
.936	1.0814	.9994	.9613	.9806
.884	1.0790	.9961	.9608	.9804
.832	1.0767	.9945	.9611	.9805
.780	1.0767	.9928	.9603	.9801
.728	1.0767	.9875	.9577	.9788
.676	1.0767	.9840	.9560	.9779
.624	1.0767	.9823	.9552	.9774
.572	1.0814	.9785	.9512	.9754
.520	1.0861	.9781	.9490	.9742
.468	1.0837	.9765	.9492	.9743
.416	1.0814	.9750	.9495	.9745
.364	1.0814	.9715	.9478	.9736
.312	1.0814	.9715	.9478	.9736
.260	1.0790	.9682	.9472	.9733
.208	1.0767	.9683	.9484	.9739
.156	1.0790	.9682	.9472	.9733
.104	1.0814	.9662	.9453	.9722
.052	1.0861	.9659	.9430	.9711
0.000	1.0908	.9655	.9408	.9699
-.104	1.0767	.9590	.9438	.9715
-.156	1.0743	.9609	.9458	.9725
-.208	1.0719	.9611	.9469	.9731
-.260	1.0649	.9634	.9512	.9754
-.312	1.0625	.9671	.9540	.9769
-.364	1.0649	.9669	.9529	.9763
-.416	1.0531	.9695	.9595	.9797
-.468	1.0554	.9728	.9601	.9800
-.520	1.0578	.9762	.9606	.9803
-.572	1.0672	.9772	.9569	.9783
-.624	1.0767	.9782	.9532	.9764
-.676	1.0837	.9847	.9532	.9764
-.728	1.0908	.9859	.9507	.9751
-.780	1.0861	.9915	.9555	.9776
-.832	1.0814	.9936	.9586	.9792
-.884	1.0932	.9962	.9546	.9772
-.936	1.1050	.9988	.9507	.9751
-.988	1.1144	1.0016	.9480	.9737
-1.040	1.1239	1.0026	.9445	.9719

(ff) $x/D = 8.39$; $y/D = 1.0$; $\alpha = 0^\circ$;

p_∞ = 101.41 psf (4855.69 N/m^2);
q_∞ = 375.53 psf (17980.63 N/m^2);
$p_{t,\infty}$ = 1268.10 psf (60716.96 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0824	.9414	.9326	.9655
.988	1.0612	.9378	.9401	.9695
.936	1.0399	.9324	.9469	.9731
.884	1.0375	.9256	.9445	.9718
.832	1.0352	.9187	.9421	.9706
.780	1.0375	.9098	.9364	.9675
.728	1.0399	.8991	.9299	.9640
.676	1.0375	.8923	.9274	.9627
.624	1.0352	.8838	.9240	.9608
.572	1.0375	.8766	.9192	.9582
.520	1.0399	.8729	.9162	.9565
.468	1.0399	.8659	.9125	.9545
.416	1.0399	.8606	.9097	.9529
.364	1.0399	.8519	.9051	.9503
.312	1.0399	.8484	.9032	.9493
.260	1.0375	.8433	.9016	.9483
.208	1.0352	.8400	.9008	.9479
.156	1.0375	.8363	.8978	.9462
.104	1.0399	.8344	.8958	.9450
.052	1.0423	.8342	.8946	.9444
0.000	1.0446	.8305	.8917	.9427
-.104	1.0304	.8246	.8946	.9444
-.156	1.0328	.8297	.8963	.9454
-.208	1.0352	.8312	.8961	.9452
-.260	1.0257	.8337	.9016	.9483
-.312	1.0281	.8405	.9042	.9498
-.364	1.0281	.8423	.9051	.9504
-.416	1.0210	.8481	.9114	.9539
-.468	1.0210	.8551	.9152	.9560
-.520	1.0210	.8603	.9180	.9575
-.572	1.0281	.8668	.9182	.9576
-.624	1.0352	.8750	.9194	.9583
-.676	1.0375	.8836	.9228	.9602
-.728	1.0399	.8921	.9262	.9620
-.780	1.0352	.8995	.9322	.9653
-.832	1.0304	.9069	.9381	.9685
-.884	1.0399	.9131	.9371	.9679
-.936	1.0493	.9247	.9387	.9688
-.988	1.0588	.9275	.9359	.9673
-1.040	1.0682	.9372	.9367	.9677

TABLE 2.- *VARIATION OF* p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(gg) x/D = 8.39; y/D = 0.83; $\alpha = 0^{\circ}$;

p_∞ = 101.43 psf (4856.46 N/m^2);
q_∞ = 375.59 psf (17983.47 N/m^2);
$p_{t,\infty}$ = 1268.30 psf (60726.53 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0631	.9165	.9285	.9633
.988	1.0418	.9093	.9342	.9664
.936	1.0206	.9022	.9402	.9696
.884	1.0182	.8919	.9359	.9673
.832	1.0159	.8833	.9325	.9654
.780	1.0182	.8744	.9267	.9623
.728	1.0206	.8620	.9190	.9581
.676	1.0182	.8517	.9146	.9556
.624	1.0159	.8413	.9101	.9531
.572	1.0182	.8342	.9051	.9503
.520	1.0206	.8270	.9002	.9476
.468	1.0229	.8180	.8943	.9442
.416	1.0253	.8144	.8912	.9424
.364	1.0206	.8060	.8887	.9410
.312	1.0159	.8011	.8880	.9406
.260	1.0135	.7960	.8862	.9396
.208	1.0111	.7874	.8825	.9374
.156	1.0135	.7837	.8794	.9356
.104	1.0159	.7818	.8773	.9343
.052	1.0182	.7781	.8742	.9325
0.000	1.0206	.7744	.8711	.9307
-.104	1.0064	.7755	.8778	.9347
-.156	1.0111	.7734	.8746	.9328
-.208	1.0159	.7801	.8763	.9338
-.260	1.0040	.7845	.8839	.9382
-.312	1.0088	.7876	.8836	.9380
-.364	1.0111	.7927	.8854	.9391
-.416	1.0017	.8022	.8949	.9445
-.468	1.0040	.8090	.8976	.9461
-.520	1.0064	.8140	.8994	.9471
-.572	1.0111	.8224	.9019	.9485
-.624	1.0159	.8308	.9044	.9499
-.676	1.0182	.8412	.9089	.9525
-.728	1.0206	.8480	.9115	.9539
-.780	1.0182	.8569	.9174	.9572
-.832	1.0159	.8676	.9241	.9609
-.884	1.0229	.8775	.9262	.9620
-.936	1.0300	.8892	.9291	.9636
-.988	1.0371	.8992	.9311	.9647
-1.040	1.0442	.9074	.9322	.9653

(hh) x/D = 8.39; y/D = 0.63; $\alpha = 0^{\circ}$;

p_∞ = 101.47 psf (4858.37 N/m^2);
q_∞ = 375.74 psf (17990.56 N/m^2);
$p_{t,\infty}$ = 1268.80 psf (60750.47 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0396	.8906	.9256	.9617
.988	1.0183	.8765	.9277	.9629
.936	.9970	.8676	.9328	.9656
.884	.9947	.8555	.9274	.9627
.832	.9923	.8452	.9229	.9602
.780	.9947	.8311	.9141	.9554
.728	.9970	.8187	.9062	.9509
.676	.9947	.8101	.9025	.9489
.624	.9923	.8033	.8997	.9473
.572	.9970	.7942	.8925	.9432
.520	1.0018	.7868	.8863	.9396
.468	1.0041	.7779	.8802	.9361
.416	1.0065	.7655	.8721	.9313
.364	.9994	.7538	.8685	.9292
.312	.9923	.7473	.8678	.9288
.260	.9899	.7300	.8587	.9233
.208	.9876	.7162	.8516	.9190
.156	.9899	.7055	.8442	.9144
.104	.9923	.6948	.8368	.9098
.052	.9947	.6859	.8304	.9058
0.000	.9970	.6840	.8283	.9045
-.104	.9876	.6785	.8289	.9049
-.156	.9899	.6801	.8289	.9048
-.208	.9923	.6939	.8363	.9095
-.260	.9852	.7068	.8470	.9161
-.312	.9876	.7153	.8511	.9187
-.364	.9876	.7294	.8594	.9237
-.416	.9829	.7472	.8719	.9312
-.468	.9829	.7595	.8791	.9354
-.520	.9829	.7717	.8861	.9395
-.572	.9876	.7784	.8878	.9405
-.624	.9923	.7868	.8904	.9420
-.676	.9947	.7936	.8932	.9436
-.728	.9970	.8057	.8989	.9469
-.780	.9947	.8146	.9050	.9503
-.832	.9923	.8253	.9120	.9542
-.884	.9970	.8372	.9163	.9566
-.936	1.0018	.8508	.9216	.9595
-.988	1.0088	.8607	.9237	.9606
-1.040	1.0159	.8724	.9267	.9623

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(ii) x/D = 8.39; y/D = 0.42; $\alpha = 0^\circ$;

p_∞ = 101.44 psf (4856.84 N/m^2);
q_∞ = 375.62 psf (17984.88 N/m^2);
$p_{t,\infty}$ = 1268.40 psf (60731.32 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0111	.8721	.9287	.9634
.988	.9898	.8527	.9282	.9631
.936	.9685	.8403	.9315	.9649
.884	.9685	.8281	.9247	.9612
.832	.9685	.8159	.9178	.9574
.780	.9733	.8015	.9075	.9517
.728	.9780	.7907	.8992	.9470
.676	.9756	.7786	.8934	.9437
.624	.9733	.7701	.8895	.9415
.572	.9756	.7629	.8843	.9384
.520	.9780	.7522	.8770	.9342
.468	.9803	.7398	.8687	.9293
.416	.9827	.7238	.8582	.9230
.364	.9756	.6999	.8470	.9161
.312	.9685	.6864	.8419	.9130
.260	.9662	.6533	.8223	.9007
.208	.9638	.6360	.8123	.8943
.156	.9685	.6146	.7966	.8839
.104	.9733	.5966	.7830	.8748
.052	.9803	.5820	.7705	.8663
0.000	.9874	.5779	.7650	.8625
-.104	.9733	.5745	.7683	.8648
-.156	.9733	.5815	.7730	.8680
-.208	.9733	.5991	.7846	.8759
-.260	.9685	.6118	.7948	.8827
-.312	.9685	.6329	.8084	.8917
-.364	.9685	.6557	.8228	.9010
-.416	.9638	.6859	.8436	.9141
-.468	.9638	.7052	.8554	.9213
-.520	.9638	.7262	.8680	.9289
-.572	.9662	.7435	.8772	.9343
-.624	.9685	.7556	.8833	.9379
-.676	.9709	.7642	.8872	.9401
-.728	.9733	.7745	.8921	.9429
-.780	.9709	.7834	.8983	.9465
-.832	.9685	.7924	.9045	.9500
-.884	.9709	.8044	.9102	.9532
-.936	.9733	.8183	.9169	.9569
-.988	.9803	.8335	.9220	.9598
-1.040	.9874	.8469	.9261	.9620

(jj) x/D = 8.39; y/D = 0.21; $\alpha = 0^\circ$;

p_∞ = 101.41 psf (4855.31 N/m^2);
q_∞ = 375.50 psf (17979.21 N/m^2);
$p_{t,\infty}$ = 1268.00 psf (60712.17 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9929	.8615	.9315	.9649
.988	.9717	.8404	.9300	.9641
.936	.9504	.8315	.9354	.9670
.884	.9504	.8175	.9275	.9627
.832	.9504	.8070	.9215	.9595
.780	.9527	.7946	.9133	.9549
.728	.9551	.7805	.9040	.9497
.676	.9527	.7684	.8981	.9464
.624	.9504	.7581	.8931	.9435
.572	.9504	.7441	.8848	.9388
.520	.9504	.7336	.8786	.9351
.468	.9527	.7177	.8679	.9288
.416	.9551	.6982	.8550	.9211
.364	.9504	.6811	.8465	.9159
.312	.9456	.6622	.8368	.9098
.260	.9433	.6290	.8166	.8970
.208	.9409	.6082	.8040	.8888
.156	.9456	.5867	.7877	.8780
.104	.9504	.5741	.7772	.8709
.052	.9575	.5630	.7668	.8637
0.000	.9646	.5553	.7588	.8581
-.104	.9551	.5515	.7599	.8589
-.156	.9551	.5586	.7647	.8623
-.208	.9551	.5727	.7743	.8689
-.260	.9527	.5834	.7825	.8745
-.312	.9527	.6027	.7954	.8831
-.364	.9504	.6258	.8114	.8937
-.416	.9504	.6574	.8317	.9066
-.468	.9480	.6821	.8482	.9169
-.520	.9456	.7051	.8635	.9262
-.572	.9480	.7224	.8729	.9318
-.624	.9504	.7362	.8802	.9360
-.676	.9527	.7518	.8883	.9408
-.728	.9551	.7639	.8943	.9442
-.780	.9551	.7762	.9015	.9483
-.832	.9551	.7884	.9086	.9523
-.884	.9575	.7987	.9134	.9550
-.936	.9598	.8126	.9201	.9587
-.988	.9669	.8225	.9223	.9599
-1.040	.9740	.8395	.9284	.9632

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Concluded

(kk) x/D = 8.39; y/D = 0.0; $\alpha = 0^o$;

p_∞ = 101.48 psf (4858.76 N/m^2);
q_∞ = 375.77 psf (17991.97 N/m^2);
$p_{t,\infty}$ = 1268.90 psf (60755.26 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9684	.8540	.9391	.9690
.988	.9518	.8343	.9362	.9674
.936	.9353	.8233	.9382	.9685
.884	.9329	.8112	.9325	.9654
.832	.9306	.7992	.9267	.9623
.780	.9329	.7868	.9183	.9577
.728	.9353	.7779	.9120	.9542
.676	.9353	.7674	.9058	.9507
.624	.9353	.7587	.9006	.9478
.572	.9353	.7499	.8954	.9449
.520	.9353	.7412	.8902	.9419
.468	.9353	.7272	.8817	.9370
.416	.9353	.7114	.8722	.9313
.364	.9329	.6959	.8637	.9263
.312	.9306	.6821	.8561	.9217
.260	.9282	.6578	.8418	.9129
.208	.9259	.6422	.8328	.9073
.156	.9306	.6225	.8179	.8979
.104	.9353	.6081	.8064	.8904
.052	.9424	.5883	.7901	.8796
0.000	.9495	.5754	.7785	.8718
-.104	.9353	.5790	.7868	.8774
-.156	.9377	.5912	.7940	.8822
-.208	.9400	.6138	.8081	.8915
-.260	.9353	.6300	.8207	.8996
-.312	.9377	.6438	.8286	.9047
-.364	.9377	.6648	.8420	.9131
-.416	.9353	.6878	.8575	.9226
-.468	.9353	.7018	.8662	.9278
-.520	.9353	.7193	.8770	.9342
-.572	.9353	.7316	.8844	.9385
-.624	.9353	.7421	.8907	.9422
-.676	.9353	.7526	.8970	.9458
-.728	.9353	.7631	.9032	.9493
-.780	.9353	.7718	.9084	.9522
-.832	.9353	.7841	.9156	.9562
-.884	.9377	.7944	.9204	.9589
-.936	.9400	.8064	.9262	.9620
-.988	.9471	.8181	.9294	.9638
-1.040	.9542	.8316	.9335	.9660

(ll) x/D = 8.39; y/D = -0.42; $\alpha = 0^o$;

p_∞ = 101.45 psf (4857.61 N/m^2);
q_∞ = 375.68 psf (17987.72 N/m^2);
$p_{t,\infty}$ = 1268.60 psf (60740.90 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9261	.8540	.9603	.9801
.988	.9095	.8343	.9577	.9788
.936	.8930	.8233	.9602	.9800
.884	.8883	.8097	.9547	.9772
.832	.8836	.7978	.9502	.9749
.780	.8883	.7835	.9392	.9690
.728	.8930	.7691	.9281	.9630
.676	.8906	.7553	.9209	.9591
.624	.8883	.7433	.9147	.9557
.572	.8906	.7291	.9048	.9502
.520	.8930	.7150	.8948	.9445
.468	.8930	.7045	.8882	.9407
.416	.8930	.7097	.8915	.9426
.364	.8906	.7239	.9015	.9483
.312	.8883	.7276	.9050	.9503
.260	.8883	.7206	.9007	.9478
.208	.8883	.7153	.8974	.9460
.156	.8883	.7101	.8941	.9441
.104	.8883	.6996	.8874	.9403
.052	.8906	.6749	.8705	.9304
0.000	.8930	.6607	.8602	.9242
-.104	.8836	.6806	.8777	.9346
-.156	.8930	.6922	.8804	.9362
-.208	.9025	.7037	.8830	.9377
-.260	.8883	.7083	.8930	.9435
-.312	.8977	.7128	.8911	.9424
-.364	.8954	.7200	.8968	.9456
-.416	.8930	.7202	.8981	.9464
-.468	.8906	.7064	.8906	.9421
-.520	.8883	.6978	.8863	.9396
-.572	.8883	.7083	.8930	.9435
-.624	.8883	.7223	.9018	.9485
-.676	.8883	.7398	.9126	.9545
-.728	.8883	.7556	.9223	.9599
-.780	.8906	.7694	.9295	.9638
-.832	.8930	.7815	.9355	.9670
-.884	.8954	.7971	.9435	.9713
-.936	.8977	.8109	.9504	.9750
-.988	.9048	.8209	.9525	.9760
-1.040	.9119	.8326	.9555	.9776

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0.0$; $\alpha = 0°$;

p_∞ = 51.77 psf (2478.89 N/m^2);
q_∞ = 317.53 psf (15203.33 N/m^2);
$p_{t,\infty}$ = 1790.80 psf (85743.97 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0340	.6555	.7962	.9092
.988	.9001	.6141	.8260	.9248
.936	.7663	.5851	.8738	.9481
.884	.7201	.5542	.8773	.9497
.832	.6739	.5316	.8881	.9546
.780	.6324	.5108	.8987	.9594
.728	.5908	.4900	.9107	.9646
.676	.5539	.4711	.9222	.9695
.624	.5170	.4562	.9394	.9767
.572	.4385	.4432	1.0053	1.0019
.520	.3600	.4281	1.0904	1.0302
.468	.3370	.4147	1.1094	1.0359
.416	.3139	.4137	1.1480	1.0469
.364	.3970	.3546	.9452	.9790
.312	.4801	.1799	.6122	.7890
.260	.5124	.0538	.3242	.4942
.208	.5447	.0124	.1511	.2459
.156	.5447	.0054	.0997	.1639
.104	.5447	.0054	.0997	.1639
.052	.5401	.0061	.1065	.1750
0.000	.5355	.0068	.1130	.1855
-.104	.5355	.0035	.0810	.1336
-.156	.5308	.0042	.0894	.1473
-.208	.5262	.0050	.0971	.1598
-.260	.4616	.0329	.2669	.4174
-.312	.4570	.1064	.4826	.6747
-.364	.4708	.2742	.7631	.8907
-.416	.3877	.4016	1.0177	1.0063
-.468	.4016	.4072	1.0070	1.0025
-.520	.4154	.4210	1.0067	1.0024
-.572	.4385	.4406	1.0024	1.0009
-.624	.4616	.4602	.9985	.9995
-.676	.5216	.4803	.9596	.9847
-.728	.5816	.4942	.9218	.9693
-.780	.6232	.5109	.9055	.9623
-.832	.6647	.5318	.8945	.9575
-.884	.7109	.5586	.8865	.9539
-.936	.7570	.5917	.8841	.9528
-.988	.8401	.6190	.8584	.9408
-1.040	.9232	.6607	.8460	.9348

(b) $x/D = 1.5$; $y/D = 0.0$; $\alpha = 0°$;

p_∞ = 51.80 psf (2480.14 N/m^2);
q_∞ = 317.69 psf (15210.97 N/m^2);
$p_{t,\infty}$ = 1791.70 psf (85787.06 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8493	.5921	.8349	.9293
.988	.7431	.5618	.8695	.9461
.936	.6370	.5418	.9222	.9695
.884	.6001	.5187	.9298	.9727
.832	.5631	.5039	.9459	.9793
.780	.5400	.4884	.9510	.9813
.728	.5170	.4771	.9607	.9852
.676	.5031	.4674	.9639	.9864
.624	.4893	.4598	.9694	.9886
.572	.4477	.4575	1.0108	1.0039
.520	.4062	.4511	1.0538	1.0186
.468	.4293	.4418	1.0145	1.0052
.416	.4523	.4593	1.0077	1.0028
.364	.6462	.5640	.9342	.9745
.312	.8401	.5884	.8369	.9303
.260	.9693	.5888	.7794	.8999
.208	1.0986	.4135	.6135	.7901
.156	1.1493	.1813	.3971	.5832
.104	1.2001	.0820	.2615	.4099
.052	1.1816	.0979	.2878	.4462
0.000	1.1632	.1397	.3465	.5225
-.104	1.1816	.0792	.2588	.4062
-.156	1.1493	.1344	.3420	.5169
-.208	1.1170	.3349	.5476	.7355
-.260	.8170	.5750	.8389	.9313
-.312	.7847	.5929	.8693	.9460
-.364	.7847	.5537	.8400	.9319
-.416	.4523	.4362	.9820	.9933
-.468	.4523	.4362	.9820	.9933
-.520	.4523	.4424	.9889	.9959
-.572	.4477	.4508	1.0034	1.0012
-.624	.4431	.4572	1.0158	1.0056
-.676	.4754	.4641	.9880	.9956
-.728	.5077	.4730	.9652	.9869
-.780	.5354	.4862	.9529	.9821
-.832	.5631	.5015	.9437	.9784
-.884	.5770	.5195	.9489	.9805
-.936	.5908	.5416	.9574	.9839
-.988	.6508	.5616	.9290	.9723
-1.040	.7108	.5920	.9126	.9654

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(c) x/D = 2.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 51.84 psf (2482.21 N/m^2);
q_∞ = 317.95 psf (15223.71 N/m^2);
$p_{t,\infty}$ = 1793.20 psf (85858.88 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7481	.5700	.8728	.9476
.988	.6604	.5491	.9119	.9651
.936	.5726	.5344	.9661	.9873
.884	.5542	.5167	.9656	.9871
.832	.5357	.5073	.9731	.9900
.780	.5218	.4976	.9765	.9913
.728	.5080	.4920	.9841	.9942
.676	.6050	.5289	.9350	.9749
.624	.7020	.5514	.8863	.9538
.572	.6650	.5366	.8983	.9592
.520	.6281	.5279	.9168	.9672
.468	.8451	.5760	.8255	.9246
.416	1.0622	.6383	.7752	.8976
.364	1.1453	.6573	.7575	.8874
.312	1.2284	.6617	.7339	.8733
.260	1.2423	.6363	.7157	.8620
.208	1.2561	.5469	.6598	.8245
.156	1.2654	.4096	.5690	.7540
.104	1.2746	.3235	.5038	.6954
.052	1.2654	.3072	.4927	.6847
0.000	1.2561	.3140	.5000	.6917
-.104	1.2654	.3307	.5112	.7024
-.156	1.2746	.3993	.5597	.7461
-.208	1.2838	.5359	.6461	.8146
-.260	1.1453	.6415	.7484	.8821
-.312	1.1545	.6618	.7571	.8872
-.364	.9744	.6595	.8227	.9231
-.416	1.0252	.6243	.7803	.9004
-.468	.8451	.5416	.8005	.9115
-.520	.6650	.5249	.8884	.9548
-.572	.6650	.5413	.9022	.9609
-.624	.6650	.5599	.9175	.9675
-.676	.5911	.4787	.8999	.9599
-.728	.5172	.4840	.9673	.9877
-.780	.5218	.4920	.9710	.9892
-.832	.5265	.5000	.9746	.9905
-.884	.5265	.5144	.9885	.9958
-.936	.5265	.5309	1.0042	1.0015
-.988	.5634	.5458	.9842	.9942
-1.040	.6004	.5709	.9752	.9908

(d) x/D = 2.5; y/D = 3.0; $\alpha = 0^\circ$;

p_∞ = 51.83 psf (2481.80 N/m^2);
q_∞ = 317.90 psf (15221.16 N/m^2);
$p_{t,\infty}$ = 1792.90 psf (85844.51 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0990	1.0041	.9558	.9833
.988	1.0390	1.0088	.9853	.9946
.936	.9790	1.0134	1.0174	1.0062
.884	.9744	1.0136	1.0199	1.0071
.832	.9697	1.0138	1.0225	1.0080
.780	.9697	1.0138	1.0225	1.0080
.728	.9697	1.0138	1.0225	1.0080
.676	.9697	1.0118	1.0214	1.0076
.624	.9697	1.0118	1.0214	1.0076
.572	.9790	1.0134	1.0174	1.0062
.520	.9882	1.0130	1.0125	1.0045
.468	.9836	1.0132	1.0149	1.0054
.416	.9790	1.0134	1.0174	1.0062
.364	.9790	1.0134	1.0174	1.0062
.312	.9790	1.0134	1.0174	1.0062
.260	.9744	1.0157	1.0210	1.0075
.208	.9697	1.0179	1.0245	1.0087
.156	.9744	1.0136	1.0199	1.0071
.104	.9790	1.0134	1.0174	1.0062
.052	.9790	1.0114	1.0164	1.0059
0.000	.9790	1.0114	1.0164	1.0059
-.104	.9697	1.0038	1.0174	1.0062
-.156	.9744	1.0057	1.0159	1.0057
-.208	.9790	1.0055	1.0134	1.0048
-.260	.9605	1.0063	1.0235	1.0084
-.312	.9651	1.0061	1.0210	1.0075
-.364	.9651	1.0061	1.0210	1.0075
-.416	.9513	1.0025	1.0266	1.0094
-.468	.9513	1.0025	1.0266	1.0094
-.520	.9513	1.0046	1.0277	1.0098
-.572	.9559	1.0023	1.0240	1.0085
-.624	.9605	1.0042	1.0225	1.0080
-.676	.9651	1.0040	1.0199	1.0071
-.728	.9697	1.0059	1.0185	1.0066
-.780	.9605	1.0063	1.0235	1.0084
-.832	.9513	1.0067	1.0287	1.0101
-.884	.9605	1.0042	1.0225	1.0080
-.936	.9697	1.0038	1.0174	1.0062
-.988	.9790	1.0034	1.0124	1.0045
-1.040	.9882	1.0010	1.0064	1.0023

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(e) $x/D = 2.5$; $y/D = 2.0$; $\alpha = 0^\circ$;

p_∞ = 51.82 psf (2481.11 N/m^2);
q_∞ = 317.81 psf (15216.92 N/m^2);
$p_{t,\infty}$ = 1792.40 psf (85820.57 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.5055	1.2004	.8930	.9568
.988	1.4224	1.1897	.9146	.9663
.936	1.3392	1.1830	.9399	.9768
.884	1.3161	1.1696	.9427	.9780
.832	1.2930	1.1645	.9490	.9805
.780	1.2792	1.1548	.9501	.9810
.728	1.2653	1.1431	.9505	.9811
.676	1.2515	1.1334	.9517	.9816
.624	1.2376	1.1237	.9529	.9821
.572	1.2469	1.1151	.9457	.9792
.520	1.2561	1.1106	.9403	.9770
.468	1.2469	1.1048	.9413	.9774
.416	1.2376	1.0991	.9424	.9779
.364	1.2284	1.0912	.9425	.9779
.312	1.2192	1.0896	.9454	.9791
.260	1.2007	1.0822	.9494	.9807
.208	1.1822	1.0809	.9562	.9834
.156	1.1868	1.0766	.9524	.9819
.104	1.1915	1.0744	.9496	.9808
.052	1.1961	1.0742	.9477	.9800
0.000	1.2007	1.0740	.9458	.9792
-.104	1.1822	1.0670	.9500	.9809
-.156	1.1776	1.0733	.9547	.9828
-.208	1.1730	1.0756	.9576	.9839
-.260	1.1545	1.0785	.9665	.9874
-.312	1.1499	1.0869	.9722	.9896
-.364	1.1591	1.0865	.9682	.9881
-.416	1.1268	1.0961	.9863	.9950
-.468	1.1360	1.1040	.9858	.9948
-.520	1.1453	1.1118	.9853	.9946
-.572	1.1915	1.1139	.9669	.9876
-.624	1.2376	1.1202	.9514	.9815
-.676	1.2700	1.1291	.9429	.9781
-.728	1.3023	1.1421	.9365	.9754
-.780	1.2838	1.1511	.9469	.9797
-.832	1.2653	1.1602	.9575	.9839
-.884	1.3115	1.1767	.9472	.9798
-.936	1.3577	1.1891	.9358	.9752
-.988	1.3900	1.2021	.9299	.9728
-1.040	1.4224	1.2110	.9227	.9697

(f) $x/D = 2.5$; $y/D = 1.5$; $\alpha = 0^\circ$;

p_∞ = 51.84 psf (2482.21 N/m^2);
q_∞ = 317.95 psf (15223.71 N/m^2);
$p_{t,\infty}$ = 1793.20 psf (85858.88 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1540	.9615	.9128	.9655
.988	1.0663	.9489	.9433	.9783
.936	.9786	.9363	.9781	.9919
.884	.9555	.9209	.9817	.9932
.832	.9324	.9095	.9877	.9955
.780	.9186	.8937	.9864	.9950
.728	.9047	.8800	.9862	.9949
.676	.8863	.8705	.9911	.9967
.624	.8678	.8590	.9949	.9981
.572	.8586	.8491	.9945	.9980
.520	.8493	.8413	.9953	.9983
.468	.8355	.8317	.9977	.9992
.416	.8216	.8241	1.0015	1.0005
.364	.8124	.8142	1.0011	1.0004
.312	.8032	.8085	1.0033	1.0012
.260	.7986	.8025	1.0025	1.0009
.208	.7939	.7986	1.0029	1.0011
.156	.7893	.7947	1.0034	1.0012
.104	.7847	.7908	1.0039	1.0014
.052	.7893	.7906	1.0008	1.0003
0.000	.7939	.7883	.9965	.9987
-.104	.7755	.7857	1.0066	1.0024
-.156	.7939	.7890	.9969	.9989
-.208	.8124	.7903	.9863	.9950
-.260	.7986	.7971	.9991	.9997
-.312	.8170	.8024	.9910	.9967
-.364	.8263	.8041	.9865	.9950
-.416	.8216	.8146	.9957	.9984
-.468	.8309	.8224	.9949	.9981
-.520	.8401	.8344	.9966	.9988
-.572	.8540	.8420	.9930	.9974
-.624	.8678	.8538	.9919	.9970
-.676	.8817	.8635	.9896	.9962
-.728	.8955	.8793	.9909	.9967
-.780	.9093	.8911	.9899	.9963
-.832	.9232	.9049	.9900	.9963
-.884	.9555	.9200	.9812	.9931
-.936	.9878	.9391	.9750	.9907
-.988	1.0201	.9521	.9661	.9873
-1.040	1.0524	.9672	.9587	.9844

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(g) $x/D = 2.5$; $y/D = 1.0$; $\alpha = 0^\circ$;

p_∞ = 51.96 psf (2483.04 N/m^2);
q_∞ = 318.06 psf (15228.80 N/m^2);
$p_{t,\infty}$ = 1793.80 psf (85887.61 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8860	.7530	.9219	.9694
.988	.8029	.7319	.9548	.9828
.936	.7199	.7191	.9995	.9998
.884	.6968	.6995	1.0020	1.0007
.832	.6737	.6820	1.0062	1.0022
.780	.6691	.6658	.9975	.9991
.728	.6645	.6475	.9871	.9953
.676	.6460	.6360	.9922	.9971
.624	.6276	.6244	.9975	.9991
.572	.6091	.6129	1.0031	1.0011
.520	.5906	.6034	1.0108	1.0039
.468	.5906	.5931	1.0021	1.0008
.416	.5906	.5849	.9951	.9982
.364	.5999	.5763	.9802	.9926
.312	.6091	.5718	.9689	.9884
.260	.6645	.5653	.9223	.9696
.208	.7199	.5587	.8810	.9514
.156	.7014	.5554	.8899	.9554
.104	.6829	.5542	.9008	.9603
.052	.6922	.5476	.8895	.9552
0.000	.7014	.5492	.8849	.9532
-.104	.7199	.5470	.8717	.9471
-.156	.7199	.5491	.8734	.9479
-.208	.7199	.5511	.8750	.9486
-.260	.7291	.5549	.8724	.9474
-.312	.7291	.5590	.8756	.9489
-.364	.6737	.5635	.9145	.9662
-.416	.7383	.5709	.8794	.9506
-.468	.6829	.5816	.9228	.9698
-.520	.6276	.5922	.9714	.9893
-.572	.6276	.6046	.9815	.9932
-.624	.6276	.6149	.9898	.9963
-.676	.6276	.6293	1.0014	1.0005
-.728	.6276	.6457	1.0144	1.0052
-.780	.6506	.6591	1.0065	1.0024
-.832	.6737	.6725	.9991	.9997
-.884	.6875	.6946	1.0051	1.0018
-.936	.7014	.7125	1.0079	1.0028
-.988	.7291	.7298	1.0005	1.0002
-1.040	.7568	.7492	.9950	.9982

(h) $x/D = 2.5$; $y/D = 0.83$; $\alpha = 0^\circ$;

p_∞ = 51.84 psf (2481.94 N/m^2);
q_∞ = 317.92 psf (15222.01 N/m^2);
$p_{t,\infty}$ = 1793.00 psf (85849.30 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8210	.6978	.9219	.9694
.988	.7426	.6745	.9530	.9821
.936	.6642	.6614	.9979	.9992
.884	.6411	.6419	1.0006	1.0002
.832	.6181	.6265	1.0068	1.0024
.780	.6135	.6102	.9974	.9990
.728	.6088	.5940	.9877	.9955
.676	.5996	.5821	.9853	.9946
.624	.5904	.5701	.9827	.9936
.572	.5719	.5627	.9919	.9970
.520	.5535	.5553	1.0016	1.0006
.468	.5397	.5477	1.0074	1.0027
.416	.5258	.5421	1.0154	1.0055
.364	.5258	.5401	1.0135	1.0048
.312	.5258	.5360	1.0096	1.0035
.260	.5397	.5313	.9922	.9971
.208	.5535	.5266	.9754	.9908
.156	.5489	.5247	.9777	.9917
.104	.5443	.5228	.9801	.9926
.052	.5397	.5189	.9806	.9928
0.000	.5350	.5212	.9870	.9952
-.104	.5535	.5195	.9688	.9883
-.156	.5673	.5189	.9564	.9835
-.208	.5812	.5204	.9463	.9794
-.260	.6135	.5190	.9198	.9685
-.312	.6273	.5225	.9127	.9654
-.364	.5996	.5258	.9364	.9754
-.416	.6734	.5287	.8861	.9537
-.468	.6457	.5341	.9094	.9640
-.520	.6181	.5435	.9377	.9760
-.572	.6227	.5536	.9429	.9781
-.624	.6273	.5616	.9462	.9794
-.676	.6088	.5748	.9716	.9894
-.728	.5904	.5879	.9979	.9992
-.780	.6042	.6018	.9979	.9993
-.832	.6181	.6156	.9980	.9993
-.884	.6227	.6360	1.0106	1.0038
-.936	.6273	.6563	1.0229	1.0081
-.988	.6596	.6714	1.0089	1.0032
-1.040	.6919	.6927	1.0006	1.0002

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(i) x/D = 2.5; y/D = 0.63; $\alpha = 0^\circ$;

p_∞ = 51.87 psf (2483.32 N/m^2);
q_∞ = 318.10 psf (15230.50 N/m^2);
$p_{t,\infty}$ = 1794.00 psf (85897.18 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7649	.6369	.9125	.9654
.988	.6866	.6177	.9485	.9803
.936	.6082	.6026	.9954	.9983
.884	.5944	.5847	.9918	.9970
.832	.5806	.5709	.9916	.9969
.780	.5760	.5588	.9850	.9945
.728	.5714	.5466	.9781	.9919
.676	.5714	.5364	.9689	.9884
.624	.5714	.5281	.9614	.9855
.572	.5529	.5248	.9743	.9904
.520	.5345	.5174	.9839	.9941
.468	.5253	.5137	.9889	.9959
.416	.5161	.5141	.9981	.9993
.364	.6773	.5441	.8962	.9583
.312	.8386	.6398	.8735	.9479
.260	.9584	.6818	.8435	.9336
.208	1.0782	.6765	.7921	.9069
.156	1.1105	.6709	.7773	.8987
.104	1.1427	.6674	.7642	.8913
.052	1.1427	.6654	.7631	.8906
0.000	1.1427	.6654	.7631	.8906
-.104	1.1335	.6604	.7633	.8908
-.156	1.1197	.6631	.7695	.8944
-.208	1.1059	.6658	.7759	.8980
-.260	.8524	.6770	.8912	.9560
-.312	.8386	.6200	.8598	.9415
-.364	.8386	.5273	.7929	.9074
-.416	.5714	.5082	.9431	.9781
-.468	.5714	.5082	.9431	.9781
-.520	.5714	.5102	.9450	.9789
-.572	.5621	.5189	.9607	.9852
-.624	.5529	.5234	.9729	.9899
-.676	.5575	.5314	.9763	.9912
-.728	.5621	.5394	.9796	.9924
-.780	.5668	.5516	.9865	.9950
-.832	.5714	.5637	.9933	.9976
-.884	.5714	.5802	1.0077	1.0028
-.936	.5714	.5987	1.0237	1.0084
-.988	.5990	.6140	1.0124	1.0045
-1.040	.6267	.6334	1.0053	1.0019

(j) x/D = 2.5; y/D = 0.42; $\alpha = 0^\circ$;

p_∞ = 51.87 psf (2483.74 N/m^2);
q_∞ = 318.15 psf (15233.05 N/m^2);
$p_{t,\infty}$ = 1794.30 psf (85911.55 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7279	.6014	.9090	.9639
.988	.6542	.5820	.9433	.9782
.936	.5805	.5709	.9917	.9970
.884	.5667	.5550	.9897	.9962
.832	.5528	.5433	.9913	.9968
.780	.5574	.5328	.9777	.9917
.728	.5620	.5244	.9659	.9872
.676	.5667	.5180	.9561	.9834
.624	.5713	.5137	.9483	.9802
.572	.8569	.6081	.8424	.9331
.520	1.1425	.6777	.7702	.8947
.468	1.1517	.6711	.7633	.8908
.416	1.1610	.6624	.7554	.8862
.364	1.1610	.6583	.7530	.8848
.312	1.1610	.6542	.7507	.8834
.260	1.1563	.6482	.7487	.8822
.208	1.1517	.6443	.7479	.8818
.156	1.1563	.6379	.7427	.8787
.104	1.1610	.6274	.7351	.8740
.052	1.1563	.6193	.7319	.8720
0.000	1.1517	.6175	.7322	.8723
-.104	1.1425	.6228	.7383	.8760
-.156	1.1471	.6329	.7428	.8787
-.208	1.1517	.6368	.7436	.8792
-.260	1.1333	.6418	.7525	.8845
-.312	1.1379	.6478	.7545	.8856
-.364	1.0550	.6536	.7871	.9042
-.416	1.1241	.6566	.7643	.8913
-.468	1.0412	.6665	.8001	.9113
-.520	.9582	.6764	.8402	.9319
-.572	.7601	.5122	.8208	.9222
-.624	.5620	.5085	.9512	.9814
-.676	.5574	.5108	.9572	.9838
-.728	.5528	.5192	.9691	.9884
-.780	.5528	.5233	.9730	.9899
-.832	.5528	.5357	.9844	.9942
-.884	.5436	.5464	1.0025	1.0009
-.936	.5344	.5632	1.0266	1.0094
-.988	.5620	.5764	1.0127	1.0046
-1.040	.5897	.5938	1.0034	1.0012

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(k) $x/D = 2.5$; $y/D = 0.21$; $\alpha = 0^o$;

$p_\infty = 51.80$ psf (2480.27 N/m^2);
$q_\infty = 317.71$ psf (15211.82 N/m^2);
$p_{t,\infty} = 1791.80$ psf (85791.85 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7200	.5793	.8970	.9586
.988	.6462	.5641	.9343	.9746
.936	.5723	.5529	.9829	.9937
.884	.5631	.5389	.9783	.9919
.832	.5539	.5311	.9792	.9923
.780	.5585	.5247	.9693	.9885
.728	.5631	.5183	.9594	.9847
.676	.8077	.6722	.9122	.9653
.624	1.0523	.6675	.7964	.9093
.572	1.1031	.6632	.7754	.8977
.520	1.1539	.6568	.7544	.8856
.468	1.1585	.6504	.7493	.8826
.416	1.1631	.6440	.7441	.8795
.364	1.1585	.6421	.7445	.8797
.312	1.1539	.6361	.7425	.8785
.260	1.1354	.6040	.7294	.8705
.208	1.1170	.5512	.7025	.8534
.156	1.1170	.4727	.6505	.8178
.104	1.1170	.3981	.5970	.7771
.052	1.1170	.3482	.5584	.7449
0.000	1.1170	.3295	.5431	.7316
-.104	1.0893	.3818	.5920	.7731
-.156	1.1123	.4471	.6340	.8057
-.208	1.1354	.5331	.6852	.8420
-.260	1.1123	.5982	.7334	.8730
-.312	1.1354	.6261	.7426	.8786
-.364	1.1216	.6371	.7537	.8852
-.416	1.1354	.6365	.7487	.8822
-.468	1.1216	.6433	.7573	.8873
-.520	1.1077	.6480	.7649	.8917
-.572	1.0800	.6534	.7778	.8990
-.624	1.0523	.6609	.7925	.9071
-.676	.8123	.5622	.8319	.9278
-.728	.5723	.5109	.9448	.9788
-.780	.5631	.5134	.9548	.9829
-.832	.5539	.5199	.9689	.9884
-.884	.5400	.5308	.9915	.9969
-.936	.5262	.5459	1.0185	1.0066
-.988	.5492	.5572	1.0072	1.0026
-1.040	.5723	.5727	1.0003	1.0001

(l) $x/D = 2.5$; $y/D = 0.0$; $\alpha = 0^o$;

$p_\infty = 51.81$ psf (2480.69 N/m^2);
$q_\infty = 317.76$ psf (15214.37 N/m^2);
$p_{t,\infty} = 1792.10$ psf (85806.21 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7199	.5751	.8938	.9572
.988	.6461	.5578	.9292	.9724
.936	.5722	.5487	.9792	.9923
.884	.6553	.6211	.9736	.9902
.832	.7384	.5949	.8976	.9589
.780	.7153	.5712	.8936	.9571
.728	.6922	.5496	.8911	.9560
.676	.7845	.5599	.8448	.9342
.624	.8768	.6608	.8681	.9454
.572	1.0199	.6730	.8123	.9177
.520	1.1629	.6665	.7571	.8872
.468	1.1629	.6624	.7547	.8858
.416	1.1629	.6562	.7512	.8837
.364	1.1629	.6480	.7465	.8809
.312	1.1629	.6315	.7369	.8751
.260	1.1491	.5868	.7146	.8612
.208	1.1352	.5234	.6790	.8378
.156	1.1352	.4386	.6216	.7963
.104	1.1352	.3909	.5868	.7688
.052	1.1445	.3718	.5700	.7548
0.000	1.1537	.3672	.5641	.7499
-.104	1.1352	.4023	.5953	.7757
-.156	1.1445	.4455	.6239	.7981
-.208	1.1537	.5218	.6725	.8333
-.260	1.1445	.5884	.7170	.8628
-.312	1.1537	.6252	.7361	.8747
-.364	1.1445	.6421	.7490	.8824
-.416	1.1537	.6479	.7494	.8826
-.468	1.1445	.6545	.7562	.8867
-.520	1.1352	.6591	.7619	.8900
-.572	.9783	.6578	.8200	.9217
-.624	.8214	.6029	.8567	.9400
-.676	.7568	.5336	.8397	.9317
-.728	.6922	.5530	.8938	.9572
-.780	.7199	.5703	.8900	.9555
-.832	.7476	.5918	.8897	.9553
-.884	.6368	.5677	.9442	.9786
-.936	.5261	.5396	1.0128	1.0046
-.988	.5445	.5512	1.0061	1.0022
-1.040	.5630	.5668	1.0034	1.0012

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(m) $x/D = 2.5$; $y/D = -0.42$; $\alpha = 0^0$;

p_∞ = 51.82 psf (2481.38 N/m^2);
q_∞ = 317.85 psf (15218.61 N/m^2);
$p_{t,\infty}$ = 1792.60 psf (85830.15 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9038	.6594	.8542	.9388
.988	.7931	.6273	.8893	.9552
.936	.6825	.6013	.9386	.9763
.884	.6502	.5718	.9378	.9760
.832	.6179	.5506	.9440	.9785
.780	.5856	.5335	.9545	.9827
.728	.5534	.5226	.9718	.9895
.676	.5487	.5125	.9665	.9874
.624	.5441	.4943	.9531	.9822
.572	.4934	.4738	.9800	.9926
.520	.4427	.4514	1.0098	1.0035
.468	.7701	.5254	.8260	.9248
.416	1.0975	.6302	.7577	.8875
.364	1.1067	.6133	.7444	.8796
.312	1.1159	.6396	.7571	.8872
.260	1.1252	.6371	.7525	.8845
.208	1.1344	.6305	.7456	.8803
.156	1.1390	.6221	.7390	.8764
.104	1.1436	.6178	.7350	.8739
.052	1.1482	.5784	.7097	.8581
0.000	1.1528	.5162	.6692	.8310
-.104	1.1344	.6114	.7341	.8734
-.156	1.1482	.6170	.7330	.8728
-.208	1.1621	.6205	.7307	.8713
-.260	1.0560	.6315	.7733	.8965
-.312	1.0698	.6329	.7692	.8941
-.364	.8208	.6193	.8686	.9457
-.416	.9776	.6350	.8059	.9144
-.468	.7286	.4171	.7566	.8869
-.520	.4796	.4508	.9696	.9886
-.572	.4842	.4774	.9930	.9974
-.624	.4888	.5019	1.0133	1.0048
-.676	.5257	.5127	.9875	.9954
-.728	.5626	.5214	.9627	.9859
-.780	.5856	.5286	.9501	.9810
-.832	.6087	.5503	.9508	.9813
-.884	.6318	.5760	.9549	.9829
-.936	.6548	.6039	.9603	.9850
-.988	.7148	.6342	.9420	.9777
-1.040	.7747	.6666	.9276	.9718

(n) $x/D = 3.0$; $y/D = 0.0$; $\alpha = 0^0$;

p_∞ = 51.78 psf (2479.03 N/m^2);
q_∞ = 317.55 psf (15204.18 N/m^2);
$p_{t,\infty}$ = 1790.90 psf (85748.75 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8862	.6554	.8600	.9416
.988	.7939	.6307	.8913	.9561
.936	.7016	.6100	.9324	.9738
.884	.7939	.5894	.8617	.9424
.832	.8862	.7193	.9009	.9603
.780	.9785	.7070	.8500	.9368
.728	1.0708	.6885	.8018	.9122
.676	1.0708	.6740	.7934	.9076
.624	1.0708	.6637	.7873	.9043
.572	1.0755	.6532	.7793	.8999
.520	1.0801	.6447	.7726	.8961
.468	1.0708	.6348	.7700	.8946
.416	1.0616	.6270	.7685	.8938
.364	1.0524	.6150	.7645	.8914
.312	1.0432	.5948	.7551	.8860
.260	1.0293	.5500	.7310	.8715
.208	1.0155	.5052	.7053	.8553
.156	1.0155	.4452	.6621	.8261
.104	1.0155	.4162	.6402	.8103
.052	1.0247	.3992	.6241	.7982
0.000	1.0339	.3883	.6129	.7896
-.104	1.0155	.4271	.6485	.8163
-.156	1.0247	.4536	.6653	.8283
-.208	1.0339	.5029	.6974	.8501
-.260	1.0339	.5567	.7338	.8732
-.312	1.0432	.5914	.7529	.8847
-.364	1.0478	.6098	.7629	.8905
-.416	1.0524	.6220	.7688	.8939
-.468	1.0570	.6321	.7733	.8965
-.520	1.0616	.6401	.7765	.8983
-.572	1.0708	.6480	.7779	.8991
-.624	1.0801	.6579	.7805	.9005
-.676	1.0801	.6703	.7878	.9046
-.728	1.0801	.6847	.7962	.9092
-.780	.9324	.7037	.8688	.9457
-.832	.7847	.6215	.8900	.9555
-.884	.7293	.5847	.8954	.9579
-.936	.6739	.6098	.9513	.9814
-.988	.7154	.6286	.9374	.9758
-1.040	.7570	.6536	.9292	.9725

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(o) x/D = 4.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 51.85 psf (2482.49 N/m^2);
q_∞ = 317.99 psf (15225.41 N/m^2);
$p_{t,\infty}$ = 1793.40 psf (85868.45 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1336	.7632	.8205	.9220
.988	1.0553	.7379	.8362	.9300
.936	.9769	.7146	.8553	.9393
.884	.9723	.6902	.8425	.9331
.832	.9677	.6740	.8345	.9291
.780	.9631	.6598	.8277	.9257
.728	.9585	.6477	.8220	.9228
.676	.9585	.6353	.8142	.9187
.624	.9585	.6271	.8089	.9159
.572	.9631	.6187	.8015	.9120
.520	.9677	.6123	.7955	.9088
.468	.9585	.6066	.7955	.9088
.416	.9493	.5988	.7942	.9081
.364	.9447	.5825	.7853	.9032
.312	.9401	.5622	.7733	.8965
.260	.9309	.5276	.7529	.8847
.208	.9216	.4972	.7345	.8736
.156	.9216	.4601	.7066	.8561
.104	.9216	.4354	.6873	.8434
.052	.9262	.4187	.6723	.8332
0.000	.9309	.4123	.6655	.8285
-.104	.9216	.4432	.6935	.8475
-.156	.9309	.4634	.7056	.8555
-.208	.9401	.4961	.7264	.8687
-.260	.9355	.5314	.7537	.8852
-.312	.9447	.5578	.7684	.8937
-.364	.9447	.5784	.7825	.9016
-.416	.9493	.5927	.7901	.9059
-.468	.9493	.6009	.7956	.9088
-.520	.9493	.6092	.8011	.9118
-.572	.9539	.6151	.8030	.9128
-.624	.9585	.6252	.8077	.9153
-.676	.9585	.6355	.8143	.9188
-.728	.9585	.6438	.8196	.9215
-.780	.9585	.6562	.8274	.9255
-.832	.9585	.6727	.8377	.9307
-.884	.9723	.6906	.8428	.9332
-.936	.9862	.7168	.8525	.9380
-.988	1.0046	.7366	.8563	.9398
-1.040	1.0230	.7646	.8645	.9437

(p) x/D = 5.0; y/D = 3.0; $\alpha = 0^\circ$;

p_∞ = 51.82 psf (2481.11 N/m^2);
q_∞ = 317.81 psf (15216.92 N/m^2);
$p_{t,\infty}$ = 1792.40 psf (85820.57 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3005	1.0999	.9196	.9684
.988	1.2268	1.1010	.9474	.9799
.936	1.1530	1.0981	.9759	.9910
.884	1.1437	1.0944	.9782	.9919
.832	1.1345	1.0948	.9823	.9935
.780	1.1253	1.0910	.9847	.9943
.728	1.1161	1.0873	.9870	.9952
.676	1.1115	1.0834	.9873	.9953
.624	1.1068	1.0836	.9894	.9961
.572	1.1207	1.0789	.9812	.9930
.520	1.1345	1.0783	.9749	.9907
.468	1.1299	1.0764	.9761	.9911
.416	1.1253	1.0725	.9763	.9912
.364	1.1207	1.0727	.9784	.9920
.312	1.1161	1.0688	.9786	.9921
.260	1.1115	1.0690	.9807	.9929
.208	1.1068	1.0692	.9829	.9937
.156	1.1115	1.0690	.9807	.9929
.104	1.1161	1.0688	.9786	.9921
.052	1.1161	1.0688	.9786	.9921
0.000	1.1161	1.0688	.9786	.9921
-.104	1.1068	1.0630	.9800	.9926
-.156	1.0976	1.0675	.9862	.9949
-.208	1.0884	1.0679	.9906	.9965
-.260	1.0838	1.0702	.9937	.9977
-.312	1.0746	1.0747	1.0001	1.0000
-.364	1.0792	1.0745	.9978	.9992
-.416	1.0607	1.0753	1.0069	1.0025
-.468	1.0653	1.0792	1.0065	1.0023
-.520	1.0699	1.0811	1.0052	1.0019
-.572	1.0976	1.0819	.9928	.9974
-.624	1.1253	1.0828	.9809	.9929
-.676	1.1391	1.0863	.9765	.9913
-.728	1.1530	1.0940	.9741	.9903
-.780	1.1437	1.0944	.9782	.9919
-.832	1.1345	1.0968	.9832	.9938
-.884	1.1576	1.1020	.9757	.9910
-.936	1.1806	1.1072	.9684	.9882
-.988	1.1991	1.1064	.9606	.9851
-1.040	1.2175	1.1097	.9547	.9828

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(q) x/D = 5.0; y/D = 2.0; $\alpha = 0^o$;

p_∞ = 51.78 psf (2479.44 N/m^2);
q_∞ = 317.60 psf (15206.73 N/m^2);
$p_{t,\infty}$ = 1791.20 psf (85763.12 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9140	.8724	.9770	.9915
.988	.8540	.8709	1.0099	1.0036
.936	.7940	.8673	1.0452	1.0157
.884	.7801	.8638	1.0523	1.0181
.832	.7663	.8582	1.0583	1.0201
.780	.7663	.8562	1.0570	1.0196
.728	.7663	.8500	1.0532	1.0184
.676	.7570	.8463	1.0573	1.0197
.624	.7478	.8446	1.0628	1.0215
.572	.7432	.8428	1.0649	1.0222
.520	.7386	.8388	1.0657	1.0224
.468	.7293	.8372	1.0714	1.0243
.416	.7201	.8355	1.0772	1.0261
.364	.7155	.8316	1.0781	1.0264
.312	.7109	.8297	1.0804	1.0271
.260	.7155	.8275	1.0754	1.0255
.208	.7201	.8273	1.0718	1.0244
.156	.7201	.8273	1.0718	1.0244
.104	.7201	.8252	1.0705	1.0240
.052	.7201	.8232	1.0692	1.0236
0.000	.7201	.8252	1.0705	1.0240
-.104	.7201	.8221	1.0684	1.0233
-.156	.7339	.8215	1.0579	1.0199
-.208	.7478	.8209	1.0477	1.0166
-.260	.7339	.8215	1.0579	1.0199
-.312	.7478	.8250	1.0503	1.0174
-.364	.7478	.8250	1.0503	1.0174
-.416	.7478	.8312	1.0543	1.0187
-.468	.7478	.8353	1.0569	1.0196
-.520	.7478	.8373	1.0582	1.0200
-.572	.7524	.8392	1.0561	1.0193
-.624	.7570	.8431	1.0553	1.0191
-.676	.7524	.8454	1.0600	1.0206
-.728	.7478	.8518	1.0673	1.0229
-.780	.7570	.8555	1.0630	1.0216
-.832	.7663	.8572	1.0577	1.0198
-.884	.7755	.8650	1.0561	1.0193
-.936	.7847	.8667	1.0509	1.0176
-.988	.7986	.8722	1.0451	1.0157
-1.040	.8124	.8778	1.0395	1.0138

(r) x/D = 5.0; y/D = 1.5; $\alpha = 0^o$;

p_∞ = 51.78 psf (2479.03 N/m^2);
q_∞ = 317.55 psf (15204.18 N/m^2);
$p_{t,\infty}$ = 1790.90 psf (85748.75 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8033	.7838	.9878	.9955
.988	.7387	.7825	1.0292	1.0103
.936	.6740	.7812	1.0765	1.0259
.884	.6648	.7774	1.0814	1.0274
.832	.6556	.7717	1.0849	1.0285
.780	.6648	.7692	1.0757	1.0256
.728	.6740	.7647	1.0651	1.0223
.676	.6787	.7645	1.0614	1.0210
.624	.6833	.8486	1.1144	1.0374
.572	.8587	.9624	1.0586	1.0202
.520	1.0342	.9548	.9609	.9852
.468	1.0342	.9507	.9588	.9844
.416	1.0342	.9445	.9557	.9832
.364	1.0342	.9404	.9536	.9824
.312	1.0342	.9384	.9526	.9820
.260	1.0295	.9344	.9527	.9820
.208	1.0249	.9346	.9549	.9829
.156	1.0295	.9344	.9527	.9820
.104	1.0342	.9301	.9484	.9803
.052	1.0342	.9301	.9484	.9803
0.000	1.0342	.9301	.9484	.9803
-.104	1.0157	.9248	.9542	.9826
-.156	1.0203	.9267	.9530	.9821
-.208	1.0249	.9265	.9508	.9812
-.260	1.0111	.9292	.9586	.9844
-.312	1.0157	.9352	.9595	.9847
-.364	.9880	.9384	.9746	.9905
-.416	1.0065	.9438	.9684	.9882
-.468	.9788	.9471	.9837	.9940
-.520	.9511	.9565	1.0029	1.0010
-.572	.8310	.9246	1.0548	1.0189
-.624	.7110	.7834	1.0497	1.0172
-.676	.6787	.7580	1.0569	1.0196
-.728	.6463	.7615	1.0854	1.0287
-.780	.6510	.7633	1.0829	1.0279
-.832	.6556	.7673	1.0818	1.0275
-.884	.6602	.7732	1.0822	1.0277
-.936	.6648	.7792	1.0826	1.0278
-.988	.6740	.7830	1.0778	1.0263
-1.040	.6833	.7887	1.0744	1.0252

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(s) x/D = 5.0; y/D = 1.0; $\alpha = 0^\circ$;

p_∞ = 51.81 psf (2480.55 N/m^2);
q_∞ = 317.74 psf (15213.52 N/m^2);
$p_{t,\infty}$ = 1792.00 psf (85801.42 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1350	.9004	.8907	.9558
.988	1.0658	.8932	.9154	.9666
.936	.9966	.8818	.9406	.9772
.884	.9920	.8697	.9363	.9754
.832	.9874	.8575	.9319	.9736
.780	.9828	.8454	.9275	.9717
.728	.9782	.8292	.9207	.9689
.676	.9735	.8170	.9161	.9669
.624	.9689	.8028	.9103	.9644
.572	.9735	.7923	.9021	.9609
.520	.9782	.7819	.8940	.9573
.468	.9735	.7718	.8904	.9556
.416	.9689	.7617	.8866	.9540
.364	.9689	.7514	.8806	.9512
.312	.9689	.7432	.8758	.9490
.260	.9643	.7372	.8744	.9483
.208	.9597	.7312	.8729	.9477
.156	.9597	.7271	.8704	.9465
.104	.9597	.7230	.8680	.9454
.052	.9643	.7208	.8645	.9437
0.000	.9689	.7205	.8624	.9427
-.104	.9505	.7189	.8697	.9462
-.156	.9597	.7206	.8665	.9447
-.208	.9689	.7222	.8634	.9432
-.260	.9551	.7311	.8749	.9486
-.312	.9643	.7369	.8742	.9482
-.364	.9643	.7431	.8778	.9499
-.416	.9597	.7536	.8861	.9537
-.468	.9597	.7639	.8922	.9565
-.520	.9597	.7742	.8982	.9591
-.572	.9689	.7862	.9008	.9603
-.624	.9782	.8002	.9045	.9619
-.676	.9828	.8123	.9092	.9639
-.728	.9874	.8286	.9161	.9669
-.780	.9874	.8410	.9229	.9698
-.832	.9874	.8534	.9297	.9726
-.884	1.0012	.8672	.9307	.9730
-.936	1.0151	.8831	.9327	.9739
-.988	1.0289	.8907	.9304	.9730
-1.040	1.0428	.9045	.9314	.9733

(t) x/D = 5.0; y/D = 0.83; $\alpha = 0^\circ$;

p_∞ = 51.81 psf (2480.55 N/m^2);
q_∞ = 317.74 psf (15213.52 N/m^2);
$p_{t,\infty}$ = 1792.00 psf (85801.42 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1258	.8628	.8754	.9488
.988	1.0566	.8493	.8966	.9584
.936	.9874	.8380	.9212	.9691
.884	.9828	.8196	.9132	.9657
.832	.9782	.8013	.9051	.9622
.780	.9689	.7832	.8990	.9595
.728	.9597	.7671	.8940	.9573
.676	.9551	.7508	.8866	.9540
.624	.9505	.7366	.8803	.9511
.572	.9551	.7220	.8695	.9461
.520	.9597	.7094	.8598	.9415
.468	.9551	.6993	.8557	.9395
.416	.9505	.6893	.8516	.9375
.364	.9505	.6769	.8439	.9338
.312	.9505	.6707	.8400	.9319
.260	.9459	.6647	.8383	.9310
.208	.9412	.6608	.8379	.9308
.156	.9459	.6565	.8331	.9284
.104	.9505	.6542	.8296	.9267
.052	.9551	.6520	.8262	.9249
0.000	.9597	.6518	.8241	.9238
-.104	.9505	.6509	.8275	.9256
-.156	.9551	.6527	.8267	.9252
-.208	.9597	.6587	.8285	.9261
-.260	.9505	.6591	.8328	.9282
-.312	.9551	.6672	.8358	.9298
-.364	.9505	.6715	.8405	.9321
-.416	.9505	.6818	.8470	.9353
-.468	.9459	.6923	.8555	.9395
-.520	.9412	.7049	.8654	.9441
-.572	.9505	.7189	.8697	.9462
-.624	.9597	.7309	.8727	.9476
-.676	.9643	.7472	.8803	.9511
-.728	.9689	.7655	.8889	.9550
-.780	.9689	.7800	.8972	.9587
-.832	.9689	.7985	.9078	.9634
-.884	.9828	.8144	.9103	.9644
-.936	.9966	.8344	.9150	.9665
-.988	1.0105	.8482	.9162	.9670
-1.040	1.0243	.8641	.9185	.9679

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(u) $x/D = 5.0$; $y/D = 0.63$; $\alpha = 0^\circ$;

p_∞ = 51.83 psf (2481.52 N/m^2);
q_∞ = 317.87 psf (15219.46 N/m^2);
$p_{t,\infty}$ = 1792.70 psf (85834.94 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0880	.8086	.8621	.9426
.988	1.0234	.7910	.8791	.9505
.936	.9589	.7732	.8980	.9590
.884	.9543	.7509	.8870	.9541
.832	.9497	.7326	.8783	.9502
.780	.9451	.7122	.8681	.9454
.728	.9404	.6940	.8590	.9411
.676	.9404	.6775	.8488	.9362
.624	.9404	.6652	.8410	.9324
.572	.9451	.6547	.8323	.9280
.520	.9497	.6442	.8236	.9236
.468	.9451	.6362	.8205	.9220
.416	.9404	.6302	.8186	.9210
.364	.9404	.6200	.8119	.9175
.312	.9404	.6159	.8092	.9161
.260	.9358	.6099	.8073	.9151
.208	.9312	.6080	.8081	.9155
.156	.9358	.6017	.8018	.9122
.104	.9404	.5974	.7970	.9096
.052	.9404	.5953	.7956	.9088
0.000	.9404	.5932	.7942	.9081
-.104	.9312	.5917	.7971	.9096
-.156	.9404	.5974	.7970	.9096
-.208	.9497	.6032	.7970	.9096
-.260	.9358	.6059	.8046	.9137
-.312	.9451	.6117	.8045	.9136
-.364	.9404	.6160	.8093	.9162
-.416	.9404	.6222	.8134	.9183
-.468	.9358	.6306	.8209	.9222
-.520	.9312	.6391	.8284	.9261
-.572	.9358	.6471	.8316	.9276
-.624	.9404	.6593	.8373	.9305
-.676	.9404	.6737	.8464	.9350
-.728	.9404	.6923	.8580	.9406
-.780	.9404	.7088	.8681	.9454
-.832	.9404	.7273	.8794	.9507
-.884	.9543	.7473	.8849	.9532
-.936	.9681	.7714	.8927	.9567
-.988	.9819	.7894	.8966	.9584
-1.040	.9958	.8094	.9016	.9606

(v) $x/D = 5.0$; $y/D = 0.42$; $\alpha = 0^\circ$;

p_∞ = 51.79 psf (2479.72 N/m^2);
q_∞ = 317.63 psf (15208.43 N/m^2);
$p_{t,\infty}$ = 1791.40 psf (85772.69 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0710	.7616	.8432	.9335
.988	1.0064	.7438	.8597	.9415
.936	.9418	.7261	.8781	.9501
.884	.9418	.7055	.8655	.9442
.832	.9418	.6891	.8554	.9394
.780	.9418	.6705	.8438	.9337
.728	.9418	.6520	.8321	.9279
.676	.9418	.6376	.8228	.9232
.624	.9418	.6273	.8161	.9197
.572	.9418	.6191	.8108	.9169
.520	.9418	.6108	.8054	.9141
.468	.9372	.6028	.8020	.9123
.416	.9325	.5948	.7986	.9105
.364	.9279	.5867	.7952	.9086
.312	.9233	.5766	.7903	.9059
.260	.9187	.5604	.7810	.9008
.208	.9141	.5461	.7730	.8963
.156	.9187	.5253	.7562	.8866
.104	.9233	.5066	.7407	.8774
.052	.9233	.4942	.7316	.8719
0.000	.9233	.4859	.7255	.8681
-.104	.9141	.4979	.7380	.8758
-.156	.9233	.5140	.7461	.8807
-.208	.9325	.5322	.7554	.8862
-.260	.9233	.5532	.7741	.8969
-.312	.9325	.5673	.7799	.9002
-.364	.9325	.5817	.7898	.9057
-.416	.9325	.5879	.7940	.9080
-.468	.9325	.5962	.7996	.9110
-.520	.9325	.6065	.8065	.9147
-.572	.9325	.6148	.8119	.9175
-.624	.9325	.6230	.8174	.9204
-.676	.9372	.6373	.8246	.9241
-.728	.9418	.6515	.8317	.9277
-.780	.9372	.6661	.8431	.9334
-.832	.9325	.6829	.8557	.9395
-.884	.9372	.7012	.8650	.9440
-.936	.9418	.7196	.8741	.9482
-.988	.9510	.7377	.8808	.9513
-1.040	.9602	.7600	.8896	.9553

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(w) x/D = 5.0; y/D = 0.21; $\alpha = 0^\circ$;

p_∞ = 51.80 psf (2480.14 N/m^2);
q_∞ = 317.69 psf (15210.97 N/m^2);
$p_{t,\infty}$ = 1791.70 psf (85787.06 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0793	.7519	.8347	.9292
.988	1.0148	.7322	.8494	.9365
.936	.9502	.7145	.8671	.9450
.884	.9456	.6921	.8555	.9394
.832	.9410	.6758	.8475	.9355
.780	.9410	.6594	.8371	.9304
.728	.9410	.6409	.8253	.9245
.676	.9364	.6246	.8168	.9201
.624	.9317	.6125	.8108	.9169
.572	.9364	.6041	.8032	.9129
.520	.9410	.5936	.7942	.9081
.468	.9364	.5876	.7922	.9070
.416	.9317	.5775	.7873	.9043
.364	.9271	.5633	.7795	.9000
.312	.9225	.5471	.7701	.8947
.260	.9179	.5143	.7486	.8821
.208	.9133	.4878	.7308	.8714
.156	.9133	.4527	.7041	.8545
.104	.9133	.4301	.6862	.8427
.052	.9179	.4154	.6727	.8335
0.000	.9225	.4111	.6675	.8299
-.104	.9133	.4234	.6808	.8390
-.156	.9225	.4436	.6935	.8475
-.208	.9317	.4763	.7150	.8615
-.260	.9225	.5077	.7419	.8781
-.312	.9317	.5362	.7586	.8881
-.364	.9271	.5571	.7752	.8975
-.416	.9317	.5713	.7831	.9020
-.468	.9271	.5798	.7908	.9062
-.520	.9225	.5883	.7985	.9104
-.572	.9271	.6004	.8048	.9138
-.624	.9317	.6126	.8109	.9170
-.676	.9364	.6269	.8182	.9208
-.728	.9410	.6432	.8267	.9252
-.780	.9410	.6555	.8347	.9292
-.832	.9410	.6700	.8438	.9337
-.884	.9456	.6883	.8532	.9383
-.936	.9502	.7088	.8637	.9433
-.988	.9594	.7269	.8704	.9465
-1.040	.9686	.7492	.8795	.9507

(x) x/D = 5.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 51.81 psf (2480.83 N/m^2);
q_∞ = 317.78 psf (15215.22 N/m^2);
$p_{t,\infty}$ = 1792.20 psf (85811.00 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0795	.7455	.8310	.9274
.988	1.0150	.7237	.8444	.9341
.936	.9504	.7061	.8619	.9425
.884	.9458	.6836	.8502	.9369
.832	.9411	.6695	.8434	.9335
.780	.9411	.6530	.8330	.9284
.728	.9411	.6386	.8238	.9237
.676	.9365	.6286	.8192	.9213
.624	.9319	.6205	.8160	.9197
.572	.9365	.6121	.8084	.9157
.520	.9411	.6057	.8023	.9124
.468	.9365	.5998	.8003	.9114
.416	.9319	.5897	.7955	.9088
.364	.9273	.5776	.7892	.9054
.312	.9227	.5592	.7785	.8994
.260	.9181	.5306	.7603	.8890
.208	.9135	.5041	.7429	.8787
.156	.9135	.4732	.7197	.8645
.104	.9135	.4526	.7039	.8544
.052	.9181	.4380	.6907	.8457
0.000	.9227	.4315	.6839	.8411
-.104	.9135	.4563	.7068	.8562
-.156	.9227	.4745	.7171	.8628
-.208	.9319	.5009	.7332	.8728
-.260	.9227	.5282	.7566	.8869
-.312	.9319	.5526	.7700	.8946
-.364	.9273	.5734	.7864	.9038
-.416	.9319	.5856	.7927	.9073
-.468	.9273	.5920	.7990	.9107
-.520	.9227	.6005	.8067	.9148
-.572	.9227	.6067	.8109	.9170
-.624	.9227	.6149	.8164	.9199
-.676	.9273	.6250	.8210	.9222
-.728	.9319	.6351	.8255	.9246
-.780	.9319	.6475	.8336	.9286
-.832	.9319	.6599	.8415	.9326
-.884	.9365	.6782	.8510	.9373
-.936	.9411	.6986	.8616	.9423
-.988	.9504	.7168	.8685	.9456
-1.040	.9596	.7391	.8776	.9498

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(y) $x/D = 5.0$; $y/D = -0.42$; $\alpha = 0^\circ$;

p_∞ = 51.81 psf (2480.69 N/m^2);
q_∞ = 317.76 psf (15214.37 N/m^2);
$p_{t,\infty}$ = 1792.10 psf (85806.21 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0808	.7784	.8487	.9361
.988	1.0115	.7589	.8662	.9445
.936	.9422	.7373	.8846	.9530
.884	.9330	.7110	.8729	.9477
.832	.9238	.6888	.8635	.9432
.780	.9145	.6666	.8537	.9386
.728	.9053	.6464	.8450	.9343
.676	.9007	.6261	.8337	.9287
.624	.8960	.6119	.8264	.9250
.572	.9007	.5993	.8158	.9195
.520	.9053	.5868	.8051	.9139
.468	.9007	.5726	.7973	.9098
.416	.8960	.5564	.7880	.9047
.364	.9007	.5438	.7770	.8986
.312	.9053	.5806	.8009	.9117
.260	.9145	.5782	.7951	.9086
.208	.9238	.5777	.7908	.9062
.156	.9469	.5726	.7776	.8989
.104	.9699	.5613	.7607	.8893
.052	.9746	.5302	.7376	.8755
0.000	.9792	.5073	.7198	.8645
-.104	.9607	.5554	.7604	.8891
-.156	.9515	.5600	.7672	.8930
-.208	.9422	.5604	.7712	.8953
-.260	.9330	.5670	.7796	.9000
-.312	.9238	.5674	.7837	.9023
-.364	.9145	.5369	.7662	.8924
-.416	.9053	.5517	.7807	.9006
-.468	.8960	.5687	.7966	.9094
-.520	.8868	.5835	.8112	.9171
-.572	.8914	.5998	.8203	.9219
-.624	.8960	.6141	.8278	.9257
-.676	.9007	.6324	.8380	.9308
-.728	.9053	.6508	.8479	.9357
-.780	.9099	.6712	.8589	.9410
-.832	.9145	.6916	.8696	.9461
-.884	.9238	.7139	.8791	.9505
-.936	.9330	.7362	.8883	.9547
-.988	.9422	.7543	.8947	.9576
-1.040	.9515	.7786	.9046	.9620

(z) $x/D = 6.0$; $y/D = 0.0$; $\alpha = 0^\circ$;

p_∞ = 51.87 psf (2483.32 N/m^2);
q_∞ = 318.10 psf (15230.50 N/m^2);
$p_{t,\infty}$ = 1794.00 psf (85897.18 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0416	.7338	.8393	.9315
.988	.9817	.7117	.8515	.9375
.936	.9218	.6938	.8676	.9452
.884	.9172	.6755	.8582	.9407
.832	.9125	.6613	.8513	.9374
.780	.9172	.6488	.8410	.9324
.728	.9218	.6424	.8348	.9293
.676	.9356	.6335	.8229	.9232
.624	.9494	.6329	.8165	.9199
.572	.9955	.6350	.7987	.9105
.520	1.0416	.6350	.7808	.9007
.468	1.0646	.6339	.7716	.8956
.416	1.0877	.6288	.7603	.8890
.364	1.1015	.6178	.7489	.8824
.312	1.1153	.6048	.7364	.8748
.260	1.1107	.5741	.7189	.8640
.208	1.1061	.5475	.7035	.8541
.156	1.1107	.5184	.6832	.8406
.104	1.1153	.4975	.6679	.8301
.052	1.1107	.4791	.6568	.8223
0.000	1.1061	.4731	.6540	.8203
-.104	1.0877	.4994	.6776	.8368
-.156	1.0877	.5180	.6901	.8453
-.208	1.0877	.5470	.7091	.8577
-.260	1.0646	.5749	.7348	.8738
-.312	1.0646	.5955	.7479	.8817
-.364	1.0324	.6176	.7734	.8966
-.416	1.0416	.6254	.7749	.8974
-.468	1.0093	.6207	.7842	.9026
-.520	.9771	.6221	.7980	.9101
-.572	.9586	.6229	.8061	.9145
-.624	.9402	.6238	.8145	.9189
-.676	.9310	.6283	.8215	.9225
-.728	.9218	.6349	.8299	.9268
-.780	.9172	.6475	.8402	.9320
-.832	.9125	.6600	.8505	.9370
-.884	.9172	.6742	.8574	.9403
-.936	.9218	.6946	.8681	.9454
-.988	.9310	.7128	.8750	.9486
-1.040	.9402	.7350	.8842	.9528

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(aa) x/D = 7.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 51.86 psf (2483.18 N/m^2);
q_∞ = 318.08 psf (15229.65 N/m^2);
$p_{t,\infty}$ = 1793.90 psf (85892.39 N/m^2);

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3084	.8250	.7941	.9080
.988	1.2439	.8032	.8036	.9131
.936	1.1794	.7814	.8140	.9186
.884	1.1748	.7549	.8016	.9121
.832	1.1702	.7366	.7934	.9077
.780	1.1563	.7167	.7873	.9043
.728	1.1425	.7009	.7832	.9021
.676	1.1425	.6844	.7740	.8969
.624	1.1425	.6762	.7693	.8942
.572	1.1425	.6659	.7635	.8909
.520	1.1425	.6598	.7599	.8888
.468	1.1379	.6497	.7556	.8863
.416	1.1333	.6376	.7501	.8830
.364	1.1287	.6234	.7432	.8789
.312	1.1241	.6092	.7362	.8747
.260	1.1149	.5849	.7243	.8674
.208	1.1057	.5668	.7160	.8621
.156	1.1103	.5419	.6986	.8509
.104	1.1149	.5170	.6810	.8391
.052	1.1149	.5025	.6714	.8325
0.000	1.1149	.4943	.6659	.8287
-.104	1.1057	.5145	.6822	.8399
-.156	1.1057	.5352	.6957	.8490
-.208	1.1057	.5599	.7116	.8594
-.260	1.1057	.5847	.7272	.8692
-.312	1.1057	.6033	.7386	.8762
-.364	1.1057	.6218	.7499	.8829
-.416	1.1057	.6362	.7586	.8880
-.468	1.1057	.6486	.7659	.8923
-.520	1.1057	.6548	.7695	.8944
-.572	1.1195	.6645	.7704	.8949
-.624	1.1333	.6741	.7713	.8953
-.676	1.1471	.6859	.7732	.8965
-.728	1.1609	.6976	.7752	.8976
-.780	1.1563	.7143	.7860	.9036
-.832	1.1517	.7289	.7955	.9088
-.884	1.1656	.7510	.8027	.9126
-.936	1.1794	.7750	.8107	.9169
-.988	1.1978	.7989	.8167	.9200
-1.040	1.2162	.8269	.8246	.9241

(bb) x/D = 8.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 51.84 psf (2482.21 N/m^2);
q_∞ = 317.95 psf (15223.71 N/m^2);
$p_{t,\infty}$ = 1793.20 psf (85858.88 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2175	.7922	.8066	.9147
.988	1.1530	.7663	.8152	.9193
.936	1.0884	.7485	.8293	.9265
.884	1.0884	.7259	.8166	.9200
.832	1.0884	.7094	.8073	.9151
.780	1.0838	.6890	.7973	.9098
.728	1.0792	.6769	.7919	.9069
.676	1.0838	.6643	.7829	.9019
.624	1.0884	.6558	.7762	.8982
.572	1.0884	.6496	.7726	.8961
.520	1.0884	.6435	.7689	.8940
.468	1.0838	.6375	.7669	.8929
.416	1.0792	.6274	.7625	.8903
.364	1.0792	.6171	.7562	.8866
.312	1.0792	.6047	.7486	.8821
.260	1.0700	.5866	.7404	.8773
.208	1.0607	.5705	.7334	.8730
.156	1.0654	.5476	.7169	.8627
.104	1.0700	.5247	.7003	.8520
.052	1.0700	.5061	.6877	.8437
0.000	1.0700	.4999	.6835	.8409
-.104	1.0607	.5154	.6970	.8499
-.156	1.0607	.5340	.7095	.8580
-.208	1.0607	.5588	.7258	.8683
-.260	1.0561	.5796	.7408	.8775
-.312	1.0561	.5962	.7513	.8838
-.364	1.0561	.6106	.7604	.8891
-.416	1.0515	.6232	.7698	.8945
-.468	1.0515	.6294	.7737	.8967
-.520	1.0515	.6376	.7787	.8995
-.572	1.0607	.6434	.7788	.8996
-.624	1.0700	.6513	.7802	.9004
-.676	1.0746	.6593	.7833	.9021
-.728	1.0792	.6715	.7888	.9051
-.780	1.0746	.6861	.7991	.9107
-.832	1.0700	.6987	.8081	.9155
-.884	1.0792	.7168	.8150	.9192
-.936	1.0884	.7391	.8241	.9238
-.988	1.1023	.7591	.8299	.9268
-1.040	1.1161	.7853	.8388	.9313

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(cc) x/D = 8.39; y/D = 3.0; $\alpha = 0^\circ$;

p_∞ = 51.80 psf (2480.00 N/m^2);
q_∞ = 317.67 psf (15210.12 N/m^2);
$p_{t,\infty}$ = 1791.60 psf (85782.27 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9228	.9027	.9891	.9960
.988	.8674	.9051	1.0215	1.0077
.936	.8120	.9075	1.0571	1.0197
.884	.8074	.9056	1.0591	1.0203
.832	.8028	.9038	1.0610	1.0209
.780	.8074	.9036	1.0579	1.0199
.728	.8120	.9013	1.0535	1.0185
.676	.8028	.8976	1.0574	1.0198
.624	.7936	.8980	1.0638	1.0218
.572	.7936	.8980	1.0638	1.0218
.520	.7936	.8959	1.0625	1.0214
.468	.7844	.8963	1.0690	1.0235
.416	.7751	.8947	1.0743	1.0252
.364	.7751	.8947	1.0743	1.0252
.312	.7751	.8926	1.0731	1.0248
.260	.7798	.8924	1.0698	1.0238
.208	.7844	.8922	1.0665	1.0227
.156	.7798	.8924	1.0698	1.0238
.104	.7751	.8926	1.0731	1.0248
.052	.7798	.8883	1.0673	1.0230
0.000	.7844	.8881	1.0641	1.0219
-.104	.7751	.8844	1.0682	1.0232
-.156	.7890	.8859	1.0596	1.0205
-.208	.8028	.8832	1.0489	1.0170
-.260	.7844	.8861	1.0628	1.0215
-.312	.7982	.8855	1.0532	1.0184
-.364	.7982	.8855	1.0532	1.0184
-.416	.7936	.8857	1.0564	1.0194
-.468	.7936	.8857	1.0564	1.0194
-.520	.7936	.8877	1.0576	1.0198
-.572	.7936	.8877	1.0576	1.0198
-.624	.7936	.8898	1.0589	1.0202
-.676	.7844	.8922	1.0665	1.0227
-.728	.7751	.8967	1.0756	1.0256
-.780	.7798	.8965	1.0723	1.0245
-.832	.7844	.8963	1.0690	1.0235
-.884	.7936	.8959	1.0625	1.0214
-.936	.8028	.8997	1.0586	1.0201
-.988	.8074	.8995	1.0555	1.0191
-1.040	.8120	.9013	1.0535	1.0185

(dd) x/D = 8.39; y/D = 2.0; $\alpha = 0^\circ$;

p_∞ = 51.77 psf (2478.75 N/m^2);
q_∞ = 317.51 psf (15202.48 N/m^2);
$p_{t,\infty}$ = 1790.70 psf (85739.18 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0804	.9694	.9472	.9798
.988	1.0204	.9720	.9760	.9911
.936	.9604	.9725	1.0063	1.0023
.884	.9604	.9705	1.0052	1.0019
.832	.9604	.9705	1.0052	1.0019
.780	.9558	.9707	1.0078	1.0028
.728	.9512	.9709	1.0103	1.0037
.676	.9512	.9667	1.0082	1.0029
.624	.9512	.9647	1.0071	1.0026
.572	.9604	.9643	1.0020	1.0007
.520	.9696	.9618	.9960	.9985
.468	.9604	.9602	.9999	1.0000
.416	.9512	.9606	1.0049	1.0018
.364	.9512	.9585	1.0039	1.0014
.312	.9512	.9565	1.0028	1.0010
.260	.9465	.9546	1.0042	1.0015
.208	.9419	.9569	1.0079	1.0028
.156	.9465	.9546	1.0042	1.0015
.104	.9512	.9544	1.0017	1.0006
.052	.9512	.9544	1.0017	1.0006
0.000	.9512	.9523	1.0006	1.0002
-.104	.9327	.9460	1.0071	1.0026
-.156	.9419	.9456	1.0020	1.0007
-.208	.9512	.9452	.9969	.9989
-.260	.9327	.9460	1.0071	1.0026
-.312	.9419	.9456	1.0020	1.0007
-.364	.9419	.9456	1.0020	1.0007
-.416	.9327	.9460	1.0071	1.0026
-.468	.9327	.9460	1.0071	1.0026
-.520	.9327	.9460	1.0071	1.0026
-.572	.9373	.9458	1.0045	1.0016
-.624	.9419	.9518	1.0052	1.0019
-.676	.9419	.9538	1.0063	1.0023
-.728	.9419	.9538	1.0063	1.0023
-.780	.9419	.9559	1.0074	1.0027
-.832	.9419	.9559	1.0074	1.0027
-.884	.9465	.9557	1.0048	1.0017
-.936	.9512	.9617	1.0055	1.0020
-.988	.9604	.9613	1.0005	1.0002
-1.040	.9696	.9609	.9955	.9984

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(ee) x/D = 8.39; y/D = 1.5; $\alpha = 0^\circ$;

p_∞ = 51.78 psf (2479.03 N/m^2);
q_∞ = 317.55 psf (15204.18 N/m^2);
$p_{t,\infty}$ = 1790.90 psf (85748.75 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0706	.9336	.9338	.9744
.988	1.0106	.9362	.9625	.9859
.936	.9506	.9368	.9927	.9973
.884	.9506	.9327	.9905	.9965
.832	.9506	.9306	.9894	.9961
.780	.9506	.9286	.9883	.9957
.728	.9506	.9224	.9850	.9945
.676	.9506	.9183	.9828	.9937
.624	.9506	.9162	.9817	.9933
.572	.9552	.9119	.9771	.9915
.520	.9598	.9097	.9735	.9901
.468	.9552	.9078	.9749	.9906
.416	.9506	.9039	.9751	.9907
.364	.9506	.8977	.9718	.9895
.312	.9506	.8936	.9696	.9886
.260	.9460	.8918	.9709	.9891
.208	.9414	.8920	.9734	.9901
.156	.9414	.8899	.9723	.9897
.104	.9414	.8879	.9712	.9892
.052	.9460	.8877	.9687	.9883
0.000	.9506	.8875	.9662	.9873
-.104	.9322	.8800	.9716	.9894
-.156	.9414	.8796	.9666	.9875
-.208	.9506	.8813	.9628	.9860
-.260	.9322	.8821	.9728	.9898
-.312	.9414	.8838	.9689	.9884
-.364	.9368	.8840	.9714	.9893
-.416	.9322	.8842	.9739	.9903
-.468	.9275	.8905	.9798	.9925
-.520	.9229	.8928	.9835	.9939
-.572	.9275	.8967	.9832	.9938
-.624	.9322	.9006	.9829	.9937
-.676	.9322	.9047	.9852	.9945
-.728	.9322	.9089	.9874	.9954
-.780	.9322	.9109	.9885	.9958
-.832	.9322	.9130	.9897	.9962
-.884	.9368	.9169	.9893	.9961
-.936	.9414	.9208	.9890	.9960
-.988	.9506	.9225	.9851	.9945
-1.040	.9598	.9241	.9812	.9931

(ff) x/D = 8.39; y/D = 1.0; $\alpha = 0^\circ$;

p_∞ = 51.77 psf (2478.89 N/m^2);
q_∞ = 317.53 psf (15203.33 N/m^2);
$p_{t,\infty}$ = 1790.80 psf (85743.97 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1540	.9270	.8963	.9583
.988	1.1448	.9521	.9120	.9651
.936	1.1355	.9484	.9139	.9660
.884	1.1401	.9379	.9070	.9630
.832	1.1448	.9233	.8981	.9591
.780	1.1355	.9093	.8949	.9576
.728	1.1263	.8932	.8905	.9557
.676	1.1263	.8768	.8823	.9520
.624	1.1263	.8623	.8750	.9486
.572	1.1401	.8494	.8631	.9431
.520	1.1540	.8364	.8514	.9374
.468	1.1494	.8201	.8447	.9342
.416	1.1448	.8121	.8423	.9330
.364	1.1401	.8000	.8376	.9307
.312	1.1355	.7878	.8329	.9283
.260	1.1263	.7800	.8322	.9279
.208	1.1171	.7742	.8325	.9281
.156	1.1263	.7676	.8256	.9246
.104	1.1355	.7590	.8176	.9205
.052	1.1355	.7590	.8176	.9205
0.000	1.1355	.7610	.8187	.9210
-.104	1.1171	.7595	.8246	.9241
-.156	1.1124	.7639	.8286	.9262
-.208	1.1078	.7682	.8327	.9282
-.260	1.0986	.7707	.8376	.9306
-.312	1.0940	.7791	.8439	.9338
-.364	1.0940	.7853	.8473	.9354
-.416	1.0801	.7942	.8575	.9404
-.468	1.0801	.8086	.8652	.9441
-.520	1.0801	.8210	.8718	.9472
-.572	1.0986	.8346	.8716	.9471
-.624	1.1171	.8503	.8725	.9475
-.676	1.1217	.8646	.8779	.9500
-.728	1.1263	.8788	.8833	.9525
-.780	1.1171	.8916	.8934	.9570
-.832	1.1078	.9064	.9046	.9619
-.884	1.1078	.9188	.9107	.9646
-.936	1.1078	.9229	.9127	.9655
-.988	1.0663	.9206	.9292	.9724
-1.040	1.0247	.8956	.9349	.9748

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(gg) x/D = 8.39; y/D = 0.83; $\alpha = 0^\circ$;

p_∞ = 51.81 psf (2480.55 N/m^2);
q_∞ = 317.74 psf (15213.52 N/m^2);
$p_{t,\infty}$ = 1792.00 psf (85801.42 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2835	.9330	.8526	.9380
.988	1.2189	.9153	.8666	.9447
.936	1.1542	.9016	.8838	.9527
.884	1.1496	.8792	.8745	.9484
.832	1.1450	.8650	.8692	.9459
.780	1.1358	.8428	.8614	.9423
.728	1.1265	.8206	.8535	.9385
.676	1.1265	.8000	.8427	.9332
.624	1.1265	.7856	.8351	.9294
.572	1.1404	.7726	.8231	.9233
.520	1.1542	.7576	.8102	.9166
.468	1.1496	.7413	.8030	.9128
.416	1.1450	.7312	.7992	.9108
.364	1.1404	.7170	.7929	.9074
.312	1.1358	.7090	.7901	.9058
.260	1.1265	.7012	.7889	.9052
.208	1.1173	.6934	.7878	.9046
.156	1.1219	.6849	.7813	.9010
.104	1.1265	.6806	.7773	.8987
.052	1.1265	.6785	.7761	.8981
0.000	1.1265	.6765	.7749	.8974
-.104	1.1173	.6777	.7788	.8996
-.156	1.1127	.6820	.7829	.9019
-.208	1.1081	.6884	.7882	.9048
-.260	1.1034	.6927	.7923	.9071
-.312	1.0988	.7012	.7988	.9106
-.364	1.0942	.7076	.8042	.9134
-.416	1.0896	.7160	.8107	.9169
-.468	1.0850	.7286	.8195	.9215
-.520	1.0804	.7432	.8294	.9266
-.572	1.0988	.7589	.8311	.9274
-.624	1.1173	.7725	.8315	.9276
-.676	1.1265	.7927	.8388	.9313
-.728	1.1358	.8108	.8449	.9343
-.780	1.1265	.8318	.8593	.9413
-.832	1.1173	.8487	.8716	.9470
-.884	1.1311	.8728	.8784	.9502
-.936	1.1450	.8887	.8810	.9514
-.988	1.1635	.9044	.8816	.9517
-1.040	1.1819	.9200	.8823	.9520

(hh) x/D = 8.39; y/D = 0.63; $\alpha = 0^\circ$;

p_∞ = 51.76 psf (2478.48 N/m^2);
q_∞ = 317.48 psf (15200.79 N/m^2);
$p_{t,\infty}$ = 1790.50 psf (85729.60 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2739	.8683	.8256	.9246
.988	1.2093	.8465	.8366	.9302
.936	1.1447	.8308	.8519	.9377
.884	1.1401	.8042	.8399	.9318
.832	1.1355	.7838	.8309	.9273
.780	1.1308	.7614	.8205	.9220
.728	1.1262	.7389	.8100	.9165
.676	1.1262	.7204	.7998	.9111
.624	1.1262	.7039	.7906	.9061
.572	1.1308	.6913	.7819	.9013
.520	1.1355	.6829	.7755	.8977
.468	1.1308	.6707	.7701	.8947
.416	1.1262	.6606	.7659	.8923
.364	1.1216	.6464	.7591	.8884
.312	1.1170	.6342	.7535	.8851
.260	1.1031	.6204	.7499	.8829
.208	1.0893	.6086	.7475	.8815
.156	1.0985	.5958	.7365	.8749
.104	1.1078	.5872	.7280	.8697
.052	1.1031	.5791	.7245	.8675
0.000	1.0985	.5773	.7249	.8677
-.104	1.0893	.5749	.7265	.8687
-.156	1.0893	.5894	.7356	.8743
-.208	1.0893	.5998	.7420	.8782
-.260	1.0847	.6103	.7501	.8831
-.312	1.0847	.6248	.7589	.8882
-.364	1.0847	.6330	.7640	.8912
-.416	1.0801	.6477	.7744	.8971
-.468	1.0801	.6601	.7818	.9013
-.520	1.0801	.6725	.7891	.9053
-.572	1.0939	.6843	.7909	.9063
-.624	1.1078	.6981	.7939	.9079
-.676	1.1170	.7122	.7985	.9104
-.728	1.1262	.7324	.8064	.9146
-.780	1.1170	.7514	.8202	.9218
-.832	1.1078	.7704	.8339	.9288
-.884	1.1216	.7946	.8417	.9327
-.936	1.1355	.8208	.8502	.9369
-.988	1.1539	.8406	.8535	.9385
-1.040	1.1724	.8625	.8577	.9405

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(ii) x/D = 8.39; y/D = 0.42; $\alpha = 0^\circ$;

p_∞ = 51.81 psf (2480.83 N/m^2);
q_∞ = 317.78 psf (15215.22 N/m^2);
$p_{t,\infty}$ = 1792.20 psf (85811.00 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2448	.8193	.8113	.9172
.988	1.1848	.7973	.8203	.9219
.936	1.1249	.7753	.8302	.9269
.884	1.1203	.7467	.8164	.9199
.832	1.1157	.7284	.8080	.9155
.780	1.1065	.7061	.7989	.9106
.728	1.0972	.6880	.7919	.9068
.676	1.1018	.6734	.7818	.9012
.624	1.1065	.6629	.7740	.8969
.572	1.1111	.6503	.7650	.8918
.520	1.1157	.6398	.7573	.8873
.468	1.1111	.6276	.7516	.8839
.416	1.1065	.6114	.7433	.8790
.364	1.0972	.5953	.7366	.8749
.312	1.0880	.5813	.7309	.8715
.260	1.0834	.5588	.7182	.8635
.208	1.0788	.5384	.7064	.8560
.156	1.0834	.5175	.6912	.8460
.104	1.0880	.5049	.6812	.8393
.052	1.0834	.4989	.6786	.8375
0.000	1.0788	.4950	.6774	.8367
-.104	1.0696	.5023	.6853	.8420
-.156	1.0696	.5105	.6909	.8458
-.208	1.0696	.5250	.7006	.8522
-.260	1.0650	.5459	.7159	.8621
-.312	1.0650	.5624	.7267	.8688
-.364	1.0650	.5810	.7386	.8762
-.416	1.0604	.6039	.7546	.8857
-.468	1.0604	.6162	.7623	.8902
-.520	1.0604	.6307	.7712	.8953
-.572	1.0742	.6424	.7733	.8965
-.624	1.0880	.6521	.7742	.8970
-.676	1.0972	.6641	.7780	.8991
-.728	1.1065	.6822	.7852	.9032
-.780	1.0972	.6971	.7971	.9096
-.832	1.0880	.7160	.8112	.9172
-.884	1.1018	.7360	.8173	.9203
-.936	1.1157	.7601	.8254	.9245
-.988	1.1295	.7842	.8333	.9285
-1.040	1.1433	.8104	.8419	.9328

(jj) x/D = 8.39; y/D = 0.21; $\alpha = 0^\circ$;

p_∞ = 51.80 psf (2480.14 N/m^2);
q_∞ = 317.69 psf (15210.97 N/m^2);
$p_{t,\infty}$ = 1791.70 psf (85787.06 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2188	.8002	.8103	.9167
.988	1.1542	.7783	.8212	.9224
.936	1.0895	.7606	.8355	.9296
.884	1.0895	.7400	.8241	.9239
.832	1.0895	.7236	.8149	.9191
.780	1.0849	.7032	.8051	.9139
.728	1.0803	.6869	.7974	.9098
.676	1.0849	.6743	.7884	.9049
.624	1.0895	.6638	.7806	.9006
.572	1.0895	.6535	.7745	.8972
.520	1.0895	.6412	.7671	.8930
.468	1.0895	.6247	.7572	.8872
.416	1.0895	.6061	.7459	.8805
.364	1.0849	.5878	.7361	.8746
.312	1.0803	.5736	.7286	.8701
.260	1.0711	.5513	.7174	.8630
.208	1.0618	.5352	.7100	.8583
.156	1.0664	.5164	.6959	.8491
.104	1.0711	.5038	.6858	.8424
.052	1.0664	.4937	.6804	.8387
0.000	1.0618	.4898	.6792	.8379
-.104	1.0526	.5032	.6914	.8462
-.156	1.0526	.5135	.6985	.8508
-.208	1.0526	.5301	.7096	.8581
-.260	1.0526	.5445	.7193	.8642
-.312	1.0526	.5611	.7301	.8709
-.364	1.0526	.5796	.7421	.8783
-.416	1.0526	.6003	.7552	.8860
-.468	1.0526	.6168	.7655	.8920
-.520	1.0526	.6333	.7757	.8978
-.572	1.0618	.6473	.7808	.9007
-.624	1.0711	.6551	.7821	.9014
-.676	1.0757	.6673	.7876	.9045
-.728	1.0803	.6815	.7943	.9081
-.780	1.0757	.6941	.8033	.9130
-.832	1.0711	.7067	.8123	.9177
-.884	1.0757	.7250	.8210	.9223
-.936	1.0803	.7496	.8330	.9284
-.988	1.0941	.7654	.8364	.9301
-1.040	1.1080	.7895	.8442	.9339

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Concluded

(kk) x/D = 8.39; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 51.79 psf (2479.58 N/m^2);
q_∞ = 317.62 psf (15207.58 N/m^2);
$p_{t,\infty}$ = 1791.30 psf (85767.91 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1816	.7835	.8143	.9188
.988	1.1216	.7594	.8228	.9232
.936	1.0616	.7414	.8357	.9297
.884	1.0616	.7188	.8228	.9232
.832	1.0616	.7023	.8134	.9183
.780	1.0616	.6838	.8026	.9126
.728	1.0616	.6694	.7940	.9080
.676	1.0616	.6591	.7879	.9046
.624	1.0616	.6508	.7830	.9019
.572	1.0662	.6444	.7774	.8988
.520	1.0709	.6380	.7719	.8957
.468	1.0662	.6321	.7699	.8946
.416	1.0616	.6240	.7667	.8927
.364	1.0616	.6137	.7603	.8891
.312	1.0616	.6014	.7526	.8845
.260	1.0570	.5830	.7427	.8786
.208	1.0524	.5688	.7352	.8741
.156	1.0524	.5461	.7203	.8649
.104	1.0524	.5234	.7052	.8552
.052	1.0524	.5069	.6940	.8479
0.000	1.0524	.5007	.6897	.8450
-.104	1.0432	.5147	.7024	.8534
-.156	1.0432	.5313	.7137	.8606
-.208	1.0432	.5540	.7288	.8701
-.260	1.0385	.5749	.7440	.8794
-.312	1.0385	.5894	.7533	.8850
-.364	1.0385	.6059	.7638	.8911
-.416	1.0339	.6164	.7721	.8958
-.468	1.0339	.6247	.7773	.8987
-.520	1.0339	.6309	.7812	.9009
-.572	1.0385	.6369	.7831	.9020
-.624	1.0432	.6449	.7863	.9038
-.676	1.0524	.6528	.7876	.9045
-.728	1.0616	.6648	.7913	.9065
-.780	1.0524	.6776	.8024	.9125
-.832	1.0432	.6924	.8147	.9190
-.884	1.0524	.7127	.8229	.9232
-.936	1.0616	.7308	.8297	.9267
-.988	1.0709	.7510	.8375	.9306
-1.040	1.0801	.7733	.8462	.9349

(ll) x/D = 8.39; y/D = -0.42; $\alpha = 0^\circ$;

p_∞ = 51.79 psf (2479.72 N/m^2);
q_∞ = 317.63 psf (15208.43 N/m^2);
$p_{t,\infty}$ = 1791.40 psf (85772.69 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1262	.8044	.8452	.9344
.988	1.0616	.7887	.8620	.9425
.936	.9969	.7710	.8794	.9507
.884	.9969	.7463	.8652	.9441
.832	.9969	.7278	.8544	.9389
.780	.9969	.7010	.8386	.9311
.728	.9969	.6784	.8249	.9243
.676	.9969	.6578	.8123	.9177
.624	.9969	.6393	.8008	.9116
.572	1.0016	.6164	.7845	.9028
.520	1.0062	.5956	.7694	.8943
.468	1.0016	.5875	.7659	.8923
.416	.9969	.6290	.7943	.9081
.364	.9969	.6310	.7956	.9088
.312	.9969	.6269	.7930	.9074
.260	.9969	.6228	.7904	.9060
.208	.9969	.6207	.7891	.9053
.156	.9969	.6145	.7851	.9031
.104	.9969	.6001	.7759	.8979
.052	.9969	.5671	.7542	.8855
0.000	.9969	.5486	.7418	.8781
-.104	.9877	.5792	.7658	.8922
-.156	.9923	.6018	.7787	.8995
-.208	.9969	.6098	.7821	.9014
-.260	.9831	.6125	.7893	.9054
-.312	.9877	.6144	.7887	.9051
-.364	.9877	.6205	.7926	.9072
-.416	.9785	.6251	.7993	.9108
-.468	.9785	.5921	.7779	.8991
-.520	.9785	.5797	.7697	.8944
-.572	.9831	.6084	.7867	.9040
-.624	.9877	.6288	.7979	.9101
-.676	.9923	.6513	.8101	.9166
-.728	.9969	.6717	.8209	.9222
-.780	.9877	.6907	.8363	.9300
-.832	.9785	.7159	.8554	.9394
-.884	.9877	.7340	.8621	.9426
-.936	.9969	.7584	.8722	.9473
-.988	1.0062	.7786	.8797	.9508
-1.040	1.0154	.7988	.8870	.9541

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER)

(a) x/D = 1.0; y/D = 0.0; $\alpha = 0^o$;

p_∞ = 22.43 psf (1073.91 N/m^2);
q_∞ = 244.97 psf (11728.99 N/m^2);
$p_{t,\infty}$ = 3185.20 psf (152508.20 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.5137	.5843	.6213	.8494
.988	1.2472	.5376	.6565	.8703
.936	.9807	.5014	.7151	.9010
.884	.9168	.4683	.7147	.9008
.832	.8528	.4432	.7209	.9038
.780	.7888	.4208	.7304	.9082
.728	.7249	.4010	.7438	.9144
.676	.6929	.3858	.7462	.9155
.624	.6609	.3759	.7542	.9190
.572	.6076	.3665	.7767	.9286
.520	.5543	.3625	.8086	.9414
.468	.5010	.3531	.8395	.9527
.416	.4477	.3437	.8762	.9652
.364	.4690	.3325	.8420	.9536
.312	.4904	.2974	.7788	.9295
.260	.5437	.1197	.4693	.7334
.208	.5970	.0280	.2166	.4106
.156	.6076	.0077	.1123	.2236
.104	.6183	.0021	.0588	.1188
.052	.6076	.0077	.1123	.2236
0.000	.5970	.0085	.1196	.2375
−.104	.5970	.0169	.1684	.3277
−.156	.5863	.0050	.0923	.1849
−.208	.5756	.0103	.1338	.2643
−.260	.5650	.0622	.3319	.5812
−.312	.5543	.2160	.6243	.8513
−.364	.5756	.3063	.7295	.9078
−.416	.5330	.3367	.7948	.9360
−.468	.5543	.3469	.7911	.9345
−.520	.5756	.3544	.7846	.9319
−.572	.5756	.3650	.7963	.9366
−.624	.5756	.3704	.8021	.9389
−.676	.6396	.3822	.7730	.9271
−.728	.7036	.3993	.7534	.9187
−.780	.7675	.4164	.7366	.9111
−.832	.8315	.4389	.7266	.9065
−.884	.9061	.4638	.7154	.9011
−.936	.9807	.4993	.7136	.9002
−.988	1.0873	.5341	.7009	.8939
−1.040	1.1939	.5796	.6967	.8918

(b) x/D = 1.5; y/D = 0.0; $\alpha = 0^o$;

p_∞ = 22.43 psf (1073.91 N/m^2);
q_∞ = 244.97 psf (11728.99 N/m^2);
$p_{t,\infty}$ = 3185.20 psf (152508.20 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2789	.4988	.6245	.8514
.988	1.0338	.4649	.6706	.8781
.936	.7886	.4469	.7528	.9184
.884	.7460	.4213	.7515	.9178
.832	.7034	.4064	.7601	.9216
.780	.6608	.3941	.7723	.9268
.728	.6181	.3818	.7859	.9324
.676	.6075	.3714	.7819	.9308
.624	.5968	.3664	.7835	.9314
.572	.5648	.3618	.8003	.9382
.520	.5329	.3599	.8218	.9463
.468	.5116	.3578	.8363	.9516
.416	.4902	.3609	.8580	.9592
.364	.6821	.4229	.7874	.9330
.312	.8739	.4608	.7262	.9063
.260	1.1084	.4951	.6683	.8768
.208	1.3428	.4972	.6085	.8413
.156	1.4174	.3644	.5071	.7667
.104	1.4920	.2496	.4090	.6729
.052	1.5347	.2321	.3889	.6507
0.000	1.5773	.2525	.4001	.6633
−.104	1.5134	.2469	.4039	.6674
−.156	1.4494	.3296	.4768	.7403
−.208	1.3855	.4786	.5878	.8277
−.260	1.0444	.4978	.6904	.8886
−.312	.9805	.4646	.6884	.8876
−.364	.9698	.4275	.6639	.8744
−.416	.5755	.3517	.7817	.9307
−.468	.5648	.3466	.7834	.9314
−.520	.5542	.3469	.7912	.9345
−.572	.5435	.3498	.8022	.9389
−.624	.5329	.3581	.8197	.9456
−.676	.5755	.3650	.7964	.9366
−.728	.6181	.3747	.7786	.9294
−.780	.6394	.3822	.7731	.9271
−.832	.6608	.4004	.7784	.9293
−.884	.7034	.4153	.7684	.9252
−.936	.7460	.4383	.7665	.9244
−.988	.8100	.4635	.7564	.9200
−1.040	.8739	.4966	.7538	.9189

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(c) $x/D = 2.0$; $y/D = 0.0$; $\alpha = 0^o$;

p_∞ = 22.43 psf (1074.05 N/m^2);
q_∞ = 245.00 psf (11730.47 N/m^2);
$p_{t,\infty}$ = 3185.60 psf (152527.35 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1311	.4609	.6383	.8597
.988	.8963	.4373	.6985	.8927
.936	.6616	.4190	.7958	.9364
.884	.6402	.4035	.7938	.9356
.832	.6189	.3933	.7972	.9369
.780	.5975	.3858	.8035	.9394
.728	.5762	.3783	.8103	.9420
.676	.5762	.3730	.8046	.9398
.624	.5762	.3730	.8046	.9398
.572	.6509	.4486	.8302	.9494
.520	.7256	.4334	.7729	.9270
.468	.9070	.4290	.6877	.8872
.416	1.0884	.4993	.6773	.8817
.364	1.2804	.5480	.6542	.8689
.312	1.4725	.5539	.6133	.8444
.260	1.5045	.5371	.5975	.8341
.208	1.5365	.4908	.5652	.8119
.156	1.5259	.4134	.5205	.7778
.104	1.5152	.3654	.4911	.7530
.052	1.5365	.3460	.4745	.7382
0.000	1.5579	.3401	.4672	.7314
-.104	1.5365	.3675	.4891	.7512
-.156	1.5579	.4018	.5079	.7674
-.208	1.5792	.4736	.5476	.7990
-.260	1.2804	.5400	.6494	.8662
-.312	1.3018	.5555	.6532	.8684
-.364	1.1951	.5474	.6768	.8814
-.416	1.0244	.4662	.6746	.8802
-.468	.9177	.4261	.6814	.8839
-.520	.8109	.4314	.7293	.9078
-.572	.6829	.4478	.8098	.9418
-.624	.5549	.3682	.8146	.9436
-.676	.5655	.3679	.8066	.9406
-.728	.5762	.3703	.8017	.9387
-.780	.5869	.3781	.8026	.9390
-.832	.5975	.3885	.8063	.9405
-.884	.6189	.4013	.8053	.9401
-.936	.6402	.4168	.8069	.9407
-.988	.6722	.4347	.8042	.9396
-1.040	.7042	.4580	.8064	.9405

(d) $x/D = 2.5$; $y/D = 3.0$; $\alpha = 0^o$;

p_∞ = 22.45 psf (1074.89 N/m^2);
q_∞ = 245.19 psf (11739.67 N/m^2);
$p_{t,\infty}$ = 3188.19 psf (152647.05 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3651	1.0019	.8567	.9587
.988	1.1731	1.0091	.9275	.9808
.936	.9811	1.0110	1.0151	1.0036
.884	.9705	1.0112	1.0208	1.0049
.832	.9598	1.0115	1.0266	1.0063
.780	.9491	1.0118	1.0325	1.0076
.728	.9385	1.0120	1.0384	1.0089
.676	.9385	1.0093	1.0371	1.0086
.624	.9385	1.0093	1.0371	1.0086
.572	.9491	1.0091	1.0311	1.0073
.520	.9598	1.0062	1.0239	1.0056
.468	.9491	1.0064	1.0297	1.0070
.416	.9385	1.0067	1.0357	1.0083
.364	.9385	1.0067	1.0357	1.0083
.312	.9385	1.0067	1.0357	1.0083
.260	.9385	1.0040	1.0343	1.0080
.208	.9385	1.0067	1.0357	1.0083
.156	.9385	1.0067	1.0357	1.0083
.104	.9385	1.0067	1.0357	1.0083
.052	.9491	1.0064	1.0297	1.0070
0.000	.9598	1.0062	1.0239	1.0056
-.104	.9385	.9957	1.0300	1.0070
-.156	.9491	.9954	1.0241	1.0057
-.208	.9598	.9951	1.0182	1.0043
-.260	.9385	.9957	1.0300	1.0070
-.312	.9491	.9954	1.0241	1.0057
-.364	.9385	.9957	1.0300	1.0070
-.416	.9385	.9930	1.0286	1.0067
-.468	.9278	.9932	1.0347	1.0081
-.520	.9171	.9935	1.0408	1.0095
-.572	.9171	.9882	1.0380	1.0088
-.624	.9171	.9882	1.0380	1.0088
-.676	.9171	.9882	1.0380	1.0088
-.728	.9171	.9882	1.0380	1.0088
-.780	.9171	.9855	1.0366	1.0085
-.832	.9171	.9855	1.0366	1.0085
-.884	.9278	.9826	1.0291	1.0068
-.936	.9385	.9823	1.0231	1.0055
-.988	.9385	.9823	1.0231	1.0055
-1.040	.9385	.9797	1.0217	1.0051

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) - Continued

(e) $x/D = 2.5$; $y/D = 2.0$; $\alpha = 0^o$;

p_∞ = 22.46 psf (1075.26 N/m^2);
q_∞ = 245.27 psf (11743.72 N/m^2);
$p_{t,\infty}$ = 3189.20 psf (152699.72 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	2.1322	1.5966	.8653	.9616
.988	1.9936	1.5653	.8861	.9684
.936	1.8550	1.5473	.9133	.9767
.884	1.8017	1.5273	.9207	.9789
.832	1.7484	1.5073	.9285	.9811
.780	1.7697	1.4881	.9170	.9778
.728	1.7910	1.4637	.9040	.9739
.676	1.7377	1.4490	.9132	.9767
.624	1.6844	1.4316	.9219	.9792
.572	1.6951	1.4127	.9129	.9766
.520	1.7057	1.4018	.9066	.9747
.468	1.6951	1.3861	.9043	.9740
.416	1.6844	1.3704	.9020	.9733
.364	1.6524	1.3579	.9065	.9747
.312	1.6204	1.3506	.9130	.9766
.260	1.5991	1.3432	.9165	.9776
.208	1.5778	1.3357	.9201	.9787
.156	1.6098	1.3323	.9097	.9756
.104	1.6418	1.3262	.8988	.9723
.052	1.6204	1.3320	.9066	.9747
0.000	1.5991	1.3272	.9110	.9760
-.104	1.5991	1.3222	.9093	.9755
-.156	1.5991	1.3302	.9121	.9763
-.208	1.5991	1.3329	.9130	.9766
-.260	1.5245	1.3427	.9385	.9840
-.312	1.5245	1.3587	.9441	.9855
-.364	1.5138	1.3616	.9484	.9867
-.416	1.4499	1.3765	.9744	.9936
-.468	1.4392	1.3980	.9856	.9964
-.520	1.4285	1.4090	.9931	.9983
-.572	1.5885	1.4185	.9450	.9858
-.624	1.7484	1.4307	.9046	.9741
-.676	1.7804	1.4433	.9004	.9728
-.728	1.8123	1.4639	.8987	.9723
-.780	1.7377	1.4843	.9242	.9799
-.832	1.6631	1.4994	.9495	.9870
-.884	1.7590	1.5345	.9340	.9827
-.936	1.8550	1.5589	.9167	.9777
-.988	1.8656	1.5826	.9210	.9790
-1.040	1.8763	1.6064	.9253	.9802

(f) $x/D = 2.5$; $y/D = 1.5$; $\alpha = 0^o$;

p_∞ = 22.46 psf (1075.36 N/m^2);
q_∞ = 245.30 psf (11744.83 N/m^2);
$p_{t,\infty}$ = 3189.50 psf (152714.08 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.6831	1.1148	.8139	.9433
.988	1.4594	1.0829	.8614	.9603
.936	1.2357	1.0616	.9269	.9807
.884	1.2037	1.0331	.9264	.9805
.832	1.1718	1.0099	.9284	.9811
.780	1.1398	.9814	.9279	.9810
.728	1.1078	.9556	.9287	.9812
.676	1.0865	.9348	.9275	.9809
.624	1.0652	.9113	.9249	.9801
.572	1.0652	.8954	.9168	.9777
.520	1.0652	.8794	.9086	.9753
.468	1.0333	.8615	.9131	.9767
.416	1.0013	.8437	.9179	.9781
.364	.9907	.8280	.9142	.9770
.312	.9800	.8176	.9134	.9767
.260	.9694	.8045	.9110	.9760
.208	.9587	.7968	.9116	.9762
.156	.9481	.7917	.9138	.9769
.104	.9374	.7867	.9161	.9775
.052	.9374	.7867	.9161	.9775
0.000	.9374	.7840	.9145	.9771
-.104	.9161	.7827	.9243	.9799
-.156	.9374	.7902	.9181	.9781
-.208	.9587	.7950	.9106	.9759
-.260	.9374	.8035	.9258	.9804
-.312	.9587	.8137	.9213	.9790
-.364	.9587	.8190	.9243	.9799
-.416	.9587	.8350	.9333	.9825
-.468	.9587	.8536	.9436	.9854
-.520	.9587	.8696	.9524	.9878
-.572	1.0013	.8873	.9413	.9848
-.624	1.0439	.9049	.9310	.9819
-.676	1.0759	.9281	.9288	.9812
-.728	1.1078	.9540	.9280	.9810
-.780	1.1078	.9753	.9383	.9839
-.832	1.1078	.9966	.9485	.9867
-.884	1.1718	1.0324	.9386	.9840
-.936	1.2357	1.0628	.9274	.9808
-.988	1.2889	1.0856	.9177	.9780
-1.040	1.3422	1.1189	.9130	.9766

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(g) $x/D = 2.5$; $y/D = 1.0$; $\alpha = 0^\circ$;

$p_\infty = 22.44$ psf (1074.59 N/m^2);
$q_\infty = 245.12$ psf (11736.36 N/m^2);
$p_{t,\infty} = 3187.20$ psf (152603.96 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2997	.7226	.7456	.9152
.988	1.0866	.6878	.7956	.9363
.936	.8736	.6689	.8751	.9648
.884	.8416	.6404	.8723	.9639
.832	.8096	.6145	.8712	.9636
.780	.7883	.5884	.8639	.9612
.728	.7670	.5649	.8582	.9592
.676	.7457	.5468	.8563	.9586
.624	.7244	.5287	.8543	.9579
.572	.7138	.5129	.8477	.9556
.520	.7031	.4999	.8432	.9540
.468	.6818	.4897	.8475	.9556
.416	.6605	.4796	.8521	.9571
.364	.6605	.4663	.8402	.9530
.312	.6605	.4609	.8354	.9513
.260	.6712	.4527	.8213	.9461
.208	.6818	.4471	.8098	.9418
.156	.7777	.4421	.7540	.9189
.104	.8736	.4345	.7052	.8961
.052	.8949	.4286	.6921	.8895
0.000	.9162	.4281	.6836	.8850
-.104	.8736	.4296	.7013	.8942
-.156	.7670	.4322	.7507	.9175
-.208	.6605	.4401	.8163	.9443
-.260	.7777	.4400	.7522	.9181
-.312	.6712	.4506	.8193	.9454
-.364	.6712	.4559	.8242	.9472
-.416	.6818	.4663	.8270	.9482
-.468	.6818	.4770	.8364	.9516
-.520	.6818	.4903	.8480	.9557
-.572	.6925	.5034	.8526	.9573
-.624	.7031	.5191	.8593	.9596
-.676	.7138	.5402	.8700	.9632
-.728	.7244	.5586	.8781	.9658
-.780	.7457	.5794	.8815	.9669
-.832	.7670	.6002	.8846	.9679
-.884	.7990	.6315	.8890	.9693
-.936	.8310	.6600	.8912	.9700
-.988	.8736	.6830	.8842	.9678
-1.040	.9162	.7193	.8861	.9684

(h) $x/D = 2.5$; $y/D = 0.83$; $\alpha = 0^\circ$;

$p_\infty = 22.45$ psf (1074.75 N/m^2);
$q_\infty = 245.16$ psf (11738.20 N/m^2);
$p_{t,\infty} = 3187.70$ psf (152627.90 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2153	.6286	.7192	.9029
.988	1.0021	.5965	.7715	.9265
.936	.7889	.5750	.8537	.9577
.884	.7569	.5491	.8517	.9570
.832	.7249	.5259	.8517	.9570
.780	.7143	.5049	.8407	.9532
.728	.7036	.4811	.8269	.9482
.676	.6823	.4683	.8285	.9488
.624	.6610	.4555	.8302	.9494
.572	.6503	.4425	.8249	.9475
.520	.6397	.4321	.8219	.9464
.468	.7463	.4188	.7492	.9168
.416	.8529	.4109	.6941	.8905
.364	.8849	.4048	.6764	.8812
.312	.9168	.3987	.6594	.8719
.260	.8955	.3992	.6677	.8765
.208	.8742	.3971	.6739	.8799
.156	.9062	.3963	.6613	.8729
.104	.9382	.3928	.6471	.8649
.052	.9275	.3877	.6466	.8646
0.000	.9168	.3880	.6505	.8669
-.104	.9168	.3831	.6464	.8645
-.156	.8529	.3847	.6716	.8786
-.208	.7889	.3889	.7022	.8946
-.260	.7782	.3892	.7072	.8971
-.312	.7143	.3961	.7447	.9148
-.364	.7143	.3961	.7447	.9148
-.416	.6397	.4086	.7992	.9377
-.468	.6397	.4139	.8044	.9397
-.520	.6397	.4219	.8121	.9427
-.572	.6397	.4326	.8224	.9465
-.624	.6397	.4432	.8324	.9502
-.676	.6503	.4590	.8401	.9530
-.728	.6610	.4747	.8475	.9555
-.780	.6823	.4929	.8499	.9564
-.832	.7036	.5137	.8544	.9579
-.884	.7249	.5345	.8587	.9594
-.936	.7463	.5633	.8688	.9628
-.988	.7782	.5892	.8701	.9632
-1.040	.8102	.6204	.8751	.9648

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(i) $x/D = 2.5$; $y/D = 0.63$; $\alpha = 0^0$;

$p_\infty = 22.42$ psf (1073.61 N/m^2);
$q_\infty = 244.90$ psf (11725.68 N/m^2);
$p_{t,\infty} = 3184.30$ psf (152465.11 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1328	.5439	.6929	.8899
.988	.9190	.5117	.7462	.9155
.936	.7053	.4955	.8382	.9523
.884	.6839	.4720	.8308	.9496
.832	.6626	.4565	.8301	.9494
.780	.6412	.4384	.8268	.9482
.728	.6198	.4255	.8286	.9488
.676	.6198	.4175	.8207	.9459
.624	.6198	.4068	.8102	.9419
.572	.6091	.4018	.8121	.9427
.520	.5984	.3967	.8141	.9435
.468	.5771	.3918	.8240	.9471
.416	.5557	.3924	.8403	.9530
.364	.5878	.3916	.8162	.9442
.312	.6198	.3935	.7968	.9368
.260	.6733	.4242	.7938	.9356
.208	.7267	.4897	.8209	.9460
.156	.9404	.5299	.7506	.9175
.104	1.1542	.5407	.6845	.8855
.052	1.1648	.5404	.6812	.8838
0.000	1.1755	.5402	.6779	.8820
-.104	1.1542	.5354	.6811	.8837
-.156	1.0152	.5121	.7102	.8986
-.208	.8763	.4647	.7282	.9072
-.260	.8870	.4057	.6763	.8812
-.312	.7481	.3824	.7149	.9009
-.364	.7374	.3800	.7178	.9023
-.416	.6198	.3828	.7859	.9324
-.468	.6091	.3857	.7958	.9364
-.520	.5984	.3887	.8059	.9403
-.572	.5984	.3940	.8114	.9424
-.624	.5984	.3993	.8169	.9445
-.676	.5984	.4073	.8250	.9475
-.728	.5984	.4180	.8358	.9514
-.780	.6091	.4311	.8413	.9534
-.832	.6198	.4469	.8491	.9561
-.884	.6412	.4677	.8541	.9578
-.936	.6626	.4912	.8610	.9602
-.988	.6946	.5118	.8584	.9593
-1.040	.7267	.5377	.8602	.9599

(j) $x/D = 2.5$; $y/D = 0.42$; $\alpha = 0^0$;

$p_\infty = 22.46$ psf (1075.53 N/m^2);
$q_\infty = 245.33$ psf (11746.67 N/m^2);
$p_{t,\infty} = 3190.00$ psf (152738.02 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1079	.4869	.6629	.8739
.988	.8949	.4628	.7192	.9029
.936	.6818	.4494	.8118	.9426
.884	.6605	.4313	.8080	.9411
.832	.6392	.4185	.8091	.9415
.780	.6285	.4081	.8057	.9403
.728	.6179	.4003	.8049	.9399
.676	.6179	.3950	.7996	.9379
.624	.6179	.3924	.7969	.9368
.572	.7244	.3898	.7335	.9097
.520	.8309	.4165	.7080	.8975
.468	1.0547	.5575	.7270	.9067
.416	1.2784	.5467	.6539	.8688
.364	1.2997	.5381	.6435	.8628
.312	1.3210	.5349	.6364	.8586
.260	1.3103	.5299	.6359	.8583
.208	1.2997	.5248	.6354	.8580
.156	1.3103	.5165	.6279	.8534
.104	1.3210	.5083	.6203	.8488
.052	1.3103	.5032	.6197	.8484
0.000	1.2997	.5035	.6224	.8501
-.104	1.2997	.5067	.6244	.8513
-.156	1.3103	.5118	.6250	.8517
-.208	1.3210	.5169	.6255	.8520
-.260	1.2784	.5233	.6398	.8606
-.312	1.2890	.5284	.6402	.8609
-.364	1.0014	.5408	.7348	.9103
-.416	1.2571	.5398	.6553	.8696
-.468	.9694	.5415	.7474	.9160
-.520	.6818	.3939	.7601	.9216
-.572	.6392	.3843	.7754	.9281
-.624	.5966	.3853	.8037	.9395
-.676	.5966	.3880	.8064	.9405
-.728	.5966	.3933	.8120	.9426
-.780	.6072	.3984	.8100	.9419
-.832	.6179	.4115	.8160	.9442
-.884	.6285	.4219	.8193	.9454
-.936	.6392	.4403	.8299	.9493
-.988	.6605	.4584	.8331	.9504
-1.040	.6818	.4819	.8407	.9532

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(k) x/D = 2.5; y/D = 0.21; $\alpha = 0^\circ$;

p_∞ = 22.45 psf (1074.69 N/m^2);
q_∞ = 245.14 psf (11737.46 N/m^2);
$p_{t,\infty}$ = 3187.50 psf (152618.32 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0673	.4568	.6542	.8690
.988	.8539	.4380	.7162	.9015
.936	.6404	.4245	.8142	.9435
.884	.6191	.4117	.8155	.9440
.832	.5977	.4016	.8197	.9455
.780	.5870	.3938	.8191	.9453
.728	.5764	.3914	.8241	.9472
.676	.6297	.3901	.7871	.9329
.624	.6831	.5302	.8810	.9667
.572	.9926	.5494	.7439	.9145
.520	1.3022	.5364	.6418	.8618
.468	1.3022	.5284	.6370	.8590
.416	1.3022	.5231	.6338	.8570
.364	1.3022	.5177	.6306	.8551
.312	1.3022	.5071	.6240	.8511
.260	1.2808	.4755	.6093	.8419
.208	1.2595	.4387	.5902	.8293
.156	1.2595	.3879	.5549	.8044
.104	1.2595	.3477	.5254	.7817
.052	1.2488	.3239	.5093	.7685
0.000	1.2381	.3188	.5074	.7670
-.104	1.2381	.3487	.5307	.7859
-.156	1.2595	.3856	.5533	.8032
-.208	1.2808	.4360	.5834	.8247
-.260	1.2595	.4793	.6169	.8467
-.312	1.2808	.5055	.6282	.8537
-.364	1.2595	.5141	.6389	.8601
-.416	1.2808	.5189	.6365	.8586
-.468	1.2595	.5274	.6471	.8649
-.520	1.2381	.5333	.6563	.8701
-.572	1.0033	.5444	.7366	.9111
-.624	.7685	.4086	.7292	.9077
-.676	.6831	.3813	.7471	.9159
-.728	.5977	.3833	.8009	.9384
-.780	.5977	.3887	.8064	.9405
-.832	.5977	.3967	.8147	.9437
-.884	.5977	.4047	.8229	.9467
-.936	.5977	.4180	.8363	.9516
-.988	.6191	.4336	.8369	.9518
-1.040	.6404	.4544	.8423	.9537

(l) x/D = 2.5; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 22.47 psf (1075.73 N/m^2);
q_∞ = 245.38 psf (11748.88 N/m^2);
$p_{t,\infty}$ = 3190.60 psf (152766.75 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0663	.4484	.6484	.8657
.988	.8530	.4296	.7097	.8983
.936	.6398	.4188	.8091	.9415
.884	.6185	.4087	.8129	.9430
.832	.5971	.4012	.8197	.9455
.780	.6718	.4633	.8305	.9495
.728	.7464	.4482	.7749	.9279
.676	.7784	.4288	.7422	.9137
.624	.8104	.4546	.7490	.9167
.572	1.0663	.5337	.7075	.8972
.520	1.3222	.5380	.6379	.8595
.468	1.3222	.5380	.6379	.8595
.416	1.3222	.5327	.6347	.8576
.364	1.3222	.5220	.6283	.8537
.312	1.3222	.5060	.6186	.8478
.260	1.3009	.4745	.6040	.8384
.208	1.2796	.4430	.5884	.8281
.156	1.2689	.4006	.5619	.8095
.104	1.2582	.3768	.5472	.7987
.052	1.2582	.3607	.5354	.7896
0.000	1.2582	.3500	.5274	.7833
-.104	1.2582	.3795	.5492	.8001
-.156	1.2796	.3976	.5574	.8063
-.208	1.3009	.4372	.5797	.8221
-.260	1.2796	.4777	.6110	.8430
-.312	1.3009	.5039	.6224	.8501
-.364	1.2689	.5207	.6406	.8611
-.416	1.3009	.5306	.6386	.8599
-.468	1.2689	.5340	.6487	.8658
-.520	1.2369	.5348	.6576	.8709
-.572	1.0023	.5033	.7086	.8978
-.624	.7677	.4237	.7429	.9140
-.676	.7784	.4288	.7422	.9137
-.728	.7891	.4445	.7506	.9174
-.780	.6931	.4655	.8195	.9455
-.832	.5971	.3932	.8115	.9424
-.884	.5971	.3985	.8169	.9445
-.936	.5971	.4118	.8305	.9495
-.988	.6185	.4246	.8286	.9488
-1.040	.6398	.4454	.8344	.9509

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(m) x/D = 2.5; y/D = -0.42; $\alpha = 0^o$;

p_∞ = 22.46 psf (1075.23 N/m^2);
q_∞ = 245.27 psf (11743.35 N/m^2);
$p_{t,\infty}$ = 3189.10 psf (152694.93 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1729	.5733	.6991	.8931
.988	.9917	.5298	.7309	.9085
.936	.8104	.4969	.7831	.9313
.884	.7677	.4660	.7791	.9296
.832	.7251	.4431	.7817	.9307
.780	.6824	.4202	.7846	.9319
.728	.6398	.4052	.7958	.9364
.676	.6398	.3946	.7853	.9322
.624	.6398	.3919	.7827	.9311
.572	.5971	.3770	.7945	.9359
.520	.5545	.3567	.8020	.9388
.468	.7038	.3318	.6866	.8866
.416	.8530	.4693	.7417	.9135
.364	1.0663	.5094	.6911	.8890
.312	1.2796	.5227	.6392	.8602
.260	1.3009	.5222	.6336	.8569
.208	1.3222	.5163	.6249	.8516
.156	1.3222	.5083	.6201	.8486
.104	1.3222	.5083	.6201	.8486
.052	1.3222	.4737	.5985	.8349
0.000	1.3222	.3882	.5419	.7946
-.104	1.3222	.5036	.6172	.8468
-.156	1.3435	.5031	.6119	.8435
-.208	1.3649	.5079	.6100	.8423
-.260	.9810	.5254	.7318	.9089
-.312	1.0023	.5248	.7236	.9051
-.364	.9597	.5126	.7308	.9085
-.416	.6398	.3097	.6958	.8913
-.468	.5971	.3294	.7427	.9139
-.520	.5545	.3518	.7965	.9366
-.572	.5651	.3755	.8151	.9438
-.624	.5758	.3912	.8243	.9472
-.676	.6078	.3958	.8070	.9407
-.728	.6398	.4030	.7937	.9355
-.780	.6718	.4182	.7890	.9337
-.832	.7038	.4415	.7920	.9349
-.884	.7464	.4671	.7910	.9345
-.936	.7891	.5007	.7966	.9367
-.988	.7677	.5385	.8375	.9520
-1.040	.7464	.5630	.8685	.9627

(n) x/D = 3.0; y/D = 0.0; $\alpha = 0^o$;

p_∞ = 22.46 psf (1075.46 N/m^2);
q_∞ = 245.32 psf (11745.93 N/m^2);
$p_{t,\infty}$ = 3189.80 psf (152728.45 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0649	.4533	.6525	.8680
.988	.9371	.5071	.7356	.9107
.936	.8093	.4862	.7751	.9280
.884	.7880	.4628	.7663	.9243
.832	.7667	.4500	.7661	.9242
.780	.9478	.5574	.7669	.9245
.728	1.1288	.5503	.6982	.8926
.676	1.1394	.5341	.6846	.8856
.624	1.1501	.5258	.6762	.8811
.572	1.1714	.5173	.6645	.8748
.520	1.1927	.5088	.6531	.8683
.468	1.1714	.4987	.6525	.8680
.416	1.1501	.4885	.6517	.8675
.364	1.1394	.4808	.6496	.8663
.312	1.1288	.4624	.6400	.8607
.260	1.1181	.4387	.6264	.8525
.208	1.1075	.4149	.6121	.8436
.156	1.0968	.3885	.5952	.8326
.104	1.0862	.3701	.5837	.8249
.052	1.0862	.3568	.5731	.8175
0.000	1.0862	.3488	.5667	.8130
-.104	1.0862	.3737	.5865	.8268
-.156	1.1075	.3865	.5908	.8297
-.208	1.1288	.4100	.6027	.8376
-.260	1.1075	.4373	.6284	.8538
-.312	1.1288	.4581	.6371	.8590
-.364	1.1288	.4768	.6500	.8665
-.416	1.1288	.4875	.6572	.8706
-.468	1.1288	.4955	.6626	.8737
-.520	1.1288	.5062	.6697	.8776
-.572	1.1501	.5110	.6666	.8759
-.624	1.1714	.5212	.6670	.8761
-.676	1.1607	.5321	.6771	.8816
-.728	1.1501	.5431	.6872	.8869
-.780	.9584	.4944	.7182	.9025
-.832	.7667	.4430	.7601	.9216
-.884	.7880	.4585	.7628	.9228
-.936	.8093	.4847	.7739	.9275
-.988	.7241	.5081	.8376	.9521
-1.040	.6389	.4488	.8381	.9522

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(o) $x/D = 4.0$; $y/D = 0.0$; $\alpha = 0^o$;

p_∞ = 22.45 psf (1074.86 N/m^2);
q_∞ = 245.18 psf (11739.30 N/m^2);
$p_{t,\infty}$ = 3188.00 psf (152642.26 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.4510	.6234	.6555	.8697
.988	1.2483	.5910	.6881	.8874
.936	1.0456	.5667	.7362	.9109
.884	1.0242	.5405	.7264	.9064
.832	1.0029	.5224	.7217	.9041
.780	.9922	.5066	.7145	.9007
.728	.9816	.4909	.7072	.8971
.676	.9709	.4805	.7035	.8952
.624	.9602	.4700	.6997	.8933
.572	.9602	.4647	.6957	.8913
.520	.9602	.4567	.6897	.8882
.468	.9389	.4492	.6917	.8893
.416	.9176	.4417	.6939	.8904
.364	.9176	.4311	.6854	.8860
.312	.9176	.4177	.6747	.8803
.260	.9069	.3966	.6613	.8730
.208	.8962	.3836	.6542	.8690
.156	.8962	.3675	.6404	.8610
.104	.8962	.3569	.6310	.8554
.052	.8962	.3435	.6191	.8480
0.000	.8962	.3382	.6143	.8450
-.104	.8962	.3515	.6263	.8525
-.156	.9069	.3646	.6341	.8572
-.208	.9176	.3804	.6438	.8630
-.260	.9069	.3966	.6613	.8730
-.312	.9176	.4124	.6704	.8780
-.364	.9176	.4257	.6812	.8838
-.416	.9176	.4364	.6897	.8882
-.468	.9176	.4471	.6980	.8925
-.520	.9176	.4524	.7022	.8946
-.572	.9389	.4572	.6978	.8924
-.624	.9602	.4674	.6977	.8923
-.676	.9602	.4780	.7056	.8963
-.728	.9602	.4887	.7134	.9002
-.780	.9709	.5018	.7189	.9028
-.832	.9816	.5175	.7261	.9063
-.884	1.0136	.5354	.7268	.9066
-.936	1.0456	.5587	.7310	.9085
-.988	1.0669	.5821	.7387	.9121
-1.040	1.0883	.6163	.7525	.9183

(p) $x/D = 5.0$; $y/D = 3.0$; $\alpha = 0^o$;

p_∞ = 22.46 psf (1075.46 N/m^2);
q_∞ = 245.32 psf (11745.93 N/m^2);
$p_{t,\infty}$ = 3189.80 psf (152728.45 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.9412	1.4027	.8501	.9564
.988	1.7598	1.4017	.8925	.9704
.936	1.5785	1.4007	.9420	.9849
.884	1.5572	1.3933	.9459	.9860
.832	1.5359	1.3858	.9499	.9871
.780	1.5252	1.3754	.9496	.9870
.728	1.5145	1.3676	.9503	.9872
.676	1.5039	1.3599	.9509	.9874
.624	1.4932	1.3495	.9507	.9873
.572	1.5145	1.3437	.9419	.9849
.520	1.5359	1.3432	.9352	.9830
.468	1.5359	1.3352	.9324	.9822
.416	1.5359	1.3325	.9314	.9820
.364	1.5145	1.3250	.9353	.9831
.312	1.4932	1.3229	.9412	.9847
.260	1.4719	1.3207	.9473	.9864
.208	1.4505	1.3185	.9534	.9881
.156	1.4612	1.3156	.9489	.9868
.104	1.4719	1.3154	.9453	.9859
.052	1.4719	1.3180	.9463	.9861
0.000	1.4719	1.3154	.9453	.9859
-.104	1.4719	1.3074	.9425	.9851
-.156	1.4399	1.3108	.9541	.9883
-.208	1.4079	1.3142	.9662	.9915
-.260	1.3972	1.3145	.9699	.9925
-.312	1.3652	1.3206	.9835	.9959
-.364	1.3545	1.3208	.9875	.9969
-.416	1.3225	1.3242	1.0006	1.0002
-.468	1.3119	1.3351	1.0088	1.0021
-.520	1.3012	1.3381	1.0141	1.0034
-.572	1.3972	1.3385	.9787	.9947
-.624	1.4932	1.3415	.9478	.9866
-.676	1.5145	1.3463	.9428	.9852
-.728	1.5359	1.3538	.9389	.9841
-.780	1.4932	1.3628	.9553	.9886
-.832	1.4505	1.3638	.9696	.9924
-.884	1.5039	1.3732	.9556	.9887
-.936	1.5572	1.3826	.9423	.9850
-.988	1.5785	1.3927	.9393	.9842
-1.040	1.5999	1.3976	.9346	.9829

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(q) x/D = 5.0; y/D = 2.0; $\alpha = 0^o$;

p_∞ = 22.47 psf (1075.63 N/m^2);
q_∞ = 245.36 psf (11747.77 N/m^2);
$p_{t,\infty}$ = 3190.30 psf (152752.39 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3632	.9422	.8314	.9498
.988	1.1502	.9367	.9024	.9734
.936	.9372	.9311	.9967	.9992
.884	.9265	.9207	.9968	.9992
.832	.9159	.9156	.9999	1.0000
.780	.8946	.9055	1.0061	1.0015
.728	.8733	.8953	1.0125	1.0030
.676	.8733	.8873	1.0080	1.0019
.624	.8733	.8793	1.0035	1.0008
.572	.8733	.8740	1.0004	1.0001
.520	.8733	.8660	.9958	.9990
.468	.8520	.8612	1.0054	1.0013
.416	.8307	.8564	1.0154	1.0037
.364	.8307	.8484	1.0106	1.0025
.312	.8307	.8457	1.0090	1.0022
.260	.8200	.8433	1.0141	1.0034
.208	.8094	.8409	1.0193	1.0046
.156	.8094	.8382	1.0177	1.0042
.104	.8094	.8329	1.0144	1.0034
.052	.8094	.8329	1.0144	1.0034
0.000	.8094	.8329	1.0144	1.0034
-.104	.8094	.8276	1.0112	1.0027
-.156	.8200	.8300	1.0061	1.0015
-.208	.8307	.8298	.9994	.9999
-.260	.8200	.8327	1.0077	1.0018
-.312	.8307	.8377	1.0042	1.0010
-.364	.8200	.8380	1.0109	1.0026
-.416	.8307	.8404	1.0058	1.0014
-.468	.8200	.8486	1.0173	1.0041
-.520	.8094	.8542	1.0273	1.0064
-.572	.8200	.8566	1.0221	1.0052
-.624	.8307	.8644	1.0201	1.0048
-.676	.8413	.8694	1.0166	1.0039
-.728	.8520	.8798	1.0162	1.0039
-.780	.8626	.8849	1.0128	1.0031
-.832	.8733	.8900	1.0095	1.0023
-.884	.8946	.9001	1.0031	1.0007
-.936	.9159	.9129	.9984	.9996
-.988	.9265	.9207	.9968	.9992
-1.040	.9372	.9284	.9953	.9989

(r) x/D = 5.0; y/D = 1.5; $\alpha = 0^o$;

p_∞ = 22.47 psf (1075.80 N/m^2);
q_∞ = 245.40 psf (11749.61 N/m^2);
$p_{t,\infty}$ = 3190.80 psf (152776.33 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1497	.7625	.8144	.9436
.988	.9475	.7514	.8906	.9698
.936	.7452	.7483	1.0021	1.0005
.884	.7239	.7355	1.0080	1.0019
.832	.7026	.7280	1.0179	1.0043
.780	.7026	.7200	1.0123	1.0029
.728	.7026	.7094	1.0048	1.0012
.676	.6920	.7016	1.0070	1.0017
.624	.6813	.6939	1.0092	1.0022
.572	.6813	.6859	1.0034	1.0008
.520	.6813	.6806	.9995	.9999
.468	.6600	.6758	1.0119	1.0028
.416	.6387	.6710	1.0249	1.0059
.364	.6387	.6630	1.0188	1.0045
.312	.6387	.6604	1.0168	1.0040
.260	.6387	.6577	1.0147	1.0035
.208	.6387	.6524	1.0106	1.0025
.156	.6387	.6497	1.0086	1.0021
.104	.6387	.6497	1.0086	1.0021
.052	.6387	.6444	1.0044	1.0011
0.000	.6387	.6471	1.0065	1.0016
-.104	.6387	.6425	1.0029	1.0007
-.156	.6387	.6451	1.0050	1.0012
-.208	.6387	.6451	1.0050	1.0012
-.260	.6494	.6475	.9986	.9997
-.312	.6494	.6475	.9986	.9997
-.364	.6387	.6505	1.0091	1.0022
-.416	.6600	.6579	.9984	.9996
-.468	.6494	.6609	1.0088	1.0021
-.520	.6387	.6664	1.0215	1.0051
-.572	.6387	.6744	1.0276	1.0065
-.624	.6387	.6797	1.0316	1.0074
-.676	.6387	.6851	1.0356	1.0083
-.728	.6387	.6957	1.0437	1.0101
-.780	.6494	.7008	1.0388	1.0090
-.832	.6600	.7085	1.0361	1.0084
-.884	.6813	.7187	1.0270	1.0064
-.936	.7026	.7315	1.0203	1.0048
-.988	.7133	.7392	1.0180	1.0043
-1.040	.7239	.7496	1.0176	1.0042

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(s) x/D = 5.0; y/D = 1.0; $\alpha = 0^\circ$;

p_∞ = 22.44 psf (1074.59 N/m^2);
q_∞ = 245.12 psf (11736.36 N/m^2);
$p_{t,\infty}$ = 3187.20 psf (152603.96 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3450	.8450	.7926	.9351
.988	1.1955	.8139	.8251	.9475
.936	1.0461	.7961	.8724	.9640
.884	1.0247	.7673	.8653	.9616
.832	1.0034	.7438	.8610	.9602
.780	.9927	.7201	.8517	.9570
.728	.9820	.6964	.8421	.9537
.676	.9714	.6753	.8338	.9507
.624	.9607	.6542	.8252	.9476
.572	.9714	.6353	.8087	.9414
.520	.9820	.6217	.7957	.9363
.468	.9714	.6059	.7898	.9340
.416	.9607	.5902	.7838	.9316
.364	.9607	.5769	.7749	.9279
.312	.9607	.5662	.7677	.9249
.260	.9500	.5558	.7649	.9237
.208	.9393	.5507	.7657	.9240
.156	.9393	.5454	.7620	.9224
.104	.9393	.5400	.7582	.9208
.052	.9393	.5374	.7564	.9200
0.000	.9393	.5374	.7564	.9200
−.104	.9393	.5400	.7582	.9208
−.156	.9500	.5425	.7556	.9197
−.208	.9607	.5449	.7531	.9185
−.260	.9287	.5536	.7721	.9267
−.312	.9393	.5614	.7731	.9271
−.364	.9393	.5667	.7767	.9286
−.416	.9180	.5806	.7953	.9362
−.468	.9180	.5939	.8043	.9397
−.520	.9180	.6099	.8151	.9438
−.572	.9393	.6281	.8177	.9448
−.624	.9607	.6435	.8185	.9451
−.676	.9607	.6622	.8302	.9494
−.728	.9607	.6862	.8451	.9547
−.780	.9607	.7075	.8582	.9592
−.832	.9607	.7289	.8710	.9635
−.884	.9927	.7548	.8719	.9638
−.936	1.0247	.7806	.8728	.9641
−.988	1.0354	.8017	.8799	.9664
−1.040	1.0461	.8281	.8897	.9695

(t) x/D = 5.0; y/D = 0.83; $\alpha = 0^\circ$;

p_∞ = 22.45 psf (1074.72 N/m^2);
q_∞ = 245.15 psf (11737.83 N/m^2);
$p_{t,\infty}$ = 3187.60 psf (152623.11 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.4286	.7646	.7316	.9088
.988	1.2260	.7322	.7728	.9270
.936	1.0235	.7104	.8332	.9505
.884	1.0128	.6814	.8202	.9457
.832	1.0022	.6577	.8101	.9419
.780	.9915	.6313	.7980	.9372
.728	.9808	.6049	.7853	.9322
.676	.9702	.5839	.7758	.9283
.624	.9595	.5655	.7677	.9249
.572	.9595	.5495	.7568	.9202
.520	.9595	.5362	.7475	.9161
.468	.9488	.5231	.7425	.9138
.416	.9382	.5127	.7393	.9123
.364	.9382	.5021	.7315	.9088
.312	.9382	.4967	.7277	.9070
.260	.9275	.4917	.7281	.9072
.208	.9169	.4866	.7285	.9074
.156	.9169	.4813	.7245	.9055
.104	.9169	.4786	.7225	.9045
.052	.9275	.4757	.7161	.9015
0.000	.9382	.4754	.7119	.8994
−.104	.9169	.4765	.7209	.9038
−.156	.9275	.4789	.7186	.9026
−.208	.9382	.4787	.7143	.9006
−.260	.9169	.4818	.7249	.9057
−.312	.9275	.4896	.7265	.9064
−.364	.9275	.4896	.7265	.9064
−.416	.9169	.5032	.7408	.9131
−.468	.9169	.5112	.7467	.9157
−.520	.9169	.5218	.7544	.9191
−.572	.9275	.5376	.7613	.9221
−.624	.9382	.5533	.7680	.9250
−.676	.9488	.5717	.7763	.9284
−.728	.9595	.5928	.7860	.9325
−.780	.9595	.6142	.8000	.9380
−.832	.9595	.6382	.8155	.9440
−.884	.9915	.6667	.8200	.9457
−.936	1.0235	.6926	.8226	.9466
−.988	1.0341	.7190	.8338	.9507
−1.040	1.0448	.7481	.8462	.9551

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(u) x/D = 5.0; y/D = 0.63; $\alpha = 0^\circ$;

p_∞ = 22.46 psf (1075.43 N/m^2);
q_∞ = 245.31 psf (11745.56 N/m^2);
$p_{t,\infty}$ = 3189.70 psf (152723.66 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3844	.6799	.7008	.8939
.988	1.1821	.6449	.7386	.9121
.936	.9797	.6205	.7958	.9364
.884	.9691	.5915	.7813	.9305
.832	.9584	.5678	.7697	.9257
.780	.9371	.5444	.7622	.9225
.728	.9158	.5262	.7580	.9207
.676	.9158	.5076	.7445	.9147
.624	.9158	.4943	.7347	.9102
.572	.9158	.4863	.7287	.9075
.520	.9158	.4756	.7207	.9037
.468	.9052	.4679	.7190	.9028
.416	.8945	.4629	.7193	.9030
.364	.8945	.4549	.7131	.9000
.312	.8945	.4522	.7110	.8990
.260	.8839	.4471	.7112	.8991
.208	.8732	.4394	.7094	.8982
.156	.8732	.4367	.7072	.8971
.104	.8732	.4341	.7050	.8960
.052	.8732	.4287	.7007	.8939
0.000	.8732	.4287	.7007	.8939
-.104	.8732	.4292	.7011	.8941
-.156	.8839	.4317	.6988	.8929
-.208	.8945	.4341	.6966	.8918
-.260	.8732	.4372	.7076	.8973
-.312	.8839	.4423	.7074	.8972
-.364	.8839	.4477	.7117	.8993
-.416	.8732	.4532	.7204	.9036
-.468	.8732	.4612	.7268	.9066
-.520	.8732	.4692	.7330	.9095
-.572	.8839	.4770	.7346	.9102
-.624	.8945	.4847	.7361	.9109
-.676	.9052	.4978	.7416	.9134
-.728	.9158	.5162	.7507	.9175
-.780	.9158	.5348	.7642	.9234
-.832	.9158	.5535	.7774	.9289
-.884	.9371	.5770	.7846	.9319
-.936	.9584	.6084	.7968	.9367
-.988	.9797	.6319	.8031	.9392
-1.040	1.0010	.6634	.8141	.9434

(v) x/D = 5.0; y/D = 0.42; $\alpha = 0^\circ$;

p_∞ = 22.46 psf (1075.56 N/m^2);
q_∞ = 245.34 psf (11747.04 N/m^2);
$p_{t,\infty}$ = 3190.10 psf (152742.81 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3651	.6137	.6705	.8780
.988	1.1624	.5787	.7056	.8963
.936	.9598	.5570	.7618	.9223
.884	.9492	.5307	.7477	.9162
.832	.9385	.5123	.7388	.9122
.780	.9172	.4969	.7360	.9109
.728	.8958	.4814	.7331	.9095
.676	.8958	.4681	.7229	.9047
.624	.8958	.4601	.7167	.9017
.572	.8958	.4521	.7104	.8987
.520	.8958	.4468	.7062	.8966
.468	.8852	.4391	.7043	.8956
.416	.8745	.4340	.7045	.8957
.364	.8638	.4236	.7003	.8936
.312	.8532	.4159	.6982	.8926
.260	.8532	.4026	.6869	.8868
.208	.8532	.3919	.6777	.8819
.156	.8532	.3759	.6638	.8743
.104	.8532	.3679	.6567	.8704
.052	.8532	.3626	.6519	.8676
0.000	.8532	.3599	.6495	.8663
-.104	.8532	.3657	.6547	.8692
-.156	.8532	.3737	.6618	.8732
-.208	.8532	.3844	.6712	.8784
-.260	.8532	.3977	.6827	.8846
-.312	.8532	.4084	.6918	.8893
-.364	.8532	.4190	.7008	.8939
-.416	.8532	.4270	.7075	.8972
-.468	.8532	.4350	.7141	.9005
-.520	.8532	.4403	.7184	.9026
-.572	.8638	.4454	.7181	.9024
-.624	.8745	.4532	.7199	.9033
-.676	.8852	.4609	.7216	.9041
-.728	.8958	.4740	.7274	.9068
-.780	.8958	.4873	.7375	.9116
-.832	.8958	.5006	.7475	.9161
-.884	.9278	.5212	.7495	.9169
-.936	.9598	.5470	.7549	.9194
-.988	.9705	.5708	.7669	.9245
-1.040	.9812	.6025	.7836	.9315

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(w) x/D = 5.0; y/D = 0.21; $\alpha = 0^\circ$;

p_∞ = 22.47 psf (1075.63 N/m^2);
q_∞ = 245.36 psf (11747.77 N/m^2);
$p_{t,\infty}$ = 3190.30 psf (152752.39 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3419	.5796	.6572	.8707
.988	1.1395	.5500	.6947	.8908
.936	.9372	.5309	.7527	.9184
.884	.9265	.5099	.7418	.9135
.832	.9159	.4942	.7346	.9102
.780	.9052	.4785	.7270	.9067
.728	.8946	.4654	.7213	.9040
.676	.8946	.4521	.7109	.8989
.624	.8946	.4468	.7067	.8969
.572	.8946	.4388	.7004	.8937
.520	.8946	.4308	.6940	.8904
.468	.8733	.4233	.6963	.8916
.416	.8520	.4159	.6987	.8928
.364	.8520	.4052	.6897	.8882
.312	.8520	.3892	.6759	.8810
.260	.8413	.3709	.6639	.8744
.208	.8307	.3551	.6538	.8688
.156	.8307	.3365	.6364	.8586
.104	.8307	.3258	.6263	.8525
.052	.8307	.3205	.6211	.8493
0.000	.8307	.3178	.6185	.8477
-.104	.8307	.3262	.6267	.8527
-.156	.8413	.3313	.6275	.8532
-.208	.8520	.3497	.6407	.8611
-.260	.8413	.3686	.6619	.8733
-.312	.8520	.3844	.6717	.8787
-.364	.8520	.3977	.6832	.8848
-.416	.8520	.4110	.6946	.8907
-.468	.8520	.4164	.6991	.8930
-.520	.8520	.4244	.7057	.8964
-.572	.8520	.4323	.7124	.8996
-.624	.8520	.4430	.7211	.9039
-.676	.8626	.4507	.7229	.9047
-.728	.8733	.4612	.7267	.9065
-.780	.8733	.4745	.7371	.9114
-.832	.8733	.4851	.7453	.9151
-.884	.8946	.5006	.7481	.9163
-.936	.9159	.5214	.7545	.9192
-.988	.9372	.5395	.7588	.9210
-1.040	.9585	.5710	.7718	.9266

(x) x/D = 5.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 22.45 psf (1074.79 N/m^2);
q_∞ = 245.17 psf (11738.57 N/m^2);
$p_{t,\infty}$ = 3187.80 psf (152632.69 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3426	.5694	.6512	.8673
.988	1.1401	.5397	.6880	.8874
.936	.9377	.5207	.7452	.9150
.884	.9270	.5023	.7361	.9109
.832	.9164	.4893	.7307	.9084
.780	.9057	.4762	.7251	.9058
.728	.8951	.4685	.7234	.9050
.676	.8844	.4581	.7197	.9032
.624	.8738	.4503	.7179	.9023
.572	.8738	.4423	.7115	.8992
.520	.8738	.4370	.7072	.8971
.468	.8631	.4319	.7074	.8972
.416	.8524	.4215	.7032	.8951
.364	.8524	.4109	.6943	.8906
.312	.8524	.4002	.6852	.8859
.260	.8418	.3845	.6758	.8809
.208	.8311	.3714	.6685	.8769
.156	.8311	.3581	.6564	.8702
.104	.8311	.3474	.6465	.8645
.052	.8311	.3367	.6365	.8587
0.000	.8311	.3341	.6340	.8572
-.104	.8311	.3425	.6419	.8619
-.156	.8418	.3529	.6475	.8651
-.208	.8524	.3660	.6552	.8695
-.260	.8418	.3796	.6715	.8786
-.312	.8524	.3900	.6764	.8812
-.364	.8524	.4060	.6901	.8885
-.416	.8524	.4167	.6992	.8931
-.468	.8524	.4220	.7036	.8953
-.520	.8524	.4300	.7103	.8986
-.572	.8524	.4354	.7146	.9008
-.624	.8524	.4434	.7212	.9039
-.676	.8524	.4487	.7255	.9060
-.728	.8524	.4567	.7320	.9090
-.780	.8631	.4671	.7357	.9107
-.832	.8738	.4802	.7413	.9133
-.884	.8951	.4930	.7422	.9137
-.936	.9164	.5112	.7469	.9158
-.988	.9270	.5296	.7558	.9197
-1.040	.9377	.5560	.7700	.9258

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(y) $x/D = 5.0$; $y/D = -0.42$; $\alpha = 0^o$;

p_∞ = 22.45 psf (1074.75 N/m^2);
q_∞ = 245.16 psf (11738.20 N/m^2);
$p_{t,\infty}$ = 3187.70 psf (152627.90 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3426	.6174	.6781	.8821
.988	1.1508	.5848	.7129	.8999
.936	.9590	.5628	.7661	.9242
.884	.9377	.5340	.7547	.9192
.832	.9164	.5132	.7484	.9165
.780	.9058	.4949	.7392	.9123
.728	.8951	.4791	.7316	.9088
.676	.8844	.4634	.7238	.9052
.624	.8738	.4503	.7179	.9023
.572	.8738	.4423	.7115	.8992
.520	.8738	.4290	.7007	.8939
.468	.8631	.4160	.6942	.8906
.416	.8525	.4002	.6852	.8859
.364	.8525	.3976	.6829	.8847
.312	.8525	.4109	.6943	.8906
.260	.8418	.4058	.6943	.8906
.208	.8312	.4007	.6944	.8906
.156	.8312	.3927	.6874	.8870
.104	.8312	.3794	.6756	.8808
.052	.8312	.3528	.6515	.8674
0.000	.8312	.3394	.6390	.8602
-.104	.8312	.3772	.6737	.8797
-.156	.8418	.3849	.6762	.8811
-.208	.8525	.3927	.6787	.8824
-.260	.8418	.3983	.6878	.8873
-.312	.8525	.4007	.6856	.8861
-.364	.8418	.3849	.6762	.8811
-.416	.8525	.3927	.6787	.8824
-.468	.8418	.4090	.6970	.8920
-.520	.8312	.4226	.7130	.9000
-.572	.8418	.4356	.7194	.9030
-.624	.8525	.4460	.7234	.9049
-.676	.8525	.4594	.7341	.9100
-.728	.8525	.4727	.7447	.9148
-.780	.8525	.4887	.7572	.9203
-.832	.8525	.5074	.7715	.9265
-.884	.8844	.5280	.7726	.9269
-.936	.9164	.5538	.7774	.9289
-.988	.9377	.5800	.7865	.9326
-1.040	.9590	.6088	.7968	.9367

(z) $x/D = 6.0$; $y/D = 0.0$; $\alpha = 0^o$;

p_∞ = 22.47 psf (1075.70 N/m^2);
q_∞ = 245.37 psf (11748.51 N/m^2);
$p_{t,\infty}$ = 3190.50 psf (152761.96 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2782	.5492	.6555	.8697
.988	1.0865	.5247	.6949	.8909
.936	.8947	.5054	.7515	.9179
.884	.8841	.4897	.7442	.9146
.832	.8734	.4793	.7408	.9130
.780	.8628	.4662	.7351	.9104
.728	.8521	.4585	.7335	.9097
.676	.8521	.4505	.7271	.9067
.624	.8521	.4425	.7206	.9036
.572	.8521	.4372	.7163	.9015
.520	.8521	.4292	.7097	.8983
.468	.8415	.4241	.7100	.8985
.416	.8308	.4137	.7057	.8963
.364	.8308	.4057	.6988	.8929
.312	.8308	.3951	.6896	.8882
.260	.8202	.3820	.6825	.8845
.208	.8095	.3716	.6776	.8818
.156	.8095	.3583	.6653	.8752
.104	.8095	.3477	.6553	.8696
.052	.8095	.3423	.6503	.8667
0.000	.8095	.3370	.6452	.8638
-.104	.8095	.3454	.6532	.8684
-.156	.8202	.3532	.6562	.8701
-.208	.8308	.3636	.6615	.8731
-.260	.8202	.3745	.6757	.8809
-.312	.8308	.3849	.6806	.8835
-.364	.8202	.3985	.6970	.8920
-.416	.8308	.4062	.6992	.8931
-.468	.8202	.4145	.7109	.8989
-.520	.8095	.4201	.7204	.9035
-.572	.8095	.4254	.7249	.9057
-.624	.8095	.4307	.7294	.9078
-.676	.8202	.4358	.7289	.9076
-.728	.8308	.4462	.7329	.9094
-.780	.8308	.4542	.7394	.9124
-.832	.8308	.4649	.7480	.9163
-.884	.8415	.4753	.7515	.9179
-.936	.8521	.4910	.7591	.9212
-.988	.8628	.5094	.7684	.9251
-1.040	.8734	.5305	.7793	.9297

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(aa) x/D = 7.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 22.44 psf (1074.48 N/m^2);
q_∞ = 245.10 psf (11735.25 N/m^2);
$p_{t,\infty}$ = 3186.90 psf (152589.59 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2574	.5398	.6552	.8695
.988	1.0656	.5178	.6971	.8920
.936	.8738	.5039	.7594	.9213
.884	.8631	.4881	.7520	.9181
.832	.8525	.4777	.7486	.9165
.780	.8525	.4671	.7402	.9128
.728	.8525	.4537	.7295	.9079
.676	.8525	.4484	.7252	.9058
.624	.8525	.4404	.7188	.9027
.572	.8525	.4351	.7144	.9006
.520	.8525	.4297	.7100	.8985
.468	.8418	.4220	.7080	.8975
.416	.8312	.4143	.7060	.8965
.364	.8205	.4039	.7016	.8943
.312	.8099	.3961	.6994	.8932
.260	.8099	.3828	.6875	.8871
.208	.8099	.3721	.6778	.8820
.156	.8099	.3614	.6681	.8767
.104	.8099	.3508	.6581	.8712
.052	.8099	.3428	.6506	.8669
0.000	.8099	.3401	.6480	.8654
-.104	.8099	.3463	.6539	.8688
-.156	.8205	.3513	.6544	.8690
-.208	.8312	.3618	.6597	.8721
-.260	.8205	.3754	.6764	.8812
-.312	.8312	.3832	.6790	.8826
-.364	.8205	.3941	.6930	.8900
-.416	.8312	.4045	.6976	.8923
-.468	.8205	.4101	.7070	.8970
-.520	.8099	.4157	.7165	.9016
-.572	.8099	.4238	.7234	.9049
-.624	.8099	.4291	.7279	.9071
-.676	.8099	.4344	.7324	.9092
-.728	.8099	.4425	.7391	.9123
-.780	.8099	.4478	.7436	.9143
-.832	.8099	.4585	.7524	.9182
-.884	.8205	.4689	.7560	.9198
-.936	.8312	.4820	.7615	.9222
-.988	.8312	.4980	.7741	.9275
-1.040	.8312	.5194	.7905	.9343

(bb) x/D = 8.0; y/D = 0.0; $\alpha = 0^\circ$;

p_∞ = 22.46 psf (1075.29 N/m^2);
q_∞ = 245.28 psf (11744.09 N/m^2);
$p_{t,\infty}$ = 3189.30 psf (152704.51 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2358	.5379	.6597	.8721
.988	1.0440	.5159	.7030	.8950
.936	.8522	.5019	.7674	.9247
.884	.8522	.4886	.7571	.9203
.832	.8522	.4806	.7509	.9176
.780	.8522	.4859	.7551	.9194
.728	.8522	.4912	.7592	.9212
.676	.9162	.4977	.7370	.9113
.624	.9801	.4988	.7134	.9001
.572	1.0333	.4975	.6939	.8904
.520	1.0866	.4962	.6757	.8809
.468	1.0973	.4906	.6686	.8770
.416	1.1079	.4796	.6580	.8711
.364	1.1079	.4690	.6506	.8669
.312	1.1079	.4583	.6432	.8626
.260	1.0973	.4399	.6331	.8566
.208	1.0866	.4295	.6287	.8539
.156	1.0866	.4161	.6188	.8479
.104	1.0866	.4054	.6108	.8428
.052	1.0760	.3950	.6059	.8397
0.000	1.0653	.3926	.6071	.8404
-.104	1.0653	.3984	.6116	.8433
-.156	1.0653	.4038	.6156	.8459
-.208	1.0653	.4171	.6257	.8521
-.260	1.0547	.4308	.6391	.8602
-.312	1.0547	.4441	.6489	.8659
-.364	1.0440	.4577	.6622	.8734
-.416	1.0440	.4711	.6717	.8787
-.468	1.0333	.4794	.6811	.8837
-.520	1.0227	.4823	.6867	.8867
-.572	1.0014	.4828	.6944	.8906
-.624	.9801	.4780	.6984	.8927
-.676	.9162	.4689	.7154	.9011
-.728	.8522	.4598	.7345	.9102
-.780	.8309	.4550	.7399	.9127
-.832	.8096	.4581	.7522	.9182
-.884	.8096	.4688	.7610	.9220
-.936	.8096	.4822	.7717	.9265
-.988	.8203	.4979	.7791	.9296
-1.040	.8309	.5190	.7903	.9342

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(cc) $x/D = 8.39$; $y/D = 3.0$; $\alpha = 0^o$;

p_∞ = 22.44 psf (1074.55 N/m^2);
q_∞ = 245.11 psf (11735.99 N/m^2);
$p_{t,\infty}$ = 3187.10 psf (152599.17 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3432	.9827	.8554	.9583
.988	1.1513	.9847	.9248	.9801
.936	.9594	.9839	1.0127	1.0030
.884	.9488	.9815	1.0171	1.0041
.832	.9381	.9791	1.0216	1.0051
.780	.9275	.9766	1.0262	1.0062
.728	.9168	.9689	1.0280	1.0066
.676	.9061	.9665	1.0328	1.0077
.624	.8955	.9641	1.0376	1.0087
.572	.9061	.9638	1.0313	1.0073
.520	.9168	.9609	1.0238	1.0056
.468	.9061	.9612	1.0299	1.0070
.416	.8955	.9561	1.0333	1.0078
.364	.8955	.9534	1.0319	1.0075
.312	.8955	.9508	1.0304	1.0071
.260	.8848	.9510	1.0367	1.0086
.208	.8742	.9513	1.0432	1.0100
.156	.8742	.9460	1.0403	1.0093
.104	.8742	.9460	1.0403	1.0093
.052	.8742	.9460	1.0403	1.0093
0.000	.8742	.9460	1.0403	1.0093
-.104	.8528	.9379	1.0487	1.0112
-.156	.8742	.9374	1.0356	1.0083
-.208	.8955	.9369	1.0229	1.0054
-.260	.8528	.9379	1.0487	1.0112
-.312	.8742	.9374	1.0356	1.0083
-.364	.8742	.9374	1.0356	1.0083
-.416	.8528	.9379	1.0487	1.0112
-.468	.8528	.9379	1.0487	1.0112
-.520	.8528	.9406	1.0502	1.0115
-.572	.8635	.9403	1.0436	1.0101
-.624	.8742	.9454	1.0400	1.0093
-.676	.8742	.9481	1.0414	1.0096
-.728	.8742	.9534	1.0444	1.0102
-.780	.8742	.9561	1.0458	1.0106
-.832	.8742	.9561	1.0458	1.0106
-.884	.8955	.9609	1.0359	1.0084
-.936	.9168	.9684	1.0278	1.0065
-.988	.9381	.9679	1.0158	1.0038
-1.040	.9594	.9728	1.0069	1.0017

(dd) $x/D = 8.39$; $y/D = 2.0$; $\alpha = 0^o$;

p_∞ = 22.45 psf (1075.13 N/m^2);
q_∞ = 245.24 psf (11742.25 N/m^2);
$p_{t,\infty}$ = 3188.80 psf (152680.57 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3848	.9743	.8388	.9525
.988	1.1931	.9736	.9034	.9737
.936	1.0013	.9728	.9857	.9965
.884	.9907	.9677	.9884	.9971
.832	.9800	.9600	.9897	.9975
.780	.9694	.9576	.9939	.9985
.728	.9587	.9498	.9954	.9989
.676	.9481	.9474	.9997	.9999
.624	.9374	.9424	1.0026	1.0006
.572	.9481	.9368	.9940	.9985
.520	.9587	.9339	.9870	.9968
.468	.9481	.9314	.9912	.9978
.416	.9374	.9264	.9941	.9986
.364	.9374	.9237	.9927	.9982
.312	.9374	.9210	.9912	.9979
.260	.9267	.9160	.9942	.9986
.208	.9161	.9162	1.0001	1.0000
.156	.9161	.9162	1.0001	1.0000
.104	.9161	.9135	.9986	.9997
.052	.9161	.9109	.9972	.9993
0.000	.9161	.9109	.9972	.9993
-.104	.9161	.9082	.9957	.9989
-.156	.9267	.9080	.9898	.9975
-.208	.9374	.9077	.9840	.9961
-.260	.9054	.9085	1.0017	1.0004
-.312	.9161	.9135	.9986	.9997
-.364	.9161	.9135	.9986	.9997
-.416	.8948	.9167	1.0122	1.0029
-.468	.8948	.9194	1.0136	1.0033
-.520	.8948	.9220	1.0151	1.0036
-.572	.9054	.9218	1.0090	1.0022
-.624	.9161	.9269	1.0059	1.0014
-.676	.9161	.9322	1.0088	1.0021
-.728	.9161	.9375	1.0116	1.0028
-.780	.9161	.9402	1.0131	1.0031
-.832	.9161	.9429	1.0145	1.0035
-.884	.9374	.9477	1.0055	1.0013
-.936	.9587	.9552	.9982	.9996
-.988	.9800	.9573	.9884	.9971
-1.040	1.0013	.9595	.9789	.9948

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(ee) $x/D = 8.39$; $y/D = 1.5$; $\alpha = 0^\circ$;

p_∞ = 22.46 psf (1075.23 N/m^2);
q_∞ = 245.27 psf (11743.35 N/m^2);
$p_{t,\infty}$ = 3189.10 psf (152694.93 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3211	.8692	.8111	.9423
.988	1.1186	.8634	.8785	.9659
.936	.9162	.8602	.9689	.9922
.884	.9056	.8524	.9702	.9925
.832	.8949	.8447	.9715	.9929
.780	.8843	.8370	.9729	.9932
.728	.8736	.8265	.9727	.9932
.676	.8736	.8186	.9680	.9919
.624	.8736	.8106	.9632	.9907
.572	.8843	.8050	.9541	.9883
.520	.8949	.7967	.9436	.9854
.468	.8736	.7919	.9521	.9877
.416	.8523	.7844	.9594	.9897
.364	.8523	.7791	.9561	.9888
.312	.8523	.7711	.9512	.9875
.260	.8523	.7684	.9495	.9870
.208	.8523	.7658	.9479	.9866
.156	.8523	.7604	.9446	.9857
.104	.8523	.7578	.9429	.9852
.052	.8523	.7525	.9396	.9843
0.000	.8523	.7525	.9396	.9843
-.104	.8523	.7498	.9379	.9838
-.156	.8630	.7522	.9336	.9826
-.208	.8736	.7519	.9278	.9809
-.260	.8523	.7578	.9429	.9852
-.312	.8630	.7602	.9386	.9840
-.364	.8523	.7631	.9462	.9861
-.416	.8523	.7658	.9479	.9866
-.468	.8416	.7767	.9606	.9900
-.520	.8310	.7769	.9669	.9917
-.572	.8416	.7847	.9656	.9913
-.624	.8523	.7924	.9642	.9910
-.676	.8523	.7977	.9675	.9918
-.728	.8523	.8057	.9723	.9931
-.780	.8523	.8111	.9755	.9939
-.832	.8523	.8191	.9803	.9951
-.884	.8736	.8265	.9727	.9932
-.936	.8949	.8367	.9669	.9917
-.988	.9056	.8444	.9657	.9913
-1.040	.9162	.8522	.9644	.9910

(ff) $x/D = 8.39$; $y/D = 1.0$; $\alpha = 0^\circ$;

p_∞ = 22.44 psf (1074.45 N/m^2);
q_∞ = 245.09 psf (11734.88 N/m^2);
$p_{t,\infty}$ = 3186.80 psf (152584.81 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2589	.7371	.7652	.9238
.988	1.0668	.7204	.8217	.9463
.936	.8748	.7117	.9019	.9733
.884	.8641	.6906	.8940	.9708
.832	.8535	.6749	.8892	.9694
.780	.8428	.6591	.8844	.9678
.728	.8321	.6381	.8757	.9650
.676	.8321	.6248	.8665	.9620
.624	.8321	.6088	.8553	.9583
.572	.8321	.5955	.8459	.9550
.520	.8321	.5848	.8383	.9523
.468	.8321	.5715	.8287	.9489
.416	.8321	.5582	.8190	.9453
.364	.8321	.5475	.8112	.9423
.312	.8321	.5369	.8032	.9393
.260	.8321	.5289	.7972	.9369
.208	.8321	.5235	.7932	.9353
.156	.8321	.5182	.7891	.9337
.104	.8321	.5155	.7871	.9329
.052	.8321	.5102	.7830	.9312
0.000	.8321	.5102	.7830	.9312
-.104	.8321	.5108	.7835	.9314
-.156	.8321	.5108	.7835	.9314
-.208	.8321	.5108	.7835	.9314
-.260	.8321	.5135	.7855	.9323
-.312	.8321	.5188	.7896	.9339
-.364	.8215	.5217	.7969	.9368
-.416	.8321	.5321	.7997	.9379
-.468	.8215	.5431	.8131	.9431
-.520	.8108	.5567	.8286	.9488
-.572	.8108	.5700	.8385	.9524
-.624	.8108	.5833	.8482	.9558
-.676	.8108	.5967	.8578	.9591
-.728	.8108	.6127	.8693	.9629
-.780	.8108	.6260	.8787	.9660
-.832	.8108	.6393	.8880	.9690
-.884	.8215	.6577	.8948	.9711
-.936	.8321	.6762	.9014	.9731
-.988	.8321	.6895	.9103	.9758
-1.040	.8321	.7055	.9208	.9789

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(gg) $x/D = 8.39$; $y/D = 0.83$; $\alpha = 0^o$;

p_∞ =22.44 psf (1074.52 N/m^2);
q_∞ = 245.10 psf (11735.62 N/m^2);
$p_{t,\infty}$ = 3187.00 psf (152594.38 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2594	.6864	.7383	.9119
.988	1.0673	.6697	.7921	.9349
.936	.8752	.6530	.8638	.9611
.884	.8645	.6320	.8550	.9581
.832	.8538	.6109	.8459	.9550
.780	.8431	.5898	.8364	.9516
.728	.8325	.5714	.8285	.9488
.676	.8325	.5555	.8169	.9445
.624	.8325	.5395	.8050	.9400
.572	.8431	.5232	.7878	.9332
.520	.8538	.5123	.7746	.9278
.468	.8431	.5046	.7736	.9273
.416	.8325	.4942	.7705	.9260
.364	.8325	.4862	.7642	.9234
.312	.8325	.4809	.7600	.9216
.260	.8325	.4755	.7558	.9197
.208	.8325	.4702	.7515	.9179
.156	.8325	.4675	.7494	.9169
.104	.8325	.4622	.7451	.9150
.052	.8325	.4595	.7430	.9140
0.000	.8325	.4595	.7430	.9140
-.104	.8325	.4601	.7434	.9142
-.156	.8325	.4601	.7434	.9142
-.208	.8325	.4601	.7434	.9142
-.260	.8325	.4627	.7456	.9152
-.312	.8325	.4654	.7477	.9162
-.364	.8218	.4683	.7549	.9193
-.416	.8325	.4734	.7541	.9190
-.468	.8218	.4817	.7656	.9240
-.520	.8111	.4899	.7772	.9288
-.572	.8111	.5006	.7856	.9323
-.624	.8111	.5139	.7960	.9364
-.676	.8111	.5246	.8042	.9397
-.728	.8111	.5433	.8184	.9451
-.780	.8111	.5593	.8304	.9495
-.832	.8111	.5780	.8441	.9544
-.884	.8218	.5964	.8519	.9571
-.936	.8325	.6174	.8612	.9602
-.988	.8325	.6334	.8723	.9639
-1.040	.8325	.6521	.8851	.9680

(hh) $x/D = 8.39$; $y/D = 0.63$; $\alpha = 0^o$;

p_∞ = 22.45 psf (1074.86 N/m^2);
q_∞ = 245.18 psf (11739.30 N/m^2);
$p_{t,\infty}$ = 3188.00 psf (152642.26 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2371	.6281	.7125	.8997
.988	1.0451	.6034	.7599	.9215
.936	.8531	.5867	.8293	.9491
.884	.8531	.5628	.8122	.9427
.832	.8531	.5441	.7986	.9375
.780	.8425	.5231	.7880	.9332
.728	.8318	.5047	.7789	.9296
.676	.8318	.4940	.7707	.9261
.624	.8318	.4807	.7602	.9216
.572	.8318	.4727	.7539	.9189
.520	.8318	.4647	.7475	.9160
.468	.8318	.4567	.7410	.9131
.416	.8318	.4514	.7367	.9112
.364	.8318	.4434	.7301	.9081
.312	.8318	.4381	.7257	.9061
.260	.8318	.4327	.7213	.9040
.208	.8318	.4274	.7168	.9018
.156	.8318	.4221	.7123	.8996
.104	.8318	.4168	.7078	.8974
.052	.8318	.4141	.7056	.8963
0.000	.8318	.4088	.7010	.8940
-.104	.8105	.4139	.7146	.9007
-.156	.8211	.4136	.7097	.8983
-.208	.8318	.4134	.7049	.8960
-.260	.8105	.4192	.7192	.9030
-.312	.8211	.4243	.7188	.9028
-.364	.8211	.4270	.7211	.9039
-.416	.8105	.4326	.7306	.9083
-.468	.8105	.4406	.7373	.9115
-.520	.8105	.4460	.7418	.9135
-.572	.8105	.4540	.7485	.9165
-.624	.8105	.4621	.7550	.9194
-.676	.8105	.4728	.7637	.9232
-.728	.8105	.4835	.7723	.9268
-.780	.8105	.4942	.7808	.9303
-.832	.8105	.5102	.7934	.9354
-.884	.8211	.5287	.8024	.9390
-.936	.8318	.5498	.8130	.9430
-.988	.8318	.5659	.8248	.9474
-1.040	.8318	.5926	.8441	.9544

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(ii) $x/D = 8.39$; $y/D = 0.42$; $\alpha = 0^\circ$;

p_∞ = 22.45 psf (1074.92 N/m^2);
q_∞ = 245.20 psf (11740.04 N/m^2);
$p_{t,\infty}$ = 3188.20 psf (152651.84 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2782	.5790	.6731	.8794
.988	1.0865	.5544	.7143	.9006
.936	.8948	.5351	.7733	.9272
.884	.8734	.5143	.7673	.9247
.832	.8521	.4962	.7631	.9229
.780	.8521	.4802	.7507	.9175
.728	.8521	.4669	.7402	.9128
.676	.8521	.4562	.7317	.9089
.624	.8521	.4482	.7252	.9058
.572	.8521	.4402	.7188	.9027
.520	.8521	.4349	.7144	.9006
.468	.8415	.4272	.7125	.8997
.416	.8308	.4221	.7128	.8998
.364	.8308	.4141	.7060	.8965
.312	.8308	.4061	.6991	.8931
.260	.8415	.3978	.6876	.8871
.208	.8521	.3922	.6785	.8823
.156	.8521	.3816	.6692	.8773
.104	.8521	.3762	.6645	.8747
.052	.8628	.3733	.6578	.8710
0.000	.8734	.3704	.6512	.8672
-.104	.8521	.3704	.6593	.8718
-.156	.8521	.3731	.6617	.8732
-.208	.8521	.3758	.6641	.8745
-.260	.8415	.3841	.6756	.8808
-.312	.8415	.3895	.6803	.8833
-.364	.8308	.3978	.6919	.8894
-.416	.8308	.4058	.6989	.8929
-.468	.8202	.4114	.7082	.8976
-.520	.8095	.4170	.7177	.9023
-.572	.8095	.4251	.7246	.9055
-.624	.8095	.4304	.7292	.9077
-.676	.8095	.4385	.7360	.9108
-.728	.8095	.4492	.7449	.9149
-.780	.8202	.4596	.7486	.9166
-.832	.8308	.4701	.7522	.9182
-.884	.8415	.4859	.7599	.9215
-.936	.8521	.5017	.7673	.9247
-.988	.8521	.5205	.7815	.9306
-1.040	.8521	.5419	.7975	.9370

(jj) $x/D = 8.39$; $y/D = 0.21$; $\alpha = 0^\circ$;

p_∞ = 22.46 psf (1075.43 N/m^2);
q_∞ = 245.31 psf (11745.56 N/m^2);
$p_{t,\infty}$ = 3189.70 psf (152723.66 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2156	.5590	.6781	.8821
.988	1.0237	.5370	.7243	.9054
.936	.8318	.5177	.7890	.9336
.884	.8318	.4964	.7726	.9269
.832	.8318	.4831	.7621	.9225
.780	.8318	.4778	.7579	.9207
.728	.8318	.4778	.7579	.9207
.676	.8744	.4794	.7405	.9129
.624	.9171	.4864	.7282	.9073
.572	.9810	.4768	.6972	.8921
.520	1.0450	.4779	.6762	.8811
.468	1.0557	.4750	.6708	.8782
.416	1.0664	.4667	.6616	.8731
.364	1.0664	.4561	.6540	.8688
.312	1.0664	.4427	.6443	.8633
.260	1.0557	.4297	.6380	.8595
.208	1.0450	.4166	.6314	.8556
.156	1.0450	.4006	.6191	.8481
.104	1.0450	.3926	.6129	.8442
.052	1.0450	.3873	.6087	.8415
0.000	1.0450	.3846	.6066	.8401
-.104	1.0450	.3864	.6081	.8411
-.156	1.0450	.3891	.6102	.8424
-.208	1.0450	.4025	.6206	.8490
-.260	1.0344	.4135	.6323	.8561
-.312	1.0344	.4295	.6444	.8633
-.364	1.0024	.4410	.6633	.8741
-.416	1.0237	.4566	.6678	.8766
-.468	.9917	.4627	.6831	.8848
-.520	.9597	.4635	.6950	.8909
-.572	.9277	.4616	.7054	.8962
-.624	.8957	.4570	.7143	.9006
-.676	.8637	.4525	.7238	.9051
-.728	.8318	.4506	.7360	.9109
-.780	.8104	.4538	.7483	.9164
-.832	.7891	.4650	.7676	.9248
-.884	.7998	.4781	.7732	.9272
-.936	.8104	.4939	.7807	.9303
-.988	.8211	.5124	.7899	.9340
-1.040	.8318	.5335	.8009	.9384

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D IN THE WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Concluded

(kk) $x/D = 8.39$; $y/D = 0.0$; $\alpha = 0^\circ$;

p_∞ = 22.44 psf (1074.48 N/m^2);
q_∞ = 245.10 psf (11735.25 N/m^2);
$p_{t,\infty}$ = 3186.90 psf (152589.59 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2793	.5846	.6760	.8810
.988	1.1727	.6086	.7204	.9035
.936	1.0661	.6005	.7505	.9174
.884	1.0874	.5787	.7295	.9078
.832	1.1088	.5648	.7137	.9003
.780	1.1088	.5488	.7036	.8953
.728	1.1088	.5355	.6950	.8909
.676	1.1194	.5246	.6846	.8855
.624	1.1301	.5136	.6742	.8800
.572	1.1301	.5056	.6689	.8772
.520	1.1301	.5003	.6654	.8752
.468	1.1301	.4896	.6582	.8712
.416	1.1301	.4816	.6528	.8682
.364	1.1194	.4712	.6488	.8659
.312	1.1088	.4608	.6447	.8635
.260	1.0981	.4451	.6366	.8587
.208	1.0874	.4347	.6322	.8561
.156	1.0874	.4213	.6224	.8501
.104	1.0874	.4106	.6145	.8452
.052	1.0874	.4026	.6085	.8413
0.000	1.0874	.3946	.6024	.8374
-.104	1.0874	.4019	.6079	.8409
-.156	1.0874	.4072	.6119	.8435
-.208	1.0874	.4206	.6219	.8498
-.260	1.0768	.4343	.6351	.8578
-.312	1.0768	.4450	.6429	.8624
-.364	1.0661	.4560	.6540	.8688
-.416	1.0661	.4694	.6635	.8742
-.468	1.0554	.4804	.6746	.8803
-.520	1.0448	.4887	.6839	.8852
-.572	1.0661	.4935	.6804	.8833
-.624	1.0874	.5010	.6788	.8825
-.676	1.0981	.5088	.6807	.8835
-.728	1.1088	.5166	.6826	.8845
-.780	1.0874	.5251	.6949	.8909
-.832	1.0661	.5391	.7111	.8990
-.884	1.0661	.5524	.7199	.9033
-.936	1.0661	.5605	.7251	.9058
-.988	.9808	.5545	.7519	.9180
-1.040	.8955	.5459	.7807	.9303

(ll) $x/D = 8.39$; $y/D = -0.42$; $\alpha = 0^\circ$;

p_∞ = 22.45 psf (1074.96 N/m^2);
q_∞ = 245.20 psf (11740.41 N/m^2);
$p_{t,\infty}$ = 3188.30 psf (152656.63 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.5349	.6901	.6705	.8780
.988	1.3430	.6628	.7025	.8948
.936	1.1512	.6328	.7414	.9133
.884	1.1405	.5984	.7244	.9054
.832	1.1298	.5774	.7149	.9009
.780	1.1085	.5566	.7086	.8978
.728	1.0872	.5358	.7020	.8945
.676	1.0872	.5171	.6897	.8882
.624	1.0872	.5011	.6789	.8826
.572	1.0979	.4849	.6646	.8748
.520	1.1085	.4713	.6520	.8677
.468	1.0979	.4502	.6404	.8609
.416	1.0872	.4425	.6379	.8595
.364	1.0872	.4611	.6513	.8673
.312	1.0872	.4718	.6588	.8715
.260	1.0765	.4694	.6603	.8724
.208	1.0659	.4643	.6600	.8722
.156	1.0659	.4590	.6562	.8701
.104	1.0659	.4403	.6427	.8623
.052	1.0659	.4110	.6209	.8492
0.000	1.0659	.3976	.6108	.8428
-.104	1.0659	.4183	.6264	.8526
-.156	1.0659	.4424	.6442	.8632
-.208	1.0659	.4558	.6539	.8688
-.260	1.0446	.4563	.6609	.8728
-.312	1.0446	.4590	.6629	.8738
-.364	1.0446	.4670	.6687	.8770
-.416	1.0233	.4461	.6603	.8724
-.468	1.0233	.4381	.6543	.8690
-.520	1.0233	.4515	.6643	.8746
-.572	1.0446	.4724	.6725	.8791
-.624	1.0659	.4879	.6766	.8813
-.676	1.0765	.5037	.6840	.8853
-.728	1.0872	.5195	.6913	.8891
-.780	1.0872	.5383	.7036	.8953
-.832	1.0872	.5570	.7158	.9013
-.884	1.1085	.5806	.7237	.9051
-.936	1.1298	.6068	.7329	.9094
-.988	1.1512	.6384	.7447	.9148
-1.040	1.1725	.6727	.7575	.9205

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF A WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 221.11 psf (10586.70 N/m^2);
q_∞ = 396.23 psf (18971.37 N/m^2);
$p_{t,\infty}$ = 939.80 psf (44997.87 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7376	.8944	1.1012	1.0635
.988	.7235	.8967	1.1133	1.0707
.936	.7095	.8791	1.1131	1.0706
.884	.6879	.8777	1.1296	1.0803
.832	.6662	.8647	1.1392	1.0858
.780	.6468	.8430	1.1417	1.0872
.728	.6273	.8329	1.1523	1.0932
.676	.5981	.7497	1.1196	1.0744
.624	.5689	.2941	.7190	.7862
.572	.5581	.0673	.3472	.4144
.520	.5473	.0149	.1650	.2015
.468	.5429	.0054	.1002	.1229
.416	.5386	.0048	.0949	.1164
.364	.5386	.0048	.0949	.1164
.312	.5386	.0048	.0949	.1164
.260	.5429	.0025	.0672	.0826
.208	.5473	.0000	.0092	.0113
.156	.5505	0.0000	0.0000	0.0000
.104	.5548	0.0000	0.0000	0.0000
.052	.5559	0.0000	0.0000	0.0000
0.000	.5624	.0007	.0345	.0424
-.052	.5635	.0047	.0911	.1117
-.104	.5646	.0041	.0850	.1043
-.156	.5635	.0047	.0911	.1117
-.208	.5624	.0053	.0968	.1187
-.260	.5624	.0053	.0968	.1187
-.312	.5624	.0053	.0968	.1187
-.364	.5646	.0041	.0850	.1043
-.416	.5667	.0118	.1441	.1762
-.468	.5743	.0554	.3105	.3727
-.520	.5819	.2641	.6738	.7463
-.572	.5959	.7777	1.1424	1.0876
-.624	.6100	.8431	1.1757	1.1063
-.676	.6262	.8487	1.1642	1.0999
-.728	.6424	.8577	1.1554	1.0950
-.780	.6662	.8637	1.1386	1.0854
-.832	.6900	.8664	1.1205	1.0750
-.884	.7041	.8740	1.1141	1.0712
-.936	.7181	.8898	1.1131	1.0706
-.988	.7387	.8930	1.0995	1.0626
-1.040	.7592	.9045	1.0915	1.0577

(b) $x/D = 1.5$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 221.23 psf (10592.33 N/m^2);
q_∞ = 396.44 psf (18981.46 N/m^2);
$p_{t,\infty}$ = 940.30 psf (45021.81 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9078	.9504	1.0232	1.0152
.988	.9110	.9332	1.0121	1.0079
.936	.9143	.9176	1.0018	1.0012
.884	.8667	.9125	1.0261	1.0170
.832	.8192	.9073	1.0524	1.0337
.780	.7630	.8901	1.0801	1.0509
.728	.7068	.8812	1.1166	1.0727
.676	.6700	.8326	1.1147	1.0716
.624	.6333	.6477	1.0113	1.0074
.572	.6192	.3015	.6977	.7676
.520	.6052	.1296	.4628	.5402
.468	.6052	.0381	.2509	.3037
.416	.6052	.0034	.0753	.0924
.364	.6041	0.0000	0.0000	0.0000
.312	.6030	0.0000	0.0000	0.0000
.260	.6041	0.0000	0.0000	0.0000
.208	.6052	0.0000	0.0000	0.0000
.156	.6106	0.0000	0.0000	0.0000
.104	.6117	0.0000	0.0000	0.0000
.052	.6084	0.0000	0.0000	0.0000
0.000	.6182	0.0000	0.0000	0.0000
-.052	.6149	0.0000	0.0000	0.0000
-.104	.6117	0.0000	0.0000	0.0000
-.156	.6171	0.0000	0.0000	0.0000
-.208	.6225	0.0000	0.0000	0.0000
-.260	.6246	.0094	.1228	.1504
-.312	.6268	.0425	.2605	.3149
-.364	.6344	.0840	.3639	.4330
-.416	.6419	.2307	.5995	.6774
-.468	.6484	.4818	.8620	.9022
-.520	.6549	.8171	1.1170	1.0729
-.572	.6841	.8718	1.1289	1.0798
-.624	.7133	.8835	1.1129	1.0705
-.676	.7651	.8814	1.0733	1.0467
-.728	.8170	.8926	1.0452	1.0292
-.780	.8473	.9040	1.0329	1.0214
-.832	.8775	.9137	1.0204	1.0134
-.884	.8851	.9257	1.0227	1.0148
-.936	.8927	.9394	1.0258	1.0169
-.988	.8267	.9522	1.0732	1.0466
-1.040	.7608	.9434	1.1135	1.0709

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF A WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(c) $x/D = 2.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 221.25 psf (10593.46 N/m^2);
q_∞ = 396.48 psf (18983.48 N/m^2);
$p_{t,\infty}$ = 940.40 psf (45026.59 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7335	.8994	1.1074	1.0672
.988	.7237	.9010	1.1158	1.0722
.936	.7140	.8910	1.1171	1.0730
.884	.7053	.8841	1.1196	1.0744
.832	.6967	.8889	1.1296	1.0802
.780	.7194	.8835	1.1082	1.0677
.728	.7421	.8780	1.0877	1.0555
.676	.7551	.8808	1.0801	1.0508
.624	.7681	.8404	1.0460	1.0297
.572	.7605	.6578	.9300	.9521
.520	.7529	.4188	.7458	.8091
.468	.7540	.1969	.5110	.5901
.416	.7551	.0619	.2863	.3449
.364	.7518	.0065	.0932	.1144
.312	.7486	0.0000	0.0000	0.0000
.260	.7529	0.0000	0.0000	0.0000
.208	.7573	0.0000	0.0000	0.0000
.156	.7659	0.0000	0.0000	0.0000
.104	.7702	0.0000	0.0000	0.0000
.052	.7735	0.0000	0.0000	0.0000
0.000	.7832	0.0000	0.0000	0.0000
−.052	.7865	.0211	.1638	.2001
−.104	.7897	.0338	.2068	.2515
−.156	.8070	.0360	.2113	.2569
−.208	.8243	.0523	.2520	.3049
−.260	.8243	.1134	.3709	.4408
−.312	.8243	.2450	.5452	.6245
−.364	.8092	.4337	.7321	.7974
−.416	.7940	.7901	.9975	.9984
−.468	.7789	.9022	1.0762	1.0485
−.520	.7637	.8882	1.0784	1.0498
−.572	.7432	.8916	1.0953	1.0601
−.624	.7226	.8967	1.1139	1.0711
−.676	.7172	.8910	1.1146	1.0715
−.728	.7118	.8919	1.1193	1.0743
−.780	.7216	.8803	1.1046	1.0656
−.832	.7313	.8853	1.1003	1.0630
−.884	.7389	.9006	1.1040	1.0653
−.936	.7464	.9093	1.1037	1.0651
−.988	.7702	.9053	1.0841	1.0533
−1.040	.7940	.9079	1.0693	1.0443

(d) $x/D = 2.5$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 221.23 psf (10592.33 N/m^2);
q_∞ = 396.44 psf (18981.46 N/m^2);
$p_{t,\infty}$ = 940.30 psf (45021.81 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6960	.9002	1.1373	1.0847
.988	.7489	.9097	1.1021	1.0641
.936	.8019	.9142	1.0677	1.0433
.884	.8397	.9178	1.0454	1.0294
.832	.8775	.9197	1.0237	1.0155
.780	.9208	.9206	.9999	.9999
.728	.9640	.9197	.9768	.9845
.676	.9910	.9150	.9609	.9736
.624	1.0180	.8883	.9341	.9549
.572	1.0267	.8277	.8979	.9289
.520	1.0353	.7107	.8285	.8763
.468	1.0213	.5279	.7190	.7862
.416	1.0072	.3630	.6003	.6783
.364	.9975	.2257	.4757	.5537
.312	.9878	.1531	.3937	.4660
.260	.9899	.1267	.3578	.4262
.208	.9921	.1309	.3632	.4323
.156	1.0396	.1822	.4186	.4931
.104	1.0418	.2265	.4663	.5439
.052	1.0461	.2083	.4462	.5227
0.000	1.0915	.2551	.4835	.5618
−.052	1.0958	.2722	.4984	.5773
−.104	1.1002	.2861	.5100	.5891
−.156	1.1185	.3121	.5282	.6076
−.208	1.1369	.4591	.6354	.7113
−.260	1.1185	.6597	.7680	.8276
−.312	1.1002	.8707	.8896	.9228
−.364	1.0872	.9268	.9233	.9473
−.416	1.0742	.9258	.9283	.9509
−.468	1.0342	.9313	.9489	.9653
−.520	.9942	.9284	.9663	.9773
−.572	.9499	.9245	.9865	.9910
−.624	.9056	.9288	1.0127	1.0084
−.676	.8775	.9187	1.0232	1.0152
−.728	.8494	.9169	1.0389	1.0253
−.780	.8116	.9051	1.0560	1.0360
−.832	.7738	.9032	1.0804	1.0510
−.884	.7543	.9064	1.0962	1.0606
−.936	.7349	.9179	1.1176	1.0733
−.988	.7143	.9015	1.1234	1.0766
−1.040	.6938	.9048	1.1420	1.0874

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF A WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(e) x/D = 3.0; y/D = 0.0; α = 5°;

p_∞ = 221.30 psf (10595.71 N/m^2);
q_∞ = 396.56 psf (18987.52 N/m^2);
$p_{t,\infty}$ = 940.60 psf (45036.17 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9246	.9433	1.0101	1.0066
.988	.9753	.9495	.9867	.9911
.936	1.0261	.9372	.9557	.9700
.884	1.0509	.9412	.9463	.9635
.832	1.0758	.9334	.9315	.9531
.780	1.0952	.9299	.9214	.9459
.728	1.1147	.9213	.9091	.9371
.676	1.1363	.8971	.8885	.9220
.624	1.1579	.8456	.8546	.8965
.572	1.1838	.7706	.8068	.8592
.520	1.2097	.6631	.7404	.8045
.468	1.1946	.5527	.6802	.7520
.416	1.1795	.4542	.6206	.6974
.364	1.1730	.3888	.5757	.6545
.312	1.1665	.3494	.5473	.6266
.260	1.1676	.3490	.5467	.6261
.208	1.1687	.4262	.6039	.6817
.156	1.2184	.4702	.6212	.6980
.104	1.2194	.4776	.6258	.7023
.052	1.2194	.4776	.6258	.7023
0.000	1.2702	.5112	.6344	.7103
-.052	1.2702	.5084	.6326	.7087
-.104	1.2702	.5530	.6598	.7337
-.156	1.2799	.6302	.7017	.7711
-.208	1.2897	.7664	.7709	.8300
-.260	1.2475	.8723	.8362	.8823
-.312	1.2054	.9142	.8709	.9088
-.364	1.1741	.9234	.8869	.9208
-.416	1.1428	.9242	.8993	.9299
-.468	1.1179	.9304	.9123	.9393
-.520	1.0931	.9315	.9232	.9472
-.572	1.0758	.9363	.9329	.9541
-.624	1.0585	.9311	.9379	.9576
-.676	1.0520	.9322	.9413	.9600
-.728	1.0455	.9284	.9423	.9607
-.780	1.0239	.9356	.9559	.9702
-.832	1.0023	.9344	.9655	.9768
-.884	.9602	.9451	.9921	.9948
-.936	.9181	.9491	1.0167	1.0110
-.988	.8500	.9374	1.0501	1.0323
-1.040	.7820	.9340	1.0929	1.0586

(f) x/D = 4.0; y/D = 0.0; α = 5°;

p_∞ = 221.34 psf (10597.97 N/m^2);
q_∞ = 396.65 psf (18991.56 N/m^2);
$p_{t,\infty}$ = 940.80 psf (45045.75 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1354	.9535	.9164	.9423
.988	1.1397	.9460	.9110	.9385
.936	1.1440	.9435	.9081	.9363
.884	1.1419	.9321	.9035	.9330
.832	1.1397	.9223	.8996	.9301
.780	1.1246	.9082	.8987	.9295
.728	1.1094	.8789	.8901	.9231
.676	1.1203	.8396	.8657	.9050
.624	1.1311	.7882	.8348	.8812
.572	1.1354	.7462	.8107	.8623
.520	1.1397	.7006	.7840	.8408
.468	1.1278	.6736	.7728	.8316
.416	1.1159	.6256	.7487	.8115
.364	1.1094	.6129	.7433	.8069
.312	1.1030	.6108	.7442	.8077
.260	1.0943	.6476	.7693	.8287
.208	1.0857	.6736	.7877	.8438
.156	1.1084	.6689	.7769	.8349
.104	1.0997	.6655	.7779	.8358
.052	1.0954	.6751	.7850	.8416
0.000	1.1138	.7093	.7980	.8521
-.052	1.1094	.7483	.8213	.8707
-.104	1.1051	.7848	.8427	.8874
-.156	1.1343	.8198	.8501	.8931
-.208	1.1635	.8582	.8588	.8997
-.260	1.1581	.8912	.8773	.9136
-.312	1.1527	.9108	.8889	.9223
-.364	1.1516	.9177	.8927	.9251
-.416	1.1505	.9229	.8956	.9272
-.468	1.1527	.9276	.8970	.9283
-.520	1.1549	.9272	.8960	.9275
-.572	1.1538	.9290	.8973	.9285
-.624	1.1527	.9292	.8978	.9289
-.676	1.1527	.9292	.8978	.9289
-.728	1.1527	.9359	.9011	.9312
-.780	1.1549	.9355	.9001	.9305
-.832	1.1570	.9452	.9038	.9332
-.884	1.1581	.9450	.9033	.9329
-.936	1.1592	.9515	.9060	.9348
-.988	1.1581	.9534	.9073	.9358
-1.040	1.1570	.9603	.9110	.9384

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF A WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(g) x/D = 5.0; y/D = 0.0; $\alpha = 5^\circ$;

p_∞ = 221.41 psf (10601.35 N/m^2);
q_∞ = 396.77 psf (18997.61 N/m^2);
$p_{t,\infty}$ = 941.10 psf (45060.11 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0421	.9439	.9517	.9673
.988	1.0464	.9381	.9468	.9639
.936	1.0507	.9255	.9385	.9581
.884	1.0399	.9191	.9401	.9592
.832	1.0291	.8992	.9348	.9554
.780	1.0129	.8820	.9332	.9543
.728	.9967	.8564	.9269	.9499
.676	1.0042	.8197	.9034	.9329
.624	1.0118	.7845	.8806	.9161
.572	1.0096	.7443	.8586	.8996
.520	1.0075	.7261	.8489	.8922
.468	.9956	.7097	.8443	.8886
.416	.9837	.6949	.8405	.8857
.364	.9869	.6994	.8418	.8867
.312	.9902	.7107	.8472	.8908
.260	.9869	.7215	.8550	.8968
.208	.9837	.7323	.8628	.9027
.156	1.0075	.7193	.8449	.8891
.104	1.0042	.7216	.8477	.8912
.052	1.0075	.7346	.8539	.8960
0.000	1.0248	.7669	.8651	.9045
-.052	1.0280	.7957	.8798	.9155
-.104	1.0313	.8237	.8937	.9258
-.156	1.0475	.8476	.8995	.9301
-.208	1.0637	.8647	.9016	.9316
-.260	1.0583	.8925	.9183	.9437
-.312	1.0529	.9035	.9264	.9494
-.364	1.0550	.9148	.9312	.9529
-.416	1.0572	.9144	.9300	.9521
-.468	1.0572	.9295	.9376	.9574
-.520	1.0572	.9278	.9368	.9568
-.572	1.0604	.9306	.9368	.9568
-.624	1.0637	.9266	.9334	.9544
-.676	1.0648	.9298	.9345	.9552
-.728	1.0659	.9279	.9331	.9542
-.780	1.0702	.9372	.9358	.9561
-.832	1.0745	.9347	.9327	.9539
-.884	1.0745	.9414	.9360	.9563
-.936	1.0745	.9531	.9418	.9604
-.988	1.0713	.9537	.9435	.9616
-1.040	1.0680	.9492	.9428	.9610

(h) x/D = 6.0; y/D = 0.0; $\alpha = 5^\circ$;

p_∞ = 221.65 psf (10612.61 N/m^2);
q_∞ = 397.19 psf (19017.80 N/m^2);
$p_{t,\infty}$ = 942.10 psf (45107.99 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0906	.9461	.9314	.9530
.988	1.0950	.9436	.9283	.9509
.936	1.0993	.9278	.9187	.9440
.884	1.0906	.9193	.9181	.9435
.832	1.0820	.9041	.9141	.9407
.780	1.0723	.8756	.9037	.9331
.728	1.0626	.8539	.8964	.9278
.676	1.0842	.8212	.8703	.9084
.624	1.1058	.7883	.8443	.8886
.572	1.1036	.7530	.8260	.8744
.520	1.1014	.7518	.8262	.8745
.468	1.0885	.7253	.8163	.8667
.416	1.0755	.7279	.8227	.8718
.364	1.0572	.7230	.8270	.8751
.312	1.0388	.7282	.8373	.8832
.260	1.0032	.7503	.8648	.9043
.208	.9675	.7485	.8796	.9154
.156	1.0032	.7351	.8560	.8976
.104	.9675	.7485	.8796	.9154
.052	.9708	.7631	.8866	.9206
0.000	.9675	.7856	.9011	.9312
-.052	.9708	.8086	.9126	.9396
-.104	.9740	.8247	.9202	.9450
-.156	.9967	.8507	.9239	.9477
-.208	1.0194	.8666	.9221	.9464
-.260	1.0572	.8966	.9209	.9456
-.312	1.0950	.9047	.9090	.9370
-.364	1.1101	.9237	.9122	.9393
-.416	1.1252	.9210	.9047	.9339
-.468	1.1252	.9310	.9096	.9374
-.520	1.1252	.9327	.9105	.9380
-.572	1.1198	.9387	.9156	.9417
-.624	1.1144	.9397	.9183	.9437
-.676	1.1241	.9362	.9126	.9396
-.728	1.1338	.9361	.9086	.9367
-.780	1.1263	.9392	.9132	.9400
-.832	1.1187	.9406	.9169	.9427
-.884	1.1122	.9501	.9242	.9479
-.936	1.1058	.9546	.9291	.9514
-.988	1.1047	.9581	.9313	.9530
-1.040	1.1036	.9550	.9302	.9522

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF A WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(i) $x/D = 7.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 221.60 psf (10610.36 N/m²);
q_∞ = 397.11 psf (19013.76 N/m²);
$p_{t,\infty}$ = 941.90 psf (45098.42 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0388	.9514	.9570	.9710
.988	1.0593	.9495	.9467	.9638
.936	1.0798	.9324	.9292	.9515
.884	1.1068	.9224	.9129	.9398
.832	1.1338	.9023	.8921	.9246
.780	1.1889	.8751	.8579	.8990
.728	1.2439	.8355	.8195	.8693
.676	1.2655	.8020	.7961	.8506
.624	1.2871	.7787	.7778	.8357
.572	1.3055	.7401	.7530	.8151
.520	1.3239	.7152	.7350	.7999
.468	1.3131	.7123	.7365	.8012
.416	1.3023	.7023	.7344	.7994
.364	1.2850	.7043	.7404	.8045
.312	1.2677	.7185	.7529	.8150
.260	1.2547	.7335	.7646	.8248
.208	1.2418	.7292	.7663	.8262
.156	1.2720	.7298	.7575	.8189
.104	1.2591	.7412	.7673	.8270
.052	1.2547	.7560	.7762	.8344
0.000	1.2763	.7775	.7805	.8379
-.052	1.2720	.8052	.7956	.8502
-.104	1.2677	.8316	.8099	.8617
-.156	1.2947	.8484	.8095	.8613
-.208	1.3217	.8686	.8107	.8623
-.260	1.2936	.8877	.8284	.8762
-.312	1.2655	.9084	.8472	.8909
-.364	1.2321	.9232	.8656	.9049
-.416	1.1986	.9345	.8830	.9179
-.468	1.1738	.9391	.8945	.9264
-.520	1.1489	.9370	.9031	.9327
-.572	1.1219	.9436	.9171	.9428
-.624	1.0949	.9434	.9282	.9508
-.676	1.0507	.9514	.9516	.9672
-.728	1.0064	.9409	.9669	.9777
-.780	.9956	.9428	.9731	.9820
-.832	.9848	.9364	.9751	.9833
-.884	.9762	.9462	.9845	.9897
-.936	.9675	.9477	.9897	.9932
-.988	.9675	.9477	.9897	.9932
-1.040	.9675	.9494	.9906	.9937

(j) $x/D = 8.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 221.72 psf (10615.99 N/m²);
q_∞ = 397.32 psf (19023.85 N/m²);
$p_{t,\infty}$ = 942.40 psf (45122.36 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1980	.9438	.8876	.9213
.988	1.1936	.9345	.8848	.9192
.936	1.1893	.9184	.8787	.9147
.884	1.1850	.9023	.8726	.9101
.832	1.1807	.8828	.8647	.9042
.780	1.1699	.8577	.8563	.8978
.728	1.1591	.8445	.8536	.8957
.676	1.1688	.8035	.8291	.8768
.624	1.1785	.7812	.8141	.8650
.572	1.1742	.7666	.8080	.8601
.520	1.1699	.7555	.8036	.8566
.468	1.1591	.7628	.8112	.8627
.416	1.1483	.7632	.8152	.8659
.364	1.1537	.7553	.8091	.8610
.312	1.1591	.7576	.8085	.8605
.260	1.1472	.7617	.8148	.8656
.208	1.1354	.7640	.8203	.8699
.156	1.1699	.7606	.8063	.8588
.104	1.1580	.7698	.8153	.8660
.052	1.1559	.7822	.8226	.8717
0.000	1.1807	.8046	.8255	.8740
-.052	1.1785	.8146	.8314	.8786
-.104	1.1764	.8353	.8427	.8873
-.156	1.2142	.8534	.8384	.8840
-.208	1.2519	.8681	.8327	.8796
-.260	1.2498	.8838	.8409	.8860
-.312	1.2476	.8977	.8483	.8917
-.364	1.2401	.9093	.8563	.8978
-.416	1.2325	.9225	.8651	.9045
-.468	1.2347	.9254	.8658	.9050
-.520	1.2368	.9284	.8664	.9055
-.572	1.2293	.9315	.8705	.9086
-.624	1.2217	.9380	.8762	.9128
-.676	1.2282	.9351	.8726	.9101
-.728	1.2347	.9372	.8713	.9091
-.780	1.2303	.9380	.8732	.9106
-.832	1.2260	.9506	.8805	.9161
-.884	1.2271	.9504	.8801	.9157
-.936	1.2282	.9603	.8842	.9188
-.988	1.2325	.9578	.8815	.9168
-1.040	1.2368	.9604	.8812	.9165

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF A WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Concluded

(k) x/D = 8.39; y/D = 0.0; $\alpha = 5^\circ$;

p_∞ = 221.70 psf (10614.86 N/m^2);
q_∞ = 397.28 psf (19021.83 N/m^2);
$p_{t,\infty}$ = 942.30 psf (45117.57 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1333	.9398	.9106	.9382
.988	1.1333	.9297	.9057	.9346
.936	1.1333	.9129	.8975	.9286
.884	1.1290	.9002	.8930	.9253
.832	1.1247	.8758	.8824	.9175
.780	1.1128	.8662	.8823	.9174
.728	1.1009	.8448	.8760	.9127
.676	1.1171	.8113	.8522	.8947
.624	1.1333	.7879	.8338	.8805
.572	1.1344	.7860	.8324	.8794
.520	1.1355	.7738	.8255	.8740
.468	1.1355	.7670	.8219	.8711
.416	1.1355	.7670	.8219	.8711
.364	1.1560	.7698	.8160	.8665
.312	1.1765	.7675	.8077	.8599
.260	1.1711	.7685	.8101	.8618
.208	1.1657	.7679	.8116	.8630
.156	1.1938	.7674	.8018	.8552
.104	1.1884	.7753	.8077	.8599
.052	1.1841	.7865	.8150	.8657
0.000	1.2110	.8067	.8162	.8666
-.052	1.2067	.8194	.8240	.8728
-.104	1.2024	.8406	.8361	.8823
-.156	1.2283	.8508	.8323	.8793
-.208	1.2542	.8610	.8285	.8764
-.260	1.2413	.8838	.8438	.8882
-.312	1.2283	.8964	.8543	.8963
-.364	1.2262	.9070	.8600	.9007
-.416	1.2240	.9208	.8674	.9062
-.468	1.2337	.9224	.8647	.9042
-.520	1.2434	.9256	.8628	.9027
-.572	1.2391	.9298	.8662	.9053
-.624	1.2348	.9356	.8705	.9085
-.676	1.2337	.9342	.8702	.9083
-.728	1.2326	.9377	.8722	.9098
-.780	1.2272	.9387	.8746	.9116
-.832	1.2218	.9498	.8817	.9169
-.884	1.2164	.9492	.8833	.9182
-.936	1.2110	.9535	.8873	.9211
-.988	1.2046	.9564	.8911	.9239
-1.040	1.1981	.9593	.8948	.9266

TABLE 6.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 101.20 psf (4845.35 N/m^2);
q_∞ = 374.73 psf (17942.35 N/m^2);
$p_{t,\infty}$ = 1265.40 psf (60587.68 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8203	.7122	.9318	.9651
.988	.7492	.6896	.9594	.9796
.936	.6781	.6652	.9904	.9953
.884	.6401	.6417	1.0013	1.0006
.832	.6022	.6236	1.0176	1.0084
.780	.5690	.6033	1.0297	1.0141
.728	.5358	.5830	1.0431	1.0203
.676	.5097	.5622	1.0502	1.0235
.624	.4837	.5466	1.0631	1.0292
.572	.4505	.5403	1.0952	1.0430
.520	.4173	.5393	1.1368	1.0600
.468	.4386	.3522	.8961	.9452
.416	.4599	.0983	.4622	.5989
.364	.4599	.0191	.2036	.2859
.312	.4599	.0040	.0938	.1340
.260	.4623	.0002	.0232	.0333
.208	.4647	0.0000	0.0000	0.0000
.156	.4765	0.0000	0.0000	0.0000
.104	.4884	0.0000	0.0000	0.0000
.052	.4647	0.0000	0.0000	0.0000
0.000	.4410	.0028	.0794	.1135
-.104	.4552	.0023	.0710	.1016
-.156	.4599	.0010	.0472	.0677
-.208	.4647	.0029	.0795	.1136
-.260	.4410	.0209	.2175	.3045
-.312	.4457	.0760	.4130	.5454
-.364	.4647	.2219	.6910	.8080
-.416	.4268	.5252	1.1094	1.0489
-.468	.4457	.5448	1.1056	1.0474
-.520	.4647	.5557	1.0935	1.0423
-.572	.4765	.5706	1.0942	1.0426
-.624	.4884	.5784	1.0883	1.0401
-.676	.5287	.5912	1.0575	1.0267
-.728	.5690	.6058	1.0318	1.0151
-.780	.5975	.6229	1.0211	1.0101
-.832	.6259	.6418	1.0126	1.0061
-.884	.6520	.6626	1.0081	1.0039
-.936	.6781	.6905	1.0091	1.0044
-.988	.7421	.7137	.9807	.9905
-1.040	.8061	.7440	.9607	.9803

(b) $x/D = 1.5$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 101.36 psf (4853.01 N/m^2);
q_∞ = 375.33 psf (17970.70 N/m^2);
$p_{t,\infty}$ = 1267.40 psf (60683.44 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6728	.6697	.9977	.9989
.988	.6160	.6531	1.0297	1.0141
.936	.5591	.6364	1.0668	1.0309
.884	.5307	.6210	1.0818	1.0373
.832	.5023	.6057	1.0982	1.0443
.780	.4762	.5937	1.1166	1.0518
.728	.4501	.5834	1.1384	1.0606
.676	.4478	.5783	1.1365	1.0598
.624	.4454	.5855	1.1465	1.0637
.572	.5117	.5998	1.0826	1.0377
.520	.5781	.6228	1.0379	1.0179
.468	.6610	.6689	1.0059	1.0029
.416	.7439	.5684	.8741	.9325
.364	.7321	.2700	.6073	.7389
.312	.7202	.1082	.3876	.5165
.260	.7202	.0219	.1743	.2461
.208	.7202	.0067	.0965	.1378
.156	.7416	0.0000	0.0000	0.0000
.104	.7629	.0048	.0795	.1137
.052	.7344	.0495	.2596	.3598
0.000	.7060	.0634	.2998	.4109
-.104	.8103	.0632	.2794	.3852
-.156	.8055	.1107	.3707	.4969
-.208	.8008	.2543	.5635	.6994
-.260	.7368	.5120	.8336	.9078
-.312	.7321	.6492	.9417	.9704
-.364	.6373	.6406	1.0026	1.0012
-.416	.6634	.6421	.9839	.9921
-.468	.5686	.6562	1.0742	1.0341
-.520	.4738	.5844	1.1106	1.0494
-.572	.4620	.5870	1.1272	1.0561
-.624	.4501	.5949	1.1496	1.0649
-.676	.4786	.6016	1.1211	1.0537
-.728	.5070	.6100	1.0969	1.0437
-.780	.5283	.6189	1.0823	1.0376
-.832	.5497	.6331	1.0732	1.0336
-.884	.5544	.6485	1.0815	1.0372
-.936	.5591	.6674	1.0925	1.0419
-.988	.6018	.6817	1.0644	1.0298
-1.040	.6444	.7048	1.0458	1.0215

TABLE 6.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) - Continued

(c) x/D = 2.0; y/D = 0.0; $\alpha = 5^o$;

p_∞ = 101.34 psf (4852.25 N/m^2);
q_∞ = 375.27 psf (17967.87 N/m^2);
$p_{t,\infty}$ = 1267.20 psf (60673.86 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6063	.6521	1.0371	1.0175
.988	.5590	.6400	1.0700	1.0322
.936	.5116	.6278	1.1077	1.0482
.884	.4926	.6135	1.1159	1.0516
.832	.4737	.6044	1.1296	1.0571
.780	.5068	.6020	1.0898	1.0408
.728	.5400	.7075	1.1446	1.0630
.676	.7058	.7267	1.0147	1.0071
.624	.8716	.7177	.9074	.9516
.572	.8905	.7180	.8979	.9463
.520	.9095	.7235	.8919	.9429
.468	.9142	.7284	.8926	.9432
.416	.9190	.7193	.8847	.9387
.364	.9095	.6816	.8657	.9275
.312	.9000	.6211	.8307	.9060
.260	.9166	.4969	.7363	.8420
.208	.9332	.3931	.6490	.7744
.156	1.0066	.2799	.5273	.6650
.104	1.0800	.3110	.5367	.6740
.052	1.0800	.4050	.6124	.7433
0.000	1.0800	.4904	.6738	.7945
-.104	1.1700	.7005	.7738	.8685
-.156	1.1700	.7691	.8108	.8933
-.208	1.1700	.7832	.8181	.8980
-.260	1.0421	.7773	.8637	.9263
-.312	1.0421	.7721	.8607	.9245
-.364	.9190	.7710	.9160	.9564
-.416	.9142	.7258	.8910	.9423
-.468	.7911	.6809	.9277	.9629
-.520	.6679	.6446	.9824	.9913
-.572	.6371	.6487	1.0090	1.0044
-.624	.6063	.6650	1.0472	1.0221
-.676	.6561	.6788	1.0172	1.0082
-.728	.7058	.6978	.9943	.9972
-.780	.6229	.6672	1.0350	1.0165
-.832	.5400	.6384	1.0873	1.0397
-.884	.5258	.6464	1.1088	1.0487
-.936	.5116	.6614	1.1371	1.0600
-.988	.5400	.6716	1.1152	1.0513
-1.040	.5684	.6870	1.0993	1.0448

(d) x/D = 2.5; y/D = 0.0; $\alpha = 5^o$;

p_∞ = 101.21 psf (4845.74 N/m^2);
q_∞ = 374.76 psf (17943.76 N/m^2);
$p_{t,\infty}$ = 1265.50 psf (60592.47 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6217	.6937	1.0564	1.0262
.988	.6644	.7273	1.0463	1.0217
.936	.7071	.7241	1.0120	1.0058
.884	.7759	.7522	.9846	.9924
.832	.8447	.7558	.9459	.9726
.780	.8874	.7578	.9241	.9609
.728	.9301	.7598	.9038	.9496
.676	.9515	.7582	.8927	.9433
.624	.9728	.7583	.8829	.9376
.572	1.0013	.7561	.8690	.9295
.520	1.0298	.7522	.8546	.9208
.468	1.0179	.7373	.8511	.9187
.416	1.0060	.7066	.8381	.9106
.364	.9871	.6536	.8138	.8952
.312	.9681	.6024	.7888	.8787
.260	.9728	.5368	.7428	.8467
.208	.9776	.4833	.7032	.8173
.156	1.0203	.4317	.6505	.7756
.104	1.0630	.4476	.6489	.7743
.052	1.0749	.5000	.6820	.8010
0.000	1.0867	.5946	.7397	.8445
-.104	1.1057	.7322	.8138	.8952
-.156	1.1199	.7487	.8177	.8977
-.208	1.1342	.7670	.8224	.9007
-.260	1.1081	.7620	.8293	.9051
-.312	1.1223	.7626	.8243	.9020
-.364	1.1128	.7669	.8302	.9057
-.416	1.1104	.7741	.8350	.9087
-.468	1.1010	.7802	.8418	.9129
-.520	1.0915	.7827	.8468	.9160
-.572	1.0369	.7869	.8711	.9307
-.624	.9823	.7911	.8974	.9460
-.676	.8138	.6897	.9206	.9590
-.728	.6454	.6796	1.0262	1.0125
-.780	.6644	.6869	1.0168	1.0081
-.832	.6833	.7031	1.0143	1.0069
-.884	.6857	.7204	1.0250	1.0119
-.936	.6881	.7448	1.0404	1.0190
-.988	.6881	.7641	1.0538	1.0251
-1.040	.6881	.7728	1.0598	1.0277

TABLE 6. - VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) - Continued

(e) $x/D = 3.0$; $y/D = 0.0$; $\alpha = 5^o$;

p_∞ = 101.25 psf (4847.65 N/m^2);
q_∞ = 374.91 psf (17950.85 N/m^2);
$p_{t,\infty}$ = 1266.00 psf (60616.41 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8875	.7993	.9491	.9742
.988	.9088	.8047	.9410	.9700
.936	.9302	.8066	.9312	.9647
.884	.9610	.8077	.9168	.9569
.832	.9919	.8054	.9011	.9481
.780	1.0037	.7975	.8914	.9425
.728	1.0156	.7826	.8778	.9347
.676	1.0085	.7691	.8733	.9320
.624	1.0014	.7557	.8687	.9293
.572	.9919	.7424	.8652	.9272
.520	.9824	.7309	.8626	.9256
.468	.9681	.7075	.8549	.9210
.416	.9539	.6753	.8414	.9127
.364	.9515	.6387	.8193	.8988
.312	.9492	.5968	.7930	.8815
.260	.9563	.5594	.7648	.8623
.208	.9634	.5306	.7422	.8463
.156	.9942	.5017	.7103	.8228
.104	1.0251	.5079	.7039	.8179
.052	1.0275	.5536	.7340	.8404
0.000	1.0298	.6273	.7804	.8731
-.104	1.0251	.7224	.8395	.9115
-.156	1.0322	.7306	.8413	.9127
-.208	1.0393	.7389	.8432	.9138
-.260	1.0275	.7398	.8485	.9171
-.312	1.0346	.7410	.8463	.9157
-.364	1.0393	.7459	.8472	.9163
-.416	1.0298	.7537	.8555	.9213
-.468	1.0346	.7604	.8573	.9224
-.520	1.0393	.7705	.8610	.9247
-.572	1.0441	.7807	.8647	.9269
-.624	1.0488	.7909	.8684	.9291
-.676	1.0559	.8027	.8719	.9312
-.728	1.0631	.8144	.8753	.9332
-.780	1.0488	.8278	.8884	.9408
-.832	1.0346	.8412	.9017	.9484
-.884	.8305	.7935	.9774	.9888
-.936	.6264	.7297	1.0793	1.0363
-.988	.6549	.7399	1.0629	1.0291
-1.040	.6834	.7571	1.0525	1.0245

(f) $x/D = 4.0$; $y/D = 0.0$; $\alpha = 5^o$;

p_∞ = 101.31 psf (4850.71 N/m^2);
q_∞ = 375.15 psf (17962.20 N/m^2);
$p_{t,\infty}$ = 1266.80 psf (60654.71 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0237	.8596	.9163	.9566
.988	1.0190	.8407	.9083	.9521
.936	1.0143	.8305	.9049	.9502
.884	1.0166	.8181	.8971	.9458
.832	1.0190	.8074	.8901	.9418
.780	1.0190	.7969	.8843	.9385
.728	1.0190	.7793	.8745	.9327
.676	1.0048	.7629	.8713	.9309
.624	.9906	.7464	.8681	.9289
.572	.9834	.7294	.8612	.9248
.520	.9763	.7089	.8521	.9193
.468	.9716	.6865	.8405	.9122
.416	.9669	.6570	.8243	.9020
.364	.9621	.6345	.8121	.8941
.312	.9574	.6190	.8041	.8889
.260	.9574	.5962	.7891	.8789
.208	.9574	.5786	.7774	.8710
.156	.9763	.5594	.7569	.8568
.104	.9953	.5614	.7510	.8526
.052	.9929	.5898	.7707	.8664
0.000	.9906	.6358	.8011	.8869
-.104	.9858	.7082	.8476	.9165
-.156	.9953	.7180	.8493	.9176
-.208	1.0048	.7260	.8500	.9180
-.260	.9929	.7304	.8577	.9227
-.312	1.0024	.7332	.8553	.9212
-.364	1.0048	.7383	.8572	.9224
-.416	1.0000	.7474	.8645	.9268
-.468	1.0024	.7525	.8664	.9279
-.520	1.0048	.7611	.8703	.9303
-.572	1.0048	.7699	.8753	.9332
-.624	1.0048	.7822	.8823	.9373
-.676	1.0119	.7921	.8848	.9387
-.728	1.0190	.8039	.8882	.9407
-.780	1.0166	.8146	.8951	.9447
-.832	1.0143	.8288	.9040	.9497
-.884	1.0166	.8426	.9104	.9533
-.936	1.0190	.8565	.9168	.9569
-.988	1.0143	.8673	.9247	.9612
-1.040	1.0095	.8782	.9327	.9655

TABLE 6.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) - *Continued*

(g) $x/D = 5.0$; $y/D = 0.0$; $\alpha = 5^o$;

p_∞ = 101.36 psf (4853.01 N/m^2);
q_∞ = 375.33 psf (17970.70 N/m^2);
$p_{t,\infty}$ = 1267.40 psf (60683.44 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1938	.9000	.8683	.9290
.988	1.1819	.8869	.8662	.9278
.936	1.1701	.8773	.8659	.9276
.884	1.1748	.8647	.8579	.9228
.832	1.1796	.8503	.8490	.9174
.780	1.1867	.8375	.8401	.9119
.728	1.1938	.8195	.8285	.9046
.676	1.1748	.7999	.8251	.9025
.624	1.1559	.7874	.8253	.9026
.572	1.1488	.7634	.8152	.8961
.520	1.1417	.7464	.8086	.8918
.468	1.1488	.7318	.7981	.8850
.416	1.1559	.7120	.7848	.8761
.364	1.1440	.7006	.7826	.8745
.312	1.1322	.6857	.7783	.8716
.260	1.1251	.6635	.7679	.8645
.208	1.1180	.6447	.7594	.8585
.156	1.1393	.6201	.7378	.8431
.104	1.1606	.6095	.7247	.8335
.052	1.1606	.6166	.7289	.8366
0.000	1.1606	.6465	.7464	.8493
-.104	1.1464	.7207	.7929	.8815
-.156	1.1417	.7475	.8091	.8922
-.208	1.1369	.7619	.8186	.8983
-.260	1.1393	.7670	.8205	.8995
-.312	1.1346	.7726	.8252	.9025
-.364	1.1346	.7779	.8280	.9043
-.416	1.1322	.7851	.8327	.9073
-.468	1.1322	.7939	.8374	.9102
-.520	1.1322	.8010	.8411	.9125
-.572	1.1393	.8109	.8437	.9141
-.624	1.1464	.8209	.8462	.9157
-.676	1.1583	.8306	.8468	.9160
-.728	1.1701	.8437	.8491	.9175
-.780	1.1630	.8583	.8591	.9235
-.832	1.1559	.8746	.8699	.9300
-.884	1.1535	.8889	.8778	.9347
-.936	1.1512	.9013	.8849	.9388
-.988	1.1322	.9116	.8973	.9459
-1.040	1.1133	.9183	.9082	.9521

(h) $x/D = 6.0$; $y/D = 0.0$; $\alpha = 5^o$;

p_∞ = 101.49 psf (4859.14 N/m^2);
q_∞ = 375.80 psf (17993.39 N/m^2);
$p_{t,\infty}$ = 1269.00 psf (60760.05 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1452	.8762	.8747	.9328
.988	1.1192	.8642	.8787	.9352
.936	1.0932	.8522	.8829	.9377
.884	1.0884	.8386	.8778	.9346
.832	1.0837	.8285	.8744	.9326
.780	1.0884	.8142	.8649	.9270
.728	1.0932	.8033	.8572	.9224
.676	1.0884	.7897	.8518	.9191
.624	1.0837	.7796	.8481	.9169
.572	1.0837	.7656	.8405	.9121
.520	1.0837	.7568	.8357	.9091
.468	1.0955	.7437	.8239	.9017
.416	1.1074	.7305	.8122	.8942
.364	1.0955	.7227	.8122	.8942
.312	1.0837	.7096	.8092	.8922
.260	1.0790	.6889	.7991	.8856
.208	1.0743	.6718	.7908	.8801
.156	1.0884	.6461	.7705	.8662
.104	1.1026	.6274	.7543	.8550
.052	1.1050	.6202	.7492	.8513
0.000	1.1074	.6323	.7556	.8559
-.104	1.0837	.6876	.7966	.8839
-.156	1.0814	.7195	.8157	.8964
-.208	1.0790	.7407	.8285	.9047
-.260	1.0790	.7512	.8344	.9083
-.312	1.0766	.7585	.8393	.9114
-.364	1.0790	.7635	.8412	.9126
-.416	1.0743	.7709	.8471	.9162
-.468	1.0766	.7778	.8499	.9180
-.520	1.0790	.7828	.8518	.9191
-.572	1.0814	.7914	.8555	.9214
-.624	1.0837	.8000	.8592	.9236
-.676	1.0932	.8080	.8597	.9239
-.728	1.1026	.8213	.8631	.9259
-.780	1.1003	.8338	.8705	.9304
-.832	1.0979	.8445	.8770	.9342
-.884	1.1026	.8599	.8831	.9378
-.936	1.1074	.8771	.8900	.9417
-.988	1.1192	.8902	.8918	.9428
-1.040	1.1310	.9050	.8945	.9443

TABLE 6.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) - Continued

(i) x/D = 7.0; y/D = 0.0; $\alpha = 5^\circ$;

p_∞ = 101.45 psf (4857.22 N/m^2);
q_∞ = 375.65 psf (17986.30 N/m^2);
$p_{t,\infty}$ = 1268.50 psf (60736.11 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0614	.8606	.9005	.9477
.988	1.0377	.8449	.9023	.9488
.936	1.0140	.8345	.9072	.9515
.884	1.0117	.8242	.9026	.9489
.832	1.0093	.8121	.8970	.9458
.780	1.0117	.7997	.8891	.9412
.728	1.0140	.7890	.8821	.9372
.676	1.0117	.7751	.8753	.9332
.624	1.0093	.7666	.8715	.9309
.572	1.0093	.7578	.8665	.9280
.520	1.0093	.7491	.8615	.9250
.468	1.0188	.7378	.8510	.9186
.416	1.0282	.7283	.8416	.9128
.364	1.0188	.7220	.8419	.9130
.312	1.0093	.7122	.8400	.9119
.260	1.0069	.6966	.8318	.9067
.208	1.0045	.6810	.8234	.9014
.156	1.0140	.6575	.8052	.8896
.104	1.0235	.6391	.7902	.8797
.052	1.0259	.6249	.7805	.8731
0.000	1.0282	.6317	.7838	.8754
-.104	1.0093	.6798	.8207	.8996
-.156	1.0140	.6987	.8301	.9056
-.208	1.0188	.7194	.8403	.9120
-.260	1.0093	.7324	.8519	.9191
-.312	1.0140	.7391	.8537	.9203
-.364	1.0164	.7459	.8567	.9221
-.416	1.0093	.7535	.8640	.9265
-.468	1.0117	.7586	.8659	.9276
-.520	1.0140	.7636	.8678	.9287
-.572	1.0140	.7724	.8728	.9317
-.624	1.0140	.7812	.8777	.9346
-.676	1.0188	.7896	.8804	.9362
-.728	1.0235	.8015	.8849	.9388
-.780	1.0211	.8104	.8909	.9423
-.832	1.0188	.8246	.8997	.9473
-.884	1.0211	.8367	.9052	.9504
-.936	1.0235	.8506	.9116	.9540
-.988	1.0330	.8621	.9136	.9551
-1.040	1.0425	.8771	.9173	.9571

(j) x/D = 8.0; y/D = 0.0; $\alpha = 5^\circ$;

p_∞ = 101.39 psf (4854.54 N/m^2);
q_∞ = 375.44 psf (17976.38 N/m^2);
$p_{t,\infty}$ = 1267.80 psf (60702.59 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9990	.8481	.9214	.9594
.988	.9777	.8288	.9207	.9590
.936	.9564	.8181	.9249	.9613
.884	.9540	.8078	.9202	.9587
.832	.9517	.7975	.9154	.9561
.780	.9540	.7869	.9082	.9521
.728	.9564	.7762	.9009	.9480
.676	.9564	.7622	.8927	.9433
.624	.9564	.7535	.8876	.9404
.572	.9564	.7448	.8824	.9374
.520	.9564	.7378	.8783	.9349
.468	.9611	.7304	.8717	.9311
.416	.9659	.7195	.8631	.9259
.364	.9588	.7113	.8614	.9249
.312	.9517	.7049	.8606	.9245
.260	.9493	.6893	.8521	.9193
.208	.9469	.6773	.8457	.9154
.156	.9517	.6524	.8280	.9043
.104	.9564	.6397	.8179	.8978
.052	.9611	.6271	.8077	.8913
0.000	.9659	.6355	.8111	.8935
-.104	.9517	.6715	.8400	.9118
-.156	.9564	.6852	.8464	.9158
-.208	.9611	.7041	.8559	.9216
-.260	.9540	.7187	.8680	.9288
-.312	.9588	.7236	.8687	.9293
-.364	.9588	.7306	.8729	.9318
-.416	.9564	.7361	.8773	.9344
-.468	.9564	.7431	.8814	.9368
-.520	.9564	.7518	.8866	.9398
-.572	.9564	.7571	.8897	.9416
-.624	.9564	.7641	.8938	.9439
-.676	.9611	.7725	.8965	.9455
-.728	.9659	.7844	.9012	.9481
-.780	.9635	.7951	.9084	.9522
-.832	.9611	.8075	.9166	.9568
-.884	.9635	.8178	.9213	.9593
-.936	.9659	.8334	.9289	.9635
-.988	.9730	.8469	.9330	.9657
-1.040	.9801	.8586	.9360	.9673

TABLE 6.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) - Concluded

(k) $x/D = 8.39$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 101.50 psf (4859.90 N/m^2);
q_∞ = 375.86 psf (17996.23 N/m^2);
$p_{t,\infty}$ = 1269.20 psf (60769.62 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9837	.8430	.9257	.9618
.988	.9624	.8219	.9241	.9609
.936	.9412	.8131	.9295	.9638
.884	.9388	.7993	.9227	.9601
.832	.9364	.7908	.9189	.9580
.780	.9388	.7801	.9116	.9540
.728	.9412	.7677	.9032	.9493
.676	.9412	.7590	.8980	.9463
.624	.9412	.7450	.8897	.9416
.572	.9412	.7380	.8855	.9392
.520	.9412	.7310	.8813	.9367
.468	.9435	.7239	.8759	.9335
.416	.9459	.7150	.8694	.9297
.364	.9412	.7066	.8665	.9280
.312	.9364	.6982	.8635	.9262
.260	.9341	.6827	.8549	.9210
.208	.9317	.6689	.8473	.9163
.156	.9364	.6493	.8327	.9073
.104	.9412	.6384	.8236	.9015
.052	.9435	.6242	.8134	.8949
0.000	.9459	.6310	.8168	.8971
-.104	.9364	.6684	.8449	.9148
-.156	.9435	.6819	.8501	.9181
-.208	.9506	.6988	.8574	.9225
-.260	.9388	.7120	.8709	.9306
-.312	.9459	.7202	.8726	.9316
-.364	.9459	.7237	.8747	.9328
-.416	.9412	.7311	.8814	.9367
-.468	.9412	.7363	.8845	.9386
-.520	.9412	.7416	.8877	.9404
-.572	.9388	.7488	.8931	.9435
-.624	.9364	.7577	.8995	.9472
-.676	.9388	.7645	.9024	.9488
-.728	.9412	.7748	.9073	.9516
-.780	.9388	.7855	.9147	.9557
-.832	.9364	.7962	.9221	.9598
-.884	.9388	.8082	.9279	.9629
-.936	.9412	.8220	.9346	.9666
-.988	.9483	.8337	.9377	.9682
-1.040	.9553	.8489	.9427	.9709

TABLE 7.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER)

(a) x/D = 1.0; y/D = 0.0; α = 5°;

p_∞ = 51.84 psf (2482.21 N/m^2);
q_∞ = 317.95 psf (15223.71 N/m^2);
$p_{t,\infty}$ = 1793.20 psf (85858.88 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0098	.6329	.7917	.9067
.988	.8801	.5995	.8254	.9245
.936	.7504	.5703	.8718	.9471
.884	.6994	.5416	.8800	.9509
.832	.6485	.5212	.8965	.9584
.780	.5975	.5029	.9174	.9675
.728	.5466	.4824	.9395	.9767
.676	.5142	.4612	.9471	.9798
.624	.4817	.4420	.9579	.9841
.572	.4123	.4245	1.0147	1.0053
.520	.3428	.4110	1.0950	1.0316
.468	.3428	.4069	1.0895	1.0299
.416	.3428	.3802	1.0531	1.0184
.364	.4123	.1544	.6120	.7889
.312	.4817	.0517	.3277	.4988
.260	.4956	.0095	.1384	.2258
.208	.5095	.0038	.0862	.1421
.156	.5234	0.0000	0.0000	0.0000
.104	.5373	0.0000	0.0000	0.0000
.052	.5234	.0088	.1298	.2122
0.000	.5095	.0109	.1462	.2381
-.104	.5466	.0089	.1278	.2091
-.156	.5281	.0117	.1488	.2423
-.208	.5095	.0441	.2943	.4549
-.260	.4817	.1596	.5755	.7595
-.312	.4632	.3259	.8388	.9313
-.364	.4817	.3931	.9034	.9614
-.416	.4169	.4227	1.0070	1.0025
-.468	.4354	.4363	1.0011	1.0004
-.520	.4539	.4499	.9956	.9984
-.572	.4632	.4640	1.0008	1.0003
-.624	.4725	.4780	1.0058	1.0021
-.676	.5281	.4859	.9592	.9846
-.728	.5836	.4979	.9236	.9701
-.780	.6300	.5164	.9054	.9623
-.832	.6763	.5433	.8963	.9583
-.884	.7226	.5763	.8930	.9568
-.936	.7689	.6093	.8902	.9556
-.988	.8569	.6466	.8687	.9457
-1.040	.9449	.6943	.8572	.9402

(b) x/D = 1.5; y/D = 0.0; α = 5°;

p_∞ = 51.87 psf (2483.74 N/m^2);
q_∞ = 318.15 psf (15233.05 N/m^2);
$p_{t,\infty}$ = 1794.30 psf (85911.55 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8232	.5680	.8307	.9272
.988	.7169	.5419	.8695	.9461
.936	.6105	.5240	.9264	.9713
.884	.5735	.5050	.9384	.9763
.832	.5365	.4882	.9539	.9825
.780	.5041	.4752	.9709	.9891
.728	.4717	.4622	.9899	.9963
.676	.4625	.4524	.9890	.9960
.624	.4532	.4445	.9904	.9965
.572	.4162	.4441	1.0329	1.0116
.520	.3792	.4416	1.0790	1.0267
.468	.5087	.4319	.9213	.9691
.416	.6382	.5474	.9261	.9712
.364	.8094	.6036	.8636	.9433
.312	.9805	.5795	.7688	.8939
.260	.9296	.4479	.6941	.8480
.208	.8787	.3098	.5937	.7744
.156	.9897	.1800	.4265	.6162
.104	1.1007	.1863	.4114	.5994
.052	1.1192	.3269	.5405	.7292
0.000	1.1377	.4692	.6422	.8117
-.104	1.4245	.6750	.6884	.8441
-.156	1.1978	.6937	.7610	.8894
-.208	.9712	.6336	.8077	.9153
-.260	1.0776	.5193	.6942	.8480
-.312	.8510	.5069	.7718	.8956
-.364	.7261	.5104	.8384	.9311
-.416	.7307	.5432	.8622	.9426
-.468	.6059	.4539	.8655	.9442
-.520	.4810	.4552	.9728	.9899
-.572	.4625	.4581	.9952	.9982
-.624	.4440	.4630	1.0212	1.0075
-.676	.4810	.4717	.9903	.9964
-.728	.5180	.4824	.9651	.9869
-.780	.5457	.4957	.9530	.9821
-.832	.5735	.5130	.9458	.9792
-.884	.5874	.5330	.9526	.9820
-.936	.6012	.5613	.9662	.9873
-.988	.6614	.5854	.9409	.9772
-1.040	.7215	.6179	.9254	.9709

TABLE 7.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(c) $x/D = 2.0$; $y/D = 0.0$; $\alpha = 5^{\circ}$;

p_∞ = 51.87 psf (2483.74 N/m^2);
q_∞ = 318.15 psf (15233.05 N/m^2);
$p_{t,\infty}$ = 1794.30 psf (85911.55 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7498	.5480	.8550	.9392
.988	.6572	.5295	.8976	.9589
.936	.5646	.5172	.9570	.9837
.884	.5415	.5038	.9646	.9867
.832	.5183	.4925	.9747	.9906
.780	.4998	.4830	.9831	.9937
.728	.4813	.4777	.9962	.9986
.676	.5693	.4780	.9163	.9670
.624	.6572	.5665	.9284	.9721
.572	.8562	.6008	.8377	.9307
.520	1.0552	.6351	.7758	.8979
.468	1.0737	.6404	.7723	.8959
.416	1.0922	.6293	.7591	.8883
.364	1.0830	.6071	.7487	.8822
.312	1.0737	.5828	.7368	.8750
.260	1.0645	.5174	.6972	.8500
.208	1.0552	.4477	.6514	.8184
.156	1.1385	.3671	.5679	.7530
.104	1.2218	.3858	.5619	.7480
.052	1.2496	.4529	.6020	.7811
0.000	1.2774	.5528	.6579	.8231
−.104	1.3607	.6656	.6994	.8514
−.156	1.3792	.6709	.6975	.8502
−.208	1.3977	.6742	.6945	.8482
−.260	1.0182	.6935	.8253	.9244
−.312	1.0367	.6947	.8186	.9210
−.364	1.0413	.6883	.8130	.9181
−.416	.6757	.5209	.8780	.9500
−.468	.6803	.5207	.8748	.9486
−.520	.6850	.5308	.8803	.9511
−.572	.6988	.5467	.8845	.9530
−.624	.7127	.5667	.8917	.9562
−.676	.6248	.5149	.9078	.9633
−.728	.5369	.4981	.9632	.9862
−.780	.5415	.5041	.9648	.9868
−.832	.5461	.5163	.9723	.9897
−.884	.5461	.5327	.9877	.9955
−.936	.5461	.5533	1.0066	1.0024
−.988	.5831	.5724	.9907	.9966
−1.040	.6202	.5955	.9799	.9926

(d) $x/D = 2.5$; $y/D = 0.0$; $\alpha = 5^{\circ}$;

p_∞ = 51.89 psf (2484.57 N/m^2);
q_∞ = 318.26 psf (15238.14 N/m^2);
$p_{t,\infty}$ = 1794.90 psf (85940.28 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7214	.5491	.8724	.9474
.988	.6335	.5365	.9203	.9687
.936	.5457	.5281	.9837	.9940
.884	.6520	.6075	.9653	.9870
.832	.7584	.5926	.8840	.9528
.780	.8740	.6245	.8453	.9345
.728	.9896	.6542	.8131	.9181
.676	1.0174	.6530	.8012	.9118
.624	1.0451	.6477	.7872	.9043
.572	1.0821	.6460	.7726	.8961
.520	1.1191	.6443	.7588	.8881
.468	1.1006	.6308	.7570	.8871
.416	1.0821	.6090	.7502	.8831
.364	1.0636	.5810	.7391	.8765
.312	1.0451	.5531	.7275	.8693
.260	1.0359	.5020	.6962	.8493
.208	1.0266	.4654	.6733	.8339
.156	1.0682	.4366	.6393	.8096
.104	1.1099	.4491	.6361	.8072
.052	1.1191	.4817	.6560	.8218
0.000	1.1284	.5410	.6924	.8468
−.104	1.1654	.6239	.7317	.8719
−.156	1.1792	.6315	.7318	.8720
−.208	1.1931	.6330	.7284	.8699
−.260	1.1746	.6379	.7370	.8752
−.312	1.1885	.6435	.7358	.8745
−.364	1.1885	.6456	.7370	.8752
−.416	1.1838	.6540	.7433	.8790
−.468	1.1838	.6602	.7468	.8811
−.520	1.1838	.6705	.7526	.8845
−.572	.9156	.6949	.8712	.9468
−.624	.6474	.5440	.9167	.9672
−.676	.6798	.5508	.9001	.9600
−.728	.7122	.5700	.8946	.9575
−.780	.7399	.5894	.8925	.9566
−.832	.7677	.6108	.8920	.9564
−.884	.6567	.6444	.9906	.9966
−.936	.5457	.5690	1.0211	1.0075
−.988	.5642	.5785	1.0126	1.0045
−1.040	.5827	.5962	1.0115	1.0041

TABLE 7.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(e) $x/D = 3.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 51.89 psf (2484.29 N/m^2);
q_∞ = 318.22 psf (15236.44 N/m^2);
$p_{t,\infty}$ = 1794.70 psf (85930.70 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8972	.6366	.8423	.9330
.988	.9204	.6500	.8404	.9320
.936	.9435	.6900	.8552	.9393
.884	.9712	.6806	.8371	.9304
.832	.9990	.6773	.8234	.9235
.780	1.0314	.6779	.8107	.9169
.728	1.0637	.6682	.7926	.9072
.676	1.0591	.6540	.7858	.9035
.624	1.0545	.6440	.7815	.9011
.572	1.0452	.6320	.7776	.8989
.520	1.0360	.6180	.7724	.8960
.468	1.0175	.6004	.7681	.8936
.416	.9990	.5765	.7597	.8887
.364	.9851	.5524	.7488	.8823
.312	.9712	.5263	.7361	.8746
.260	.9666	.4956	.7160	.8622
.208	.9620	.4793	.7059	.8556
.156	.9851	.4617	.6846	.8416
.104	1.0082	.4627	.6775	.8367
.052	1.0129	.4852	.6921	.8466
0.000	1.0175	.5242	.7177	.8632
−.104	1.0360	.5906	.7551	.8860
−.156	1.0545	.5981	.7531	.8848
−.208	1.0730	.6034	.7499	.8829
−.260	1.0499	.6106	.7627	.8904
−.312	1.0684	.6139	.7581	.8877
−.364	1.0730	.6179	.7588	.8882
−.416	1.0637	.6245	.7662	.8924
−.468	1.0684	.6325	.7694	.8943
−.520	1.0730	.6426	.7739	.8968
−.572	1.0822	.6546	.7777	.8990
−.624	1.0915	.6686	.7827	.9017
−.676	1.1054	.6865	.7881	.9047
−.728	1.1192	.7086	.7957	.9089
−.780	.9111	.7384	.9002	.9600
−.832	.7030	.5931	.9185	.9679
−.884	.6984	.6139	.9376	.9759
−.936	.6937	.6429	.9627	.9859
−.988	.7354	.6637	.9501	.9810
−1.040	.7770	.6928	.9443	.9786

(f) $x/D = 4.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 51.80 psf (2480.41 N/m^2);
q_∞ = 317.72 psf (15212.67 N/m^2);
$p_{t,\infty}$ = 1791.90 psf (85796.63 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1035	.7223	.8091	.9160
.988	1.0293	.7010	.8252	.9244
.936	.9551	.6816	.8448	.9342
.884	.9505	.6633	.8354	.9296
.832	.9458	.6532	.8311	.9274
.780	.9458	.6430	.8245	.9240
.728	.9458	.6327	.8179	.9206
.676	.9458	.6224	.8112	.9172
.624	.9458	.6100	.8031	.9129
.572	.9458	.5977	.7949	.9085
.520	.9458	.5812	.7839	.9024
.468	.9319	.5613	.7761	.8980
.416	.9180	.5413	.7679	.8934
.364	.9134	.5292	.7611	.8895
.312	.9087	.5129	.7513	.8837
.260	.9041	.5007	.7442	.8795
.208	.8995	.4927	.7401	.8771
.156	.9180	.4816	.7243	.8673
.104	.9366	.4807	.7164	.8624
.052	.9366	.4910	.7241	.8672
0.000	.9366	.5178	.7436	.8791
−.104	.9458	.5613	.7703	.8948
−.156	.9597	.5730	.7727	.8962
−.208	.9737	.5807	.7723	.8959
−.260	.9551	.5815	.7803	.9004
−.312	.9690	.5871	.7784	.8994
−.364	.9690	.5912	.7811	.9009
−.416	.9644	.5977	.7872	.9043
−.468	.9644	.6018	.7899	.9058
−.520	.9644	.6101	.7954	.9087
−.572	.9690	.6181	.7987	.9105
−.624	.9737	.6303	.8046	.9137
−.676	.9783	.6446	.8117	.9174
−.728	.9829	.6609	.8200	.9217
−.780	.9783	.6776	.8323	.9280
−.832	.9737	.6964	.8457	.9347
−.884	.9876	.7206	.8542	.9388
−.936	1.0015	.7510	.8660	.9444
−.988	1.0247	.7768	.8707	.9466
−1.040	1.0478	.8068	.8775	.9498

TABLE 7.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(g) $x/D = 5.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 51.81 psf (2480.69 N/m^2);
q_∞ = 317.76 psf (15214.37 N/m^2);
$p_{t,\infty}$ = 1792.10 psf (85806.21 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0665	.7104	.8161	.9197
.988	1.0016	.6926	.8316	.9277
.936	.9366	.6791	.8515	.9375
.884	.9320	.6628	.8433	.9335
.832	.9274	.6506	.8376	.9307
.780	.9274	.6362	.8283	.9260
.728	.9274	.6259	.8216	.9225
.676	.9227	.6097	.8128	.9180
.624	.9181	.5975	.8067	.9148
.572	.9181	.5852	.7984	.9103
.520	.9181	.5687	.7870	.9042
.468	.9088	.5505	.7783	.8993
.416	.8995	.5365	.7723	.8959
.364	.8995	.5283	.7663	.8925
.312	.8995	.5200	.7603	.8891
.260	.8949	.5120	.7564	.8868
.208	.8903	.5060	.7539	.8853
.156	.9042	.4951	.7400	.8770
.104	.9181	.4924	.7323	.8723
.052	.9227	.5004	.7364	.8748
0.000	.9274	.5188	.7479	.8818
-.104	.9181	.5576	.7794	.8999
-.156	.9320	.5694	.7816	.9012
-.208	.9459	.5770	.7811	.9008
-.260	.9274	.5820	.7922	.9070
-.312	.9413	.5834	.7873	.9043
-.364	.9366	.5857	.7908	.9062
-.416	.9366	.5919	.7950	.9085
-.468	.9320	.5963	.7998	.9111
-.520	.9274	.6027	.8061	.9145
-.572	.9274	.6109	.8116	.9174
-.624	.9274	.6212	.8185	.9209
-.676	.9320	.6355	.8257	.9247
-.728	.9366	.6497	.8329	.9283
-.780	.9366	.6683	.8447	.9342
-.832	.9366	.6889	.8576	.9405
-.884	.9413	.7093	.8681	.9454
-.936	.9459	.7359	.8821	.9519
-.988	.9598	.7580	.8887	.9549
-1.040	.9737	.7822	.8962	.9583

(h) $x/D = 6.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 51.83 psf (2481.66 N/m^2);
q_∞ = 317.88 psf (15220.31 N/m^2);
$p_{t,\infty}$ = 1792.80 psf (85839.73 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0554	.7023	.8158	.9195
.988	.9859	.6828	.8322	.9279
.936	.9165	.6694	.8546	.9390
.884	.9119	.6531	.8463	.9350
.832	.9072	.6389	.8392	.9315
.780	.9072	.6266	.8310	.9274
.728	.9072	.6122	.8214	.9225
.676	.9072	.5978	.8117	.9174
.624	.9072	.5854	.8033	.9130
.572	.9396	.5757	.7827	.9018
.520	.9720	.5578	.7575	.8874
.468	.9906	.5652	.7554	.8861
.416	1.0091	.5561	.7424	.8784
.364	1.0276	.5552	.7351	.8740
.312	1.0461	.5544	.7280	.8696
.260	1.0415	.5567	.7311	.8716
.208	1.0368	.5486	.7274	.8693
.156	1.0646	.5350	.7089	.8576
.104	1.0924	.5358	.7003	.8520
.052	1.0878	.5442	.7073	.8566
0.000	1.0831	.5630	.7210	.8653
-.104	1.0831	.5982	.7431	.8789
-.156	1.0739	.6089	.7530	.8848
-.208	1.0646	.6176	.7617	.8898
-.260	1.0368	.6189	.7726	.8961
-.312	1.0276	.6152	.7737	.8967
-.364	1.0044	.6100	.7793	.8999
-.416	.9906	.6168	.7891	.9053
-.468	.9674	.6075	.7925	.9071
-.520	.9443	.6106	.8042	.9134
-.572	.9350	.6110	.8084	.9157
-.624	.9258	.6218	.8195	.9215
-.676	.9258	.6321	.8263	.9250
-.728	.9258	.6466	.8357	.9297
-.780	.9211	.6612	.8473	.9354
-.832	.9165	.6821	.8627	.9429
-.884	.9211	.7046	.8746	.9484
-.936	.9258	.7312	.8887	.9549
-.988	.9396	.7512	.8941	.9573
-1.040	.9535	.7754	.9018	.9607

TABLE 7.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(i) $x/D = 7.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 51.84 psf (2482.35 N/m^2);
q_∞ = 317.97 psf (15224.56 N/m^2);
$p_{t,\infty}$ = 1793.30 psf (85863.67 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3241	.7992	.7769	.8985
.988	1.2593	.7794	.7867	.9040
.936	1.1944	.7597	.7975	.9099
.884	1.1852	.7375	.7888	.9051
.832	1.1759	.7214	.7833	.9021
.780	1.1620	.7014	.7769	.8985
.728	1.1481	.6856	.7727	.8962
.676	1.1389	.6675	.7656	.8921
.624	1.1296	.6535	.7606	.8892
.572	1.1250	.6413	.7550	.8860
.520	1.1204	.6271	.7482	.8819
.468	1.1204	.6189	.7432	.8789
.416	1.1204	.6086	.7370	.8752
.364	1.1111	.6028	.7366	.8749
.312	1.1018	.5970	.7361	.8746
.260	1.0972	.5869	.7314	.8718
.208	1.0926	.5768	.7266	.8688
.156	1.1111	.5574	.7083	.8572
.104	1.1296	.5463	.6954	.8488
.052	1.1250	.5444	.6956	.8490
0.000	1.1204	.5549	.7038	.8543
-.104	1.1296	.5917	.7238	.8670
-.156	1.1250	.6106	.7367	.8750
-.208	1.1204	.6232	.7458	.8805
-.260	1.1157	.6296	.7512	.8837
-.312	1.1111	.6360	.7566	.8869
-.364	1.1204	.6376	.7544	.8856
-.416	1.1018	.6426	.7637	.8910
-.468	1.1111	.6484	.7639	.8911
-.520	1.1204	.6562	.7653	.8919
-.572	1.1296	.6662	.7679	.8934
-.624	1.1389	.6802	.7728	.8962
-.676	1.1528	.6961	.7771	.8986
-.728	1.1667	.7162	.7835	.9022
-.780	1.1574	.7352	.7970	.9096
-.832	1.1481	.7624	.8149	.9191
-.884	1.1667	.7884	.8221	.9228
-.936	1.1852	.8207	.8321	.9279
-.988	1.2083	.8485	.8380	.9309
-1.040	1.2315	.8764	.8436	.9336

(j) $x/D = 8.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 51.85 psf (2482.63 N/m^2);
q_∞ = 318.01 psf (15226.25 N/m^2);
$p_{t,\infty}$ = 1793.50 psf (85873.24 N/m^2)

z/D	$p_1/1_\infty$	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2139	.7649	.7938	.9079
.988	1.1490	.7493	.8075	.9152
.936	1.0842	.7316	.8215	.9225
.884	1.0795	.7154	.8140	.9186
.832	1.0749	.7012	.8076	.9153
.780	1.0749	.6888	.8005	.9115
.728	1.0749	.6765	.7933	.9076
.676	1.0749	.6641	.7860	.9036
.624	1.0749	.6559	.7811	.9009
.572	1.0749	.6476	.7762	.8981
.520	1.0749	.6394	.7713	.8953
.468	1.0749	.6332	.7675	.8932
.416	1.0749	.6270	.7638	.8910
.364	1.0703	.6169	.7592	.8884
.312	1.0656	.6089	.7559	.8865
.260	1.0610	.5988	.7513	.8837
.208	1.0564	.5867	.7452	.8801
.156	1.0610	.5700	.7329	.8727
.104	1.0656	.5533	.7205	.8650
.052	1.0656	.5430	.7138	.8607
0.000	1.0656	.5430	.7138	.8607
-.104	1.0564	.5681	.7333	.8730
-.156	1.0564	.5847	.7439	.8794
-.208	1.0564	.5971	.7518	.8841
-.260	1.0517	.6035	.7575	.8874
-.312	1.0517	.6076	.7601	.8889
-.364	1.0564	.6074	.7583	.8879
-.416	1.0471	.6202	.7696	.8944
-.468	1.0517	.6283	.7729	.8963
-.520	1.0564	.6384	.7774	.8988
-.572	1.0610	.6485	.7818	.9013
-.624	1.0656	.6586	.7862	.9037
-.676	1.0749	.6747	.7923	.9070
-.728	1.0842	.6929	.7995	.9109
-.780	1.0795	.7096	.8108	.9169
-.832	1.0749	.7326	.8255	.9246
-.884	1.0795	.7571	.8375	.9306
-.936	1.0842	.7838	.8502	.9369
-.988	1.1027	.8056	.8548	.9391
-1.040	1.1212	.8317	.8612	.9422

TABLE 7.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Concluded

(k) $x/D = 8.39$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 51.82 psf (2481.24 N/m^2);
q_∞ = 317.83 psf (15217.76 N/m^2);
$p_{t,\infty}$ = 1792.50 psf (85825.36 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1865	.7604	.8006	.9115
.988	1.1262	.7446	.8131	.9182
.936	1.0660	.7287	.8268	.9252
.884	1.0613	.7125	.8193	.9214
.832	1.0567	.6983	.8129	.9180
.780	1.0567	.6839	.8045	.9136
.728	1.0567	.6736	.7984	.9103
.676	1.0567	.6633	.7922	.9070
.624	1.0567	.6550	.7873	.9043
.572	1.0613	.6466	.7805	.9005
.520	1.0660	.6381	.7737	.8967
.468	1.0613	.6321	.7718	.8956
.416	1.0567	.6262	.7698	.8945
.364	1.0567	.6179	.7647	.8916
.312	1.0567	.6117	.7609	.8894
.260	1.0521	.5996	.7549	.8859
.208	1.0474	.5895	.7502	.8831
.156	1.0521	.5687	.7352	.8741
.104	1.0567	.5519	.7227	.8664
.052	1.0521	.5418	.7177	.8632
0.000	1.0474	.5400	.7180	.8634
-.104	1.0382	.5631	.7365	.8749
-.156	1.0428	.5774	.7441	.8795
-.208	1.0474	.5896	.7502	.8831
-.260	1.0335	.5943	.7583	.8879
-.312	1.0382	.5962	.7578	.8876
-.364	1.0382	.6003	.7604	.8891
-.416	1.0289	.6111	.7707	.8950
-.468	1.0289	.6214	.7771	.8987
-.520	1.0289	.6317	.7836	.9023
-.572	1.0382	.6417	.7862	.9037
-.624	1.0474	.6516	.7887	.9051
-.676	1.0567	.6656	.7937	.9078
-.728	1.0660	.6838	.8009	.9117
-.780	1.0567	.7049	.8167	.9201
-.832	1.0474	.7260	.8325	.9281
-.884	1.0567	.7483	.8415	.9326
-.936	1.0660	.7726	.8514	.9374
-.988	1.0752	.7970	.8609	.9420
-1.040	1.0845	.8214	.8703	.9464

TABLE 8.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER)

(a) x/D = 1.0; y/D = 0.0; $\alpha = 5^\circ$;

p_∞ = 22.46 psf (1075.39 N/m^2);
q_∞ = 245.30 psf (11745.19 N/m^2);
$p_{t,\infty}$ = 3189.60 psf (152718.87 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.5402	.5597	.6028	.8377
.988	1.2514	.5135	.6406	.8611
.936	.9626	.4859	.7105	.8987
.884	.8878	.4531	.7144	.9006
.832	.8129	.4336	.7303	.9082
.780	.7487	.4111	.7410	.9131
.728	.6845	.3940	.7587	.9210
.676	.6418	.3764	.7658	.9241
.624	.5990	.3641	.7797	.9299
.572	.5669	.3569	.7934	.9354
.520	.5348	.3497	.8086	.9413
.468	.4706	.3405	.8506	.9566
.416	.4065	.3341	.9066	.9747
.364	.4706	.3032	.8027	.9391
.312	.5348	.1736	.5697	.8151
.260	.5455	.0275	.2245	.4236
.208	.5562	.0075	.1158	.2303
.156	.5776	.0010	.0415	.0840
.104	.5990	.0038	.0801	.1610
.052	.5776	.0291	.2245	.4236
0.000	.5562	.0303	.2333	.4378
-.104	.6418	.0255	.1994	.3817
-.156	.6204	.0432	.2639	.4855
-.208	.5990	.1752	.5409	.7938
-.260	.5883	.3362	.7560	.9198
-.312	.5669	.3394	.7738	.9274
-.364	.5776	.3365	.7632	.9230
-.416	.5348	.3455	.8038	.9395
-.468	.5455	.3479	.7986	.9375
-.520	.5562	.3584	.8027	.9391
-.572	.5562	.3637	.8087	.9414
-.624	.5562	.3717	.8175	.9447
-.676	.6311	.3887	.7848	.9320
-.728	.7059	.4083	.7605	.9218
-.780	.7701	.4254	.7432	.9142
-.832	.8343	.4506	.7349	.9104
-.884	.9092	.4836	.7293	.9077
-.936	.9840	.5246	.7301	.9081
-.988	1.0910	.5701	.7229	.9047
-1.040	1.1980	.6317	.7262	.9063

(b) x/D = 1.5; y/D = 0.0; $\alpha = 5^\circ$;

p_∞ = 22.46 psf (1075.19 N/m^2);
q_∞ = 245.26 psf (11742.99 N/m^2);
$p_{t,\infty}$ = 3189.00 psf (152690.14 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3049	.4701	.6002	.8360
.988	1.0375	.4447	.6547	.8692
.936	.7701	.4272	.7448	.9149
.884	.7273	.4069	.7479	.9163
.832	.6845	.3919	.7566	.9201
.780	.6310	.3798	.7758	.9283
.728	.5776	.3704	.8009	.9384
.676	.5669	.3600	.7969	.9368
.624	.5562	.3549	.7989	.9376
.572	.5348	.3528	.8122	.9427
.520	.5134	.3453	.8201	.9457
.468	.4920	.3431	.8351	.9512
.416	.4706	.3517	.8644	.9613
.364	.8236	.4633	.7500	.9172
.312	1.1765	.4974	.6502	.8667
.260	1.1551	.4524	.6258	.8522
.208	1.1337	.3540	.5588	.8072
.156	1.2621	.2324	.4291	.6942
.104	1.3904	.2125	.3909	.6530
.052	1.4974	.3392	.4759	.7395
0.000	1.6043	.4759	.5446	.7967
-.104	1.8610	.6027	.5691	.8147
-.156	1.5081	.5794	.6198	.8485
-.208	1.1551	.5211	.6717	.8787
-.260	1.2407	.4331	.5909	.8297
-.312	.8877	.4339	.6991	.8930
-.364	.8556	.4373	.7149	.9009
-.416	.6203	.3600	.7618	.9223
-.468	.5883	.3554	.7773	.9289
-.520	.5562	.3535	.7972	.9369
-.572	.5455	.3564	.8084	.9413
-.624	.5348	.3621	.8228	.9467
-.676	.5776	.3691	.7994	.9378
-.728	.6203	.3787	.7814	.9306
-.780	.6524	.3914	.7745	.9277
-.832	.6845	.4093	.7733	.9272
-.884	.7166	.4327	.7770	.9288
-.936	.7487	.4613	.7850	.9320
-.988	.8129	.4919	.7779	.9291
-1.040	.8770	.5359	.7817	.9307

TABLE 8.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(c) $x/D = 2.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 22.46 psf (1075.23 N/m²);
q_∞ = 245.27 psf (11743.35 N/m²);
$p_{t,\infty}$ = 3189.10 psf (152694.93 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1548	.4364	.6147	.8453
.988	.9196	.4182	.6744	.8801
.936	.6843	.4079	.7720	.9267
.884	.6523	.3953	.7785	.9294
.832	.6202	.3854	.7883	.9334
.780	.5881	.3809	.8047	.9399
.728	.5560	.3736	.8197	.9456
.676	.5667	.3680	.8059	.9403
.624	.5774	.3678	.7981	.9373
.572	.8554	.4652	.7374	.9115
.520	1.1334	.5091	.6702	.8779
.468	1.2404	.5358	.6573	.8707
.416	1.3473	.5305	.6275	.8532
.364	1.3366	.5094	.6173	.8469
.312	1.3259	.4856	.6052	.8392
.260	1.3152	.4431	.5804	.8226
.208	1.3045	.3978	.5522	.8024
.156	1.3794	.3476	.5020	.7624
.104	1.4542	.3618	.4988	.7597
.052	1.4863	.4092	.5247	.7812
0.000	1.5184	.4754	.5595	.8078
-.104	1.6253	.5523	.5829	.8244
-.156	1.6681	.5592	.5790	.8217
-.208	1.7108	.5662	.5753	.8191
-.260	1.2083	.5787	.6921	.8895
-.312	1.2511	.5804	.6811	.8837
-.364	1.2724	.5396	.6512	.8673
-.416	.7913	.4201	.7287	.9074
-.468	.8126	.4196	.7186	.9026
-.520	.8340	.4325	.7201	.9034
-.572	.7592	.4504	.7702	.9259
-.624	.6843	.3718	.7371	.9114
-.676	.6416	.3729	.7623	.9226
-.728	.5988	.3792	.7958	.9364
-.780	.6095	.3870	.7969	.9368
-.832	.6202	.4002	.8033	.9393
-.884	.6309	.4160	.8120	.9426
-.936	.6416	.4371	.8254	.9477
-.988	.6843	.4602	.8201	.9457
-1.040	.7271	.4913	.8220	.9464

(d) $x/D = 2.5$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 22.46 psf (1075.53 N/m²);
q_∞ = 245.33 psf (11746.67 N/m²);
$p_{t,\infty}$ = 3190.00 psf (152738.02 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0901	.4267	.6256	.8521
.988	.8657	.4136	.6912	.8890
.936	.6412	.4057	.7954	.9362
.884	.6305	.3953	.7918	.9348
.832	.6199	.3875	.7907	.9343
.780	.7267	.4649	.7998	.9380
.728	.8336	.4890	.7659	.9241
.676	.9939	.5358	.7342	.9100
.624	1.1542	.5292	.6771	.8816
.572	1.1970	.5228	.6609	.8727
.520	1.2397	.5191	.6471	.8649
.468	1.2397	.5164	.6454	.8639
.416	1.2397	.5004	.6353	.8579
.364	1.2290	.4766	.6227	.8503
.312	1.2183	.4529	.6097	.8421
.260	1.1863	.4216	.5962	.8333
.208	1.1542	.3984	.5875	.8275
.156	1.1970	.3812	.5644	.8113
.104	1.2397	.3855	.5576	.8064
.052	1.2504	.4040	.5684	.8142
0.000	1.2611	.4411	.5914	.8301
-.104	1.3252	.4973	.6126	.8440
-.156	1.3466	.5048	.6123	.8438
-.208	1.3680	.5097	.6104	.8425
-.260	1.3252	.5134	.6224	.8501
-.312	1.3466	.5156	.6188	.8478
-.364	1.3145	.5244	.6316	.8557
-.416	1.3252	.5322	.6337	.8570
-.468	1.2932	.5410	.6468	.8647
-.520	1.2611	.5525	.6619	.8733
-.572	1.0153	.4140	.6386	.8599
-.624	.7695	.4200	.7388	.9121
-.676	.7909	.4356	.7421	.9136
-.728	.8122	.4538	.7474	.9160
-.780	.7160	.4748	.8143	.9435
-.832	.6199	.4103	.8136	.9432
-.884	.6199	.4183	.8215	.9462
-.936	.6199	.4370	.8397	.9528
-.988	.6412	.4552	.8426	.9538
-1.040	.6626	.4815	.8524	.9572

TABLE 8.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(e) $x/D = 3.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 22.46 psf (1075.50 N/m^2);
q_∞ = 245.33 psf (11746.30 N/m^2);
$p_{t,\infty}$ = 3189.90 psf (152733.24 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0683	.4251	.6308	.8552
.988	.9508	.4867	.7155	.9012
.936	.8333	.4896	.7665	.9244
.884	.9508	.5375	.7518	.9180
.832	1.0683	.5346	.7074	.8972
.780	1.0790	.5263	.6984	.8927
.728	1.0897	.5261	.6948	.8909
.676	1.1110	.5202	.6843	.8854
.624	1.1324	.5117	.6722	.8789
.572	1.1324	.5010	.6651	.8751
.520	1.1324	.4903	.6580	.8711
.468	1.1110	.4775	.6555	.8697
.416	1.0897	.4566	.6473	.8650
.364	1.0790	.4408	.6392	.8602
.312	1.0683	.4224	.6288	.8540
.260	1.0469	.4016	.6193	.8482
.208	1.0256	.3914	.6178	.8472
.156	1.0469	.3802	.6026	.8375
.104	1.0683	.3796	.5961	.8333
.052	1.0790	.3901	.6012	.8366
0.000	1.0897	.4138	.6163	.8463
-.104	1.1110	.4604	.6437	.8629
-.156	1.1324	.4706	.6446	.8634
-.208	1.1538	.4754	.6419	.8618
-.260	1.1217	.4762	.6516	.8674
-.312	1.1431	.4784	.6469	.8648
-.364	1.1538	.4835	.6473	.8650
-.416	1.1324	.4893	.6574	.8707
-.468	1.1431	.4944	.6577	.8709
-.520	1.1538	.5049	.6615	.8731
-.572	1.1751	.5151	.6621	.8734
-.624	1.1965	.5280	.6643	.8746
-.676	1.1431	.5454	.6907	.8888
-.728	1.0897	.5681	.7220	.9043
-.780	.9294	.4434	.6907	.8888
-.832	.7692	.4607	.7739	.9275
-.884	.7906	.4843	.7827	.9311
-.936	.8119	.5132	.7951	.9361
-.988	.7265	.5447	.8659	.9618
-1.040	.6410	.4852	.8700	.9632

(f) $x/D = 4.0$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 22.45 psf (1074.69 N/m^2);
q_∞ = 245.14 psf (11737.46 N/m^2);
$p_{t,\infty}$ = 3187.50 psf (152618.32 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.4549	.5803	.6315	.8557
.988	1.2410	.5562	.6695	.8775
.936	1.0270	.5402	.7252	.9058
.884	1.0163	.5218	.7165	.9017
.832	1.0056	.5087	.7112	.8991
.780	.9949	.4983	.7077	.8973
.728	.9842	.4852	.7021	.8946
.676	.9735	.4695	.6944	.8907
.624	.9628	.4617	.6925	.8897
.572	.9521	.4487	.6865	.8865
.520	.9414	.4383	.6823	.8844
.468	.9200	.4228	.6779	.8820
.416	.8986	.4100	.6754	.8807
.364	.8986	.3993	.6666	.8759
.312	.8986	.3886	.6576	.8709
.260	.8879	.3809	.6550	.8694
.208	.8772	.3758	.6545	.8691
.156	.8879	.3702	.6457	.8641
.104	.8986	.3700	.6416	.8617
.052	.9093	.3750	.6422	.8620
0.000	.9200	.3881	.6495	.8663
-.104	.9200	.4162	.6726	.8792
-.156	.9414	.4264	.6730	.8794
-.208	.9628	.4312	.6693	.8773
-.260	.9414	.4345	.6793	.8828
-.312	.9628	.4366	.6734	.8796
-.364	.9521	.4395	.6794	.8828
-.416	.9628	.4446	.6796	.8829
-.468	.9521	.4502	.6877	.8872
-.520	.9414	.4559	.6959	.8914
-.572	.9628	.4634	.6937	.8903
-.624	.9842	.4709	.6917	.8893
-.676	.9949	.4840	.6975	.8922
-.728	1.0056	.4998	.7050	.8960
-.780	1.0056	.5185	.7181	.9024
-.832	1.0056	.5399	.7327	.9093
-.884	1.0377	.5659	.7384	.9120
-.936	1.0698	.6025	.7505	.9174
-.988	1.0912	.6341	.7623	.9226
-1.040	1.1126	.6737	.7781	.9292

TABLE 8.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(g) x/D = 5.0; y/D = 0.0; α = 5°;

p_∞ = 22.45 psf (1075.13 N/m^2);
q_∞ = 245.24 psf (11742.25 N/m^2);
$p_{t,\infty}$ = 3188.80 psf (152680.57 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3281	.5331	.6336	.8569
.988	1.1246	.5142	.6761	.8811
.936	.9211	.5058	.7410	.9131
.884	.9104	.4900	.7337	.9098
.832	.8997	.4796	.7301	.9081
.780	.8890	.4692	.7265	.9064
.728	.8783	.4588	.7228	.9047
.676	.8676	.4457	.7168	.9018
.624	.8569	.4353	.7128	.8998
.572	.8569	.4246	.7040	.8955
.520	.8569	.4140	.6951	.8910
.468	.8354	.4012	.6929	.8899
.416	.8140	.3910	.6931	.8900
.364	.8140	.3830	.6859	.8863
.312	.8140	.3777	.6811	.8837
.260	.8140	.3697	.6739	.8799
.208	.8140	.3670	.6714	.8785
.156	.8140	.3616	.6665	.8759
.104	.8140	.3616	.6665	.8759
.052	.8140	.3670	.6714	.8785
0.000	.8140	.3750	.6787	.8825
-.104	.8140	.3951	.6967	.8918
-.156	.8354	.4026	.6942	.8905
-.208	.8569	.4101	.6918	.8893
-.260	.8354	.4160	.7056	.8963
-.312	.8569	.4181	.6985	.8928
-.364	.8569	.4181	.6985	.8928
-.416	.8569	.4261	.7052	.8961
-.468	.8569	.4261	.7052	.8961
-.520	.8569	.4342	.7118	.8994
-.572	.8569	.4395	.7162	.9015
-.624	.8569	.4476	.7227	.9046
-.676	.8676	.4553	.7245	.9055
-.728	.8783	.4658	.7282	.9072
-.780	.8783	.4792	.7386	.9121
-.832	.8783	.4952	.7509	.9176
-.884	.8997	.5161	.7574	.9204
-.936	.9211	.5450	.7692	.9255
-.988	.9425	.5713	.7785	.9294
-1.040	.9640	.6055	.7926	.9351

(h) x/D = 6.0; y/D = 0.0; α = 5°;

p_∞ = 22.46 psf (1075.50 N/m^2);
q_∞ = 245.33 psf (11746.30 N/m^2);
$p_{t,\infty}$ = 3189.90 psf (152733.24 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2828	.5139	.6330	.8565
.988	1.0797	.5002	.6807	.8835
.936	.8766	.4892	.7470	.9158
.884	.8659	.4761	.7415	.9134
.832	.8552	.4683	.7400	.9127
.780	.8445	.4579	.7363	.9110
.728	.8338	.4448	.7303	.9082
.676	.8338	.4341	.7215	.9041
.624	.8338	.4234	.7126	.8997
.572	.8338	.4127	.7035	.8953
.520	.8338	.4020	.6943	.8906
.468	.8231	.3916	.6897	.8882
.416	.8124	.3838	.6873	.8870
.364	.8124	.3785	.6825	.8845
.312	.8124	.3731	.6777	.8819
.260	.8018	.3707	.6800	.8831
.208	.7911	.3656	.6798	.8830
.156	.8018	.3627	.6726	.8791
.104	.8124	.3624	.6679	.8766
.052	.8124	.3651	.6703	.8779
0.000	.8124	.3731	.6777	.8819
-.104	.8124	.3923	.6949	.8909
-.156	.8231	.4000	.6971	.8921
-.208	.8338	.4051	.6971	.8920
-.260	.8231	.4108	.7064	.8967
-.312	.8338	.4132	.7039	.8955
-.364	.8231	.4134	.7087	.8978
-.416	.8338	.4185	.7085	.8977
-.468	.8231	.4215	.7156	.9012
-.520	.8124	.4271	.7250	.9057
-.572	.8124	.4297	.7273	.9068
-.624	.8124	.4378	.7341	.9100
-.676	.8231	.4455	.7357	.9107
-.728	.8338	.4560	.7395	.9125
-.780	.8338	.4667	.7481	.9163
-.832	.8338	.4827	.7609	.9219
-.884	.8552	.4983	.7633	.9230
-.936	.8766	.5245	.7735	.9273
-.988	.8766	.5486	.7911	.9345
-1.040	.8766	.5780	.8120	.9427

TABLE 8.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Continued

(i) x/D = 7.0; y/D = 0.0; α = 5°;

p_∞ = 22.46 psf (1075.46 N/m^2);
q_∞ = 245.32 psf (11745.93 N/m^2);
$p_{t,\infty}$ = 3189.80 psf (152728.45 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2834	.5181	.6353	.8580
.988	1.0802	.5017	.6815	.8839
.936	.8770	.4934	.7500	.9172
.884	.8663	.4803	.7446	.9148
.832	.8556	.4725	.7432	.9141
.780	.8449	.4595	.7374	.9115
.728	.8342	.4491	.7337	.9098
.676	.8342	.4357	.7227	.9046
.624	.8342	.4277	.7160	.9014
.572	.8342	.4144	.7048	.8959
.520	.8342	.4037	.6957	.8913
.468	.8235	.3960	.6934	.8901
.416	.8128	.3882	.6911	.8890
.364	.8128	.3829	.6863	.8865
.312	.8128	.3802	.6839	.8852
.260	.8128	.3776	.6815	.8840
.208	.8128	.3749	.6791	.8827
.156	.8128	.3696	.6743	.8801
.104	.8128	.3696	.6743	.8801
.052	.8128	.3722	.6767	.8814
0.000	.8128	.3802	.6839	.8852
-.104	.8128	.3896	.6923	.8896
-.156	.8235	.3974	.6946	.8908
-.208	.8342	.4025	.6946	.8907
-.260	.8128	.4083	.7088	.8979
-.312	.8235	.4108	.7062	.8966
-.364	.8235	.4134	.7085	.8978
-.416	.8128	.4164	.7157	.9013
-.468	.8128	.4190	.7180	.9024
-.520	.8128	.4217	.7203	.9035
-.572	.8128	.4271	.7248	.9056
-.624	.8128	.4351	.7316	.9088
-.676	.8128	.4405	.7361	.9109
-.728	.8128	.4512	.7450	.9149
-.780	.8128	.4619	.7538	.9189
-.832	.8128	.4752	.7646	.9236
-.884	.8235	.4937	.7743	.9276
-.936	.8342	.5148	.7856	.9323
-.988	.8449	.5387	.7984	.9374
-1.040	.8556	.5652	.8127	.9429

(j) x/D = 8.0; y/D = 0.0; α = 5°;

p_∞ = 22.48 psf (1076.47 N/m^2);
q_∞ = 245.55 psf (11756.98 N/m^2);
$p_{t,\infty}$ = 3192.80 psf (152872.09 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2401	.5139	.6437	.8629
.988	1.0476	.4973	.6890	.8878
.936	.8552	.4860	.7538	.9189
.884	.8338	.4732	.7533	.9186
.832	.8125	.4630	.7549	.9193
.780	.8125	.4523	.7462	.9155
.728	.8125	.4443	.7395	.9125
.676	.8338	.4332	.7207	.9037
.624	.8552	.4326	.7112	.8991
.572	.9194	.4364	.6890	.8878
.520	.9835	.4295	.6608	.8727
.468	1.0049	.4370	.6594	.8719
.416	1.0263	.4364	.6521	.8678
.364	1.0370	.4362	.6486	.8657
.312	1.0476	.4332	.6431	.8625
.260	1.0370	.4308	.6446	.8634
.208	1.0263	.4284	.6461	.8643
.156	1.0476	.4225	.6351	.8578
.104	1.0690	.4193	.6263	.8525
.052	1.0583	.4223	.6317	.8557
0.000	1.0476	.4306	.6411	.8614
-.104	1.0476	.4476	.6537	.8686
-.156	1.0583	.4554	.6560	.8700
-.208	1.0690	.4605	.6563	.8701
-.260	1.0263	.4696	.6764	.8812
-.312	1.0370	.4693	.6727	.8792
-.364	.9835	.4706	.6917	.8893
-.416	1.0049	.4674	.6820	.8842
-.468	.9514	.4634	.6979	.8924
-.520	.8980	.4567	.7131	.9000
-.572	.8659	.4468	.7183	.9025
-.624	.8338	.4502	.7348	.9103
-.676	.8125	.4454	.7404	.9129
-.728	.7911	.4486	.7530	.9185
-.780	.7911	.4593	.7619	.9224
-.832	.7911	.4726	.7729	.9271
-.884	.8018	.4911	.7826	.9311
-.936	.8125	.5122	.7940	.9357
-.988	.8125	.5362	.8124	.9428
-1.040	.8125	.5630	.8324	.9502

TABLE 8.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞, AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 140°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 x 10^6 PER FOOT (5.42 x 10^6 PER METER) – Concluded

(k) $x/D = 8.39$; $y/D = 0.0$; $\alpha = 5^\circ$;

p_∞ = 22.46 psf (1075.29 N/m^2);
q_∞ = 245.28 psf (11744.09 N/m^2);
$p_{t,\infty}$ = 3189.30 psf (152704.51 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2842	.5214	.6372	.8591
.988	1.1237	.5254	.6838	.8851
.936	.9632	.5373	.7469	.9158
.884	1.0060	.5389	.7319	.9090
.832	1.0488	.5379	.7161	.9015
.780	1.0702	.5320	.7051	.8960
.728	1.0916	.5208	.6907	.8888
.676	1.1023	.5045	.6765	.8813
.624	1.1130	.4909	.6641	.8745
.572	1.1130	.4802	.6569	.8705
.520	1.1130	.4669	.6477	.8652
.468	1.1023	.4591	.6454	.8639
.416	1.0916	.4514	.6430	.8625
.364	1.0809	.4463	.6425	.8622
.312	1.0702	.4412	.6421	.8619
.260	1.0595	.4388	.6435	.8628
.208	1.0488	.4337	.6431	.8625
.156	1.0702	.4252	.6303	.8549
.104	1.0916	.4219	.6217	.8497
.052	1.0916	.4219	.6217	.8497
0.000	1.0916	.4273	.6256	.8521
-.104	1.0916	.4422	.6365	.8586
-.156	1.0916	.4530	.6442	.8632
-.208	1.0916	.4610	.6499	.8665
-.260	1.0702	.4696	.6624	.8736
-.312	1.0702	.4723	.6643	.8746
-.364	1.0702	.4749	.6662	.8757
-.416	1.0488	.4781	.6752	.8806
-.468	1.0488	.4835	.6790	.8826
-.520	1.0488	.4862	.6809	.8836
-.572	1.0595	.4940	.6828	.8846
-.624	1.0702	.4991	.6829	.8847
-.676	1.0702	.5071	.6884	.8875
-.728	1.0702	.5178	.6956	.8913
-.780	1.0167	.5299	.7219	.9043
-.832	.9632	.5365	.7463	.9155
-.884	.9097	.5271	.7612	.9221
-.936	.8562	.5230	.7816	.9307
-.988	.8348	.5343	.8000	.9380
-1.040	.8134	.5589	.8289	.9489

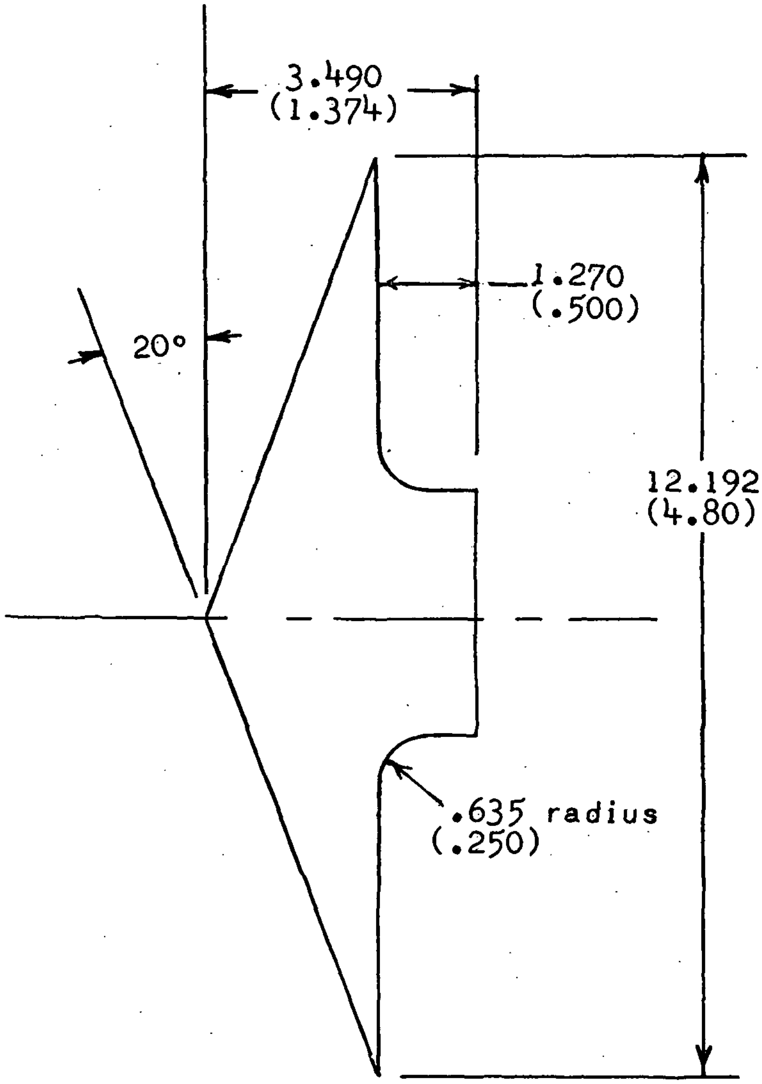


Figure 1.- Sketch of 140°-included-angle cone used in wake survey. Dimensions in cm (in.).

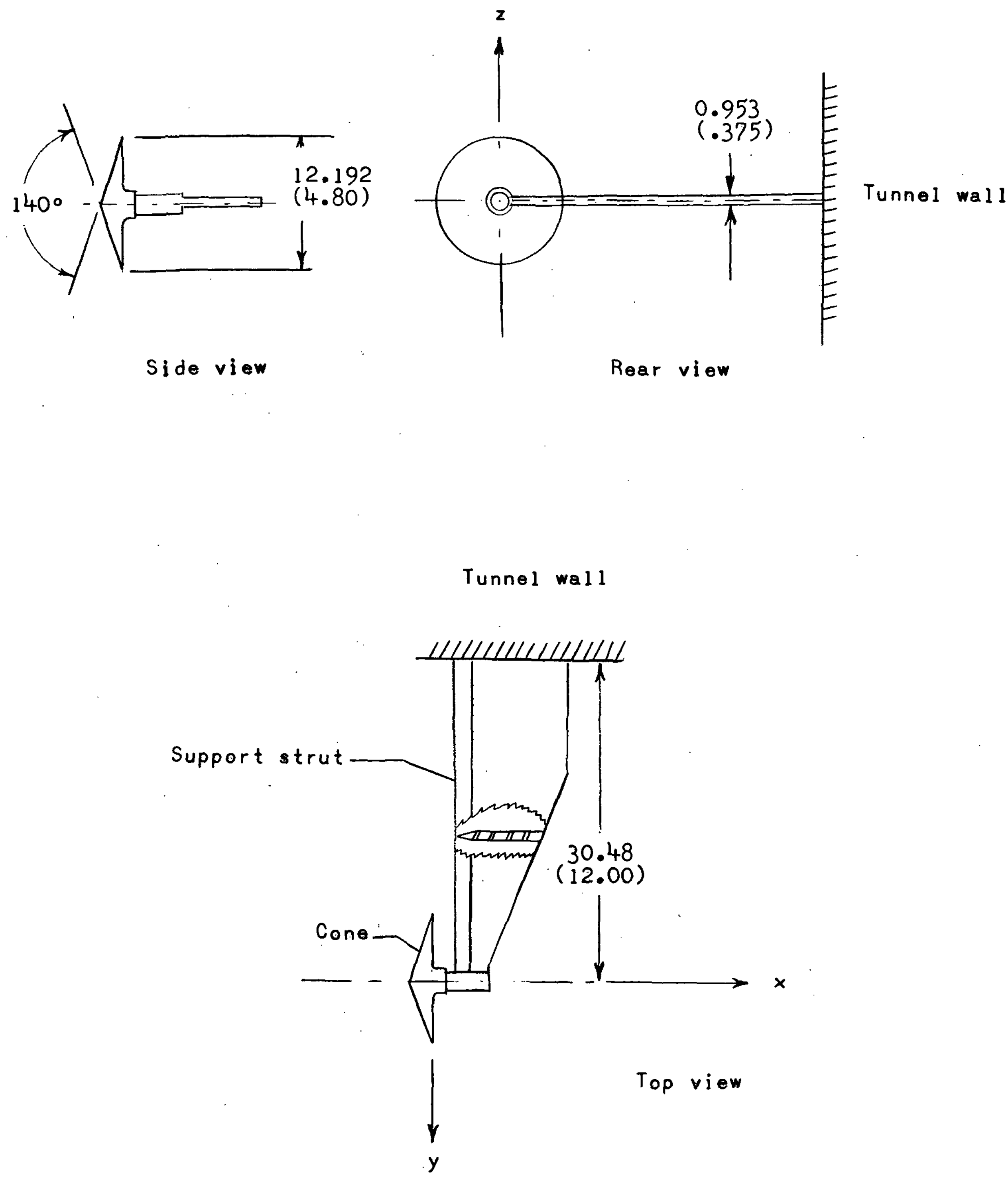


Figure 2.- Sketch of model and model support system. Dimensions in cm (in.).

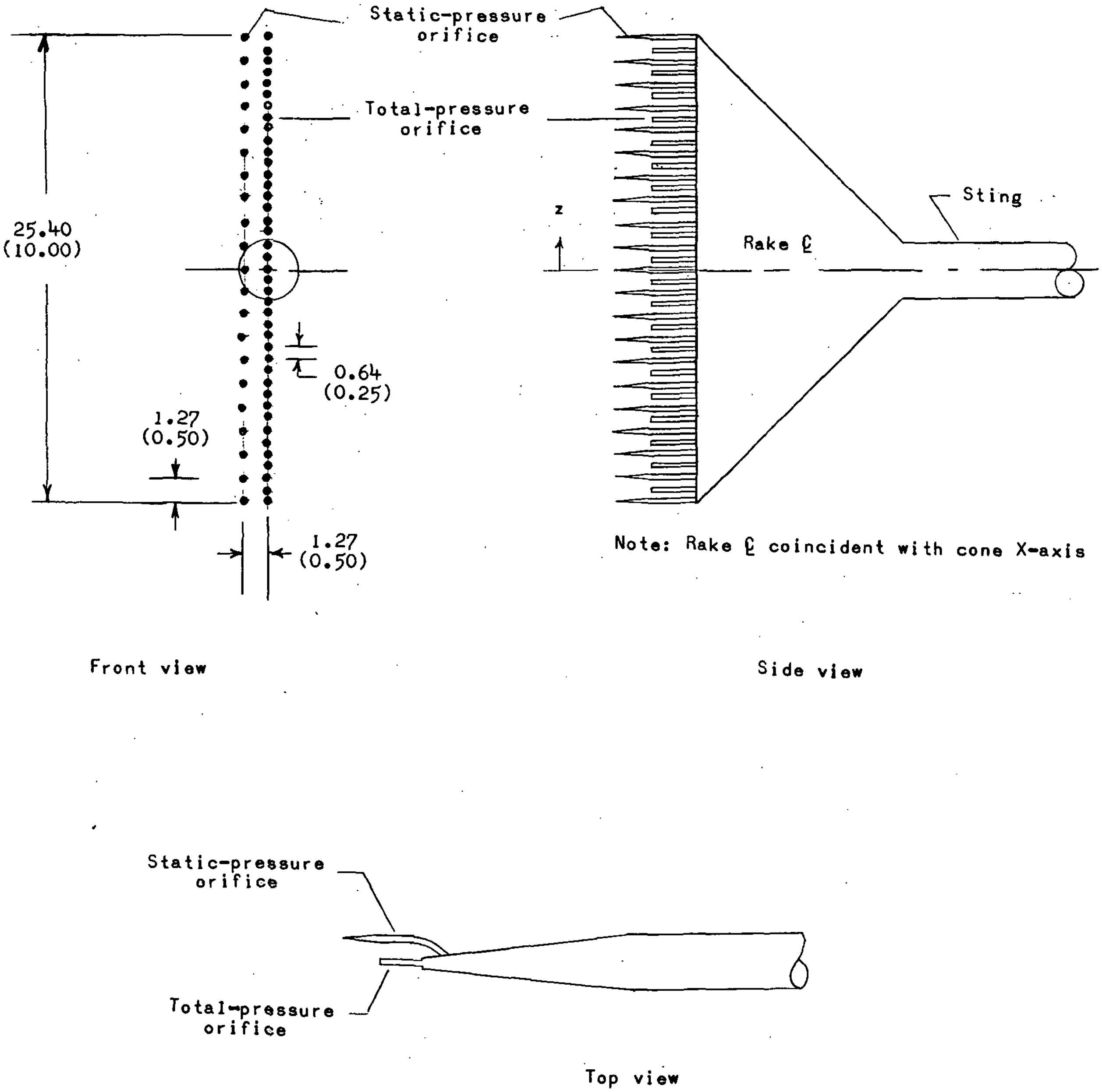


Figure 3.- Sketch of pressure rake used in wake survey. Dimensions in cm (in.).

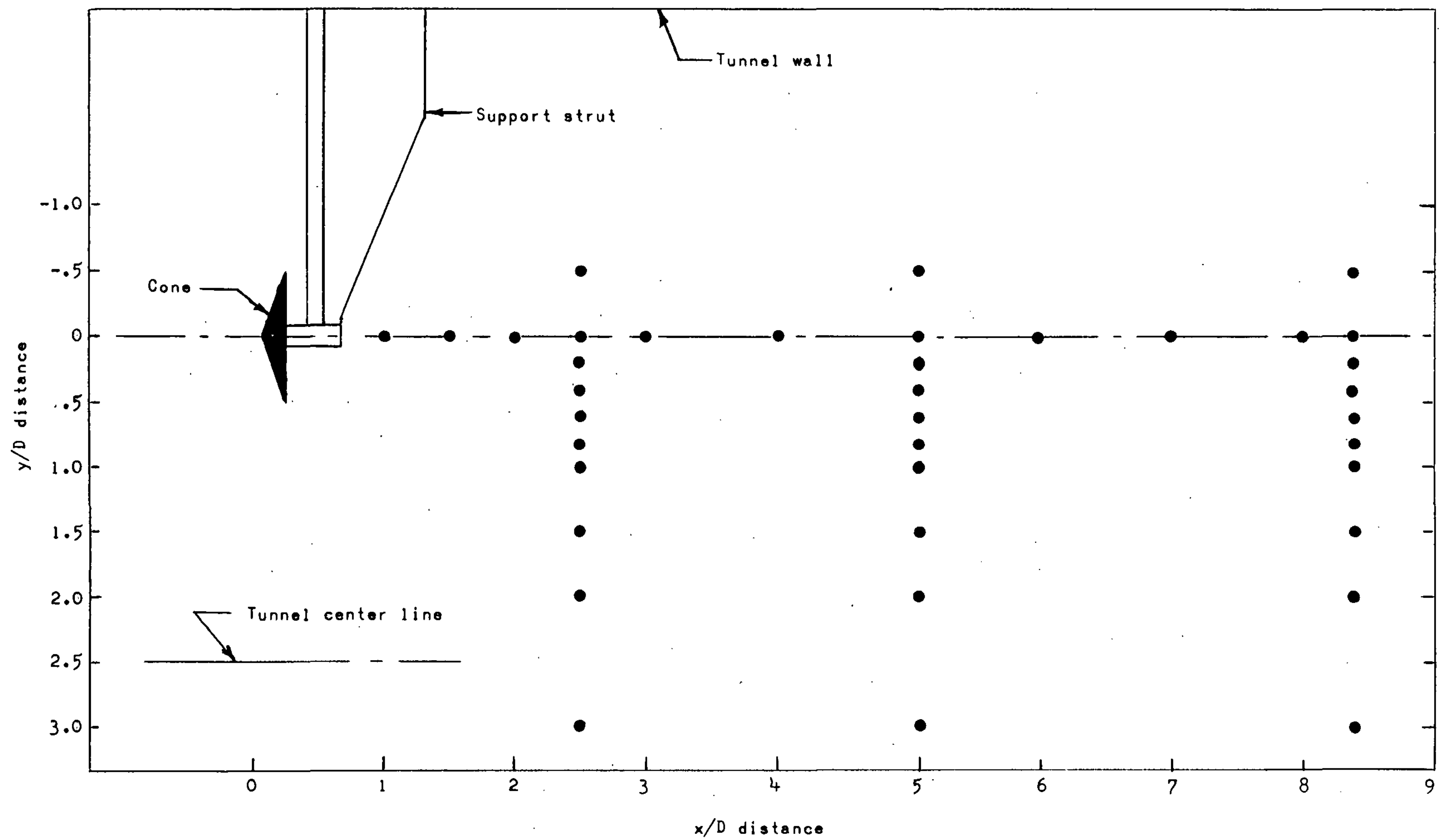
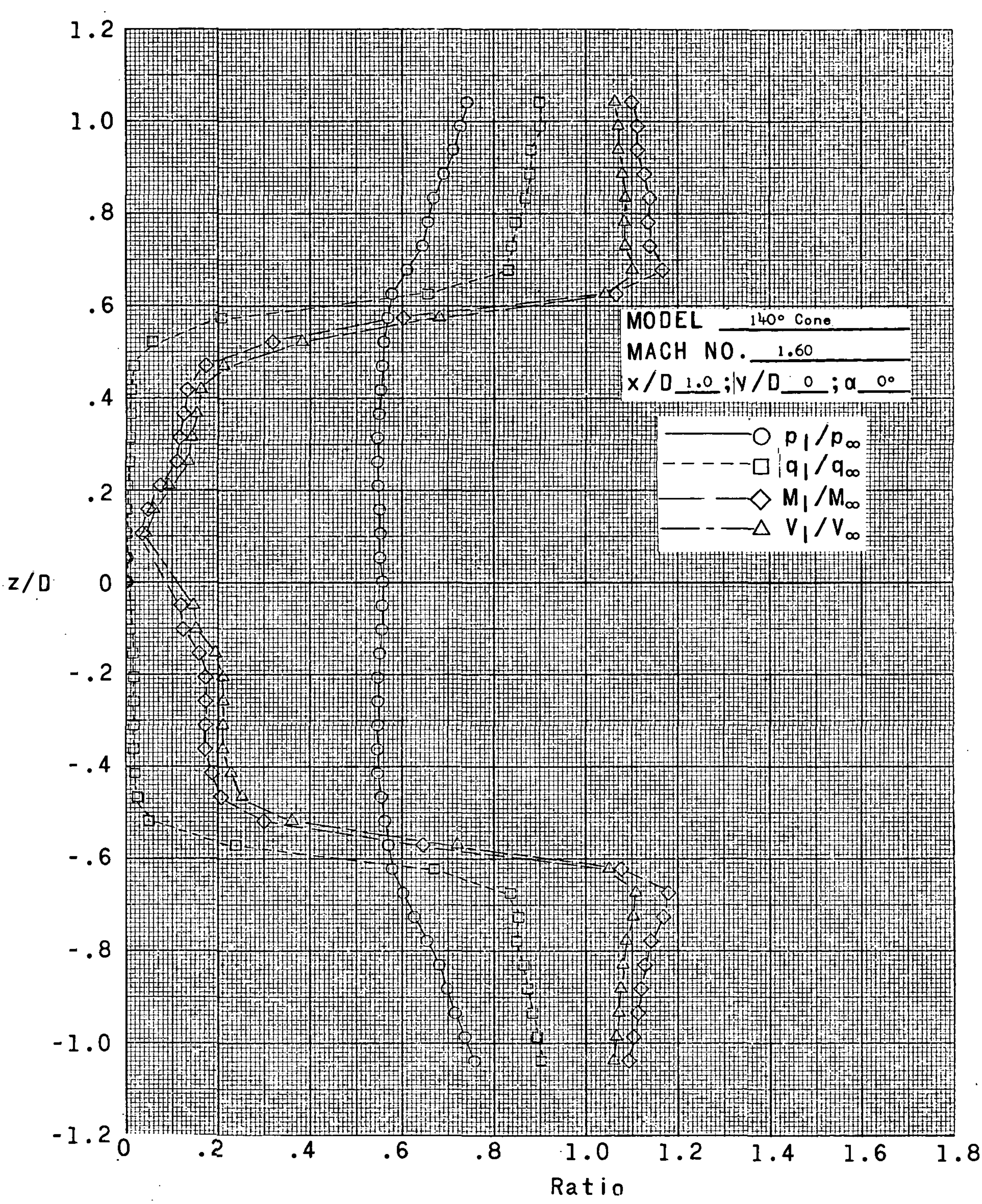
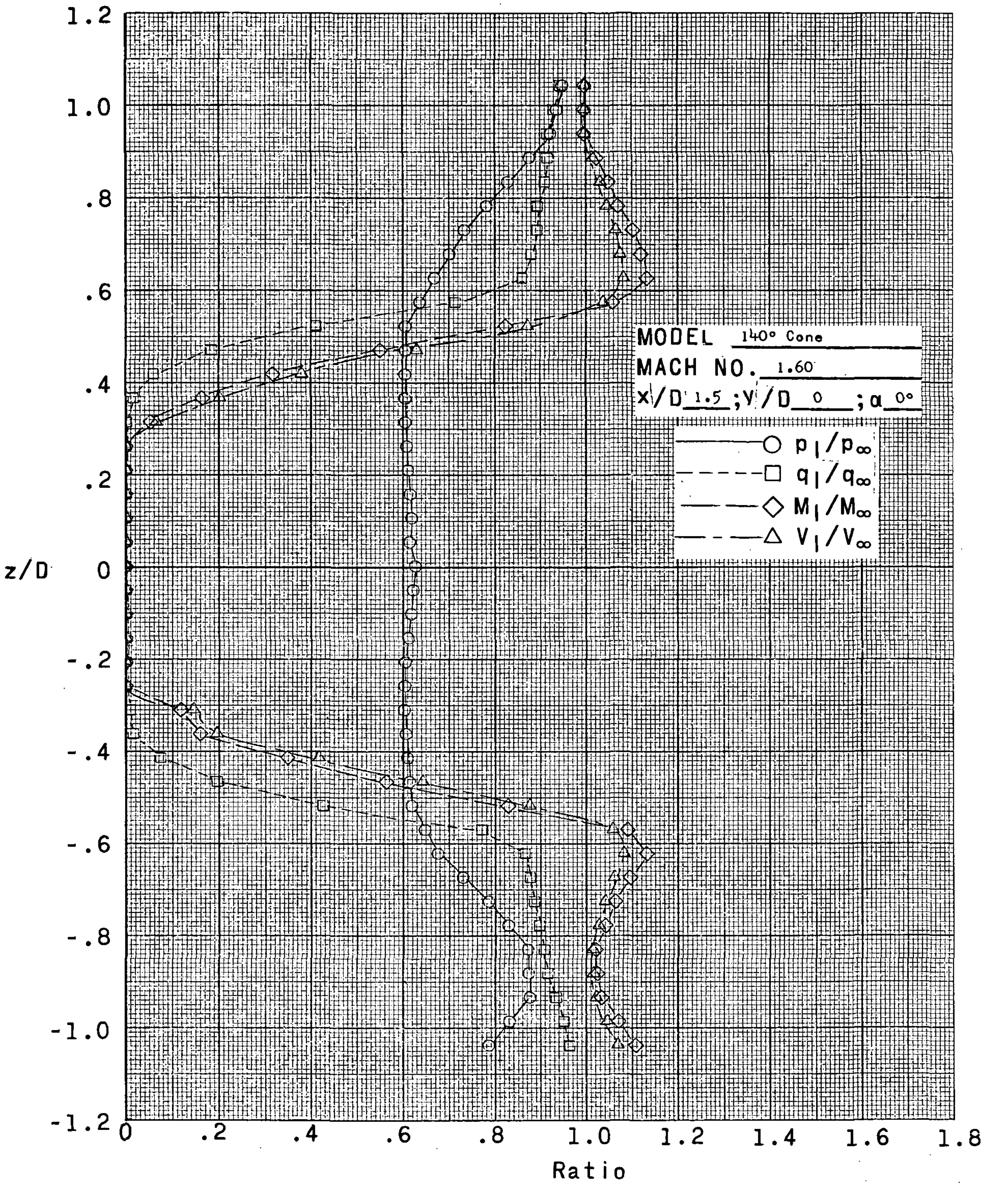


Figure 4.- Schematic representation of lateral and longitudinal stations used in wake survey.



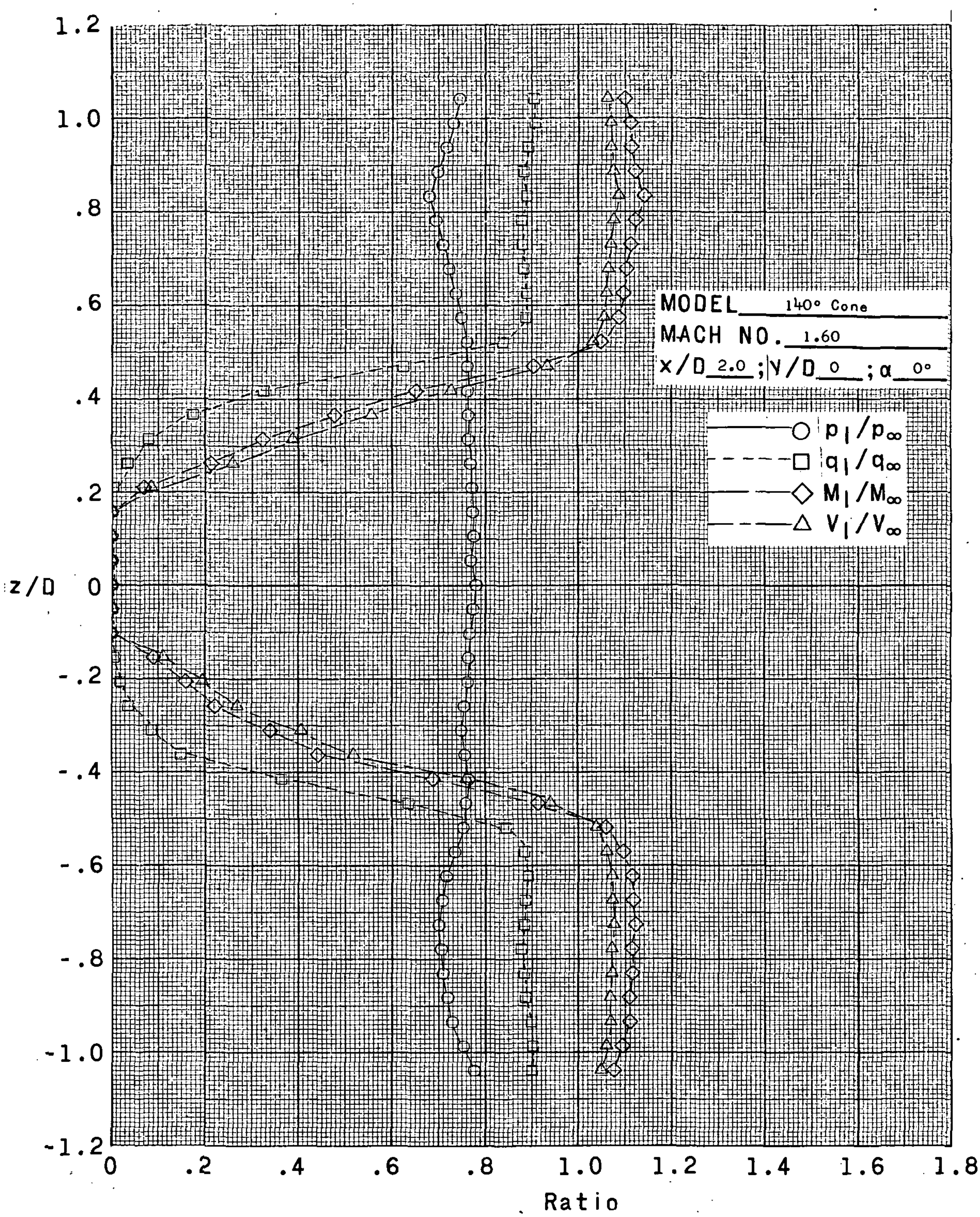
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 5.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D in wake of 140^0-included-angle cone at Mach number of 1.60 and Reynolds number of 5.42×10^6 per meter (1.65×10^6 per foot).



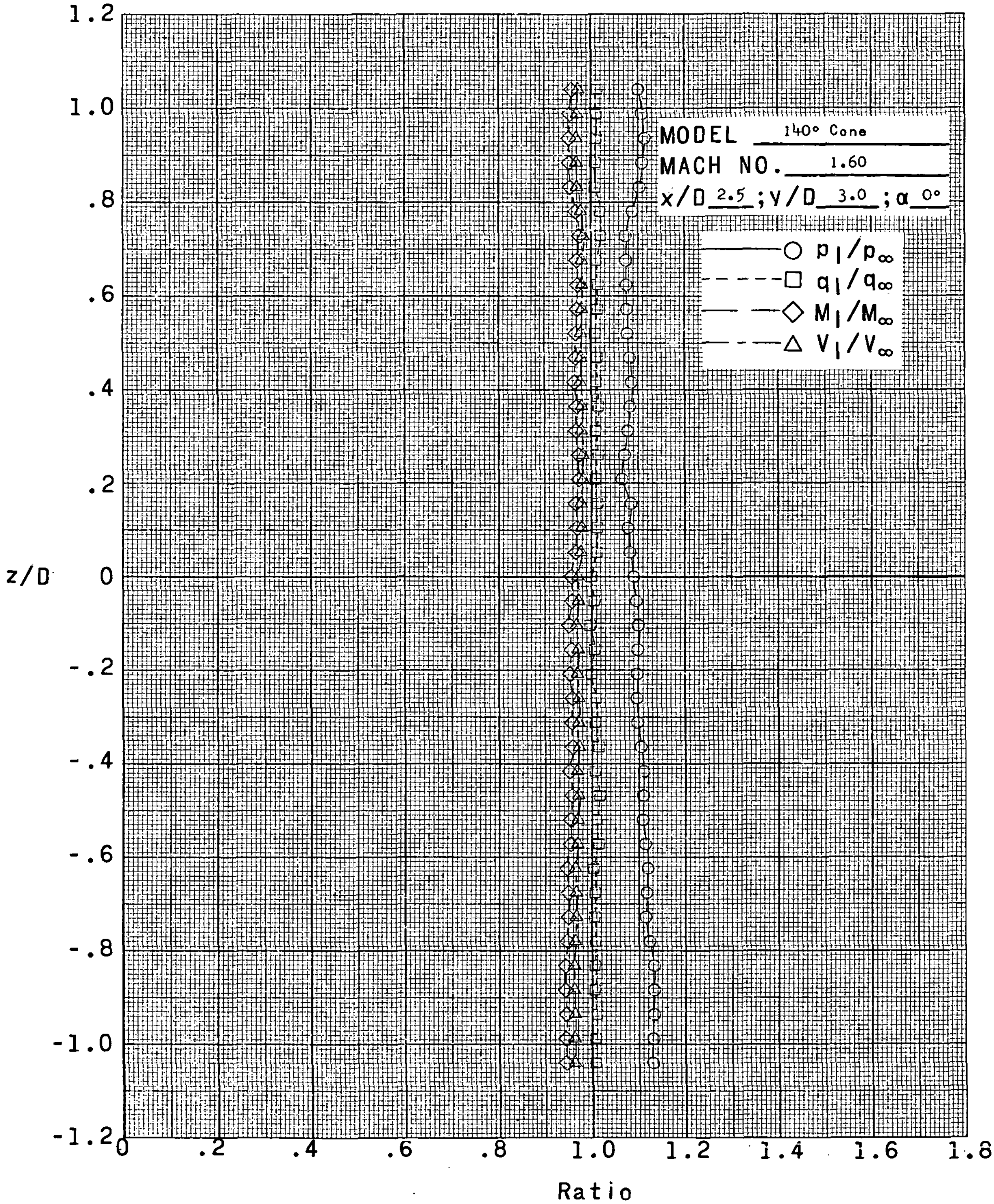
(b) x/D = 1.5; y/D = 0; α = 0°.

Figure 5.- Continued.



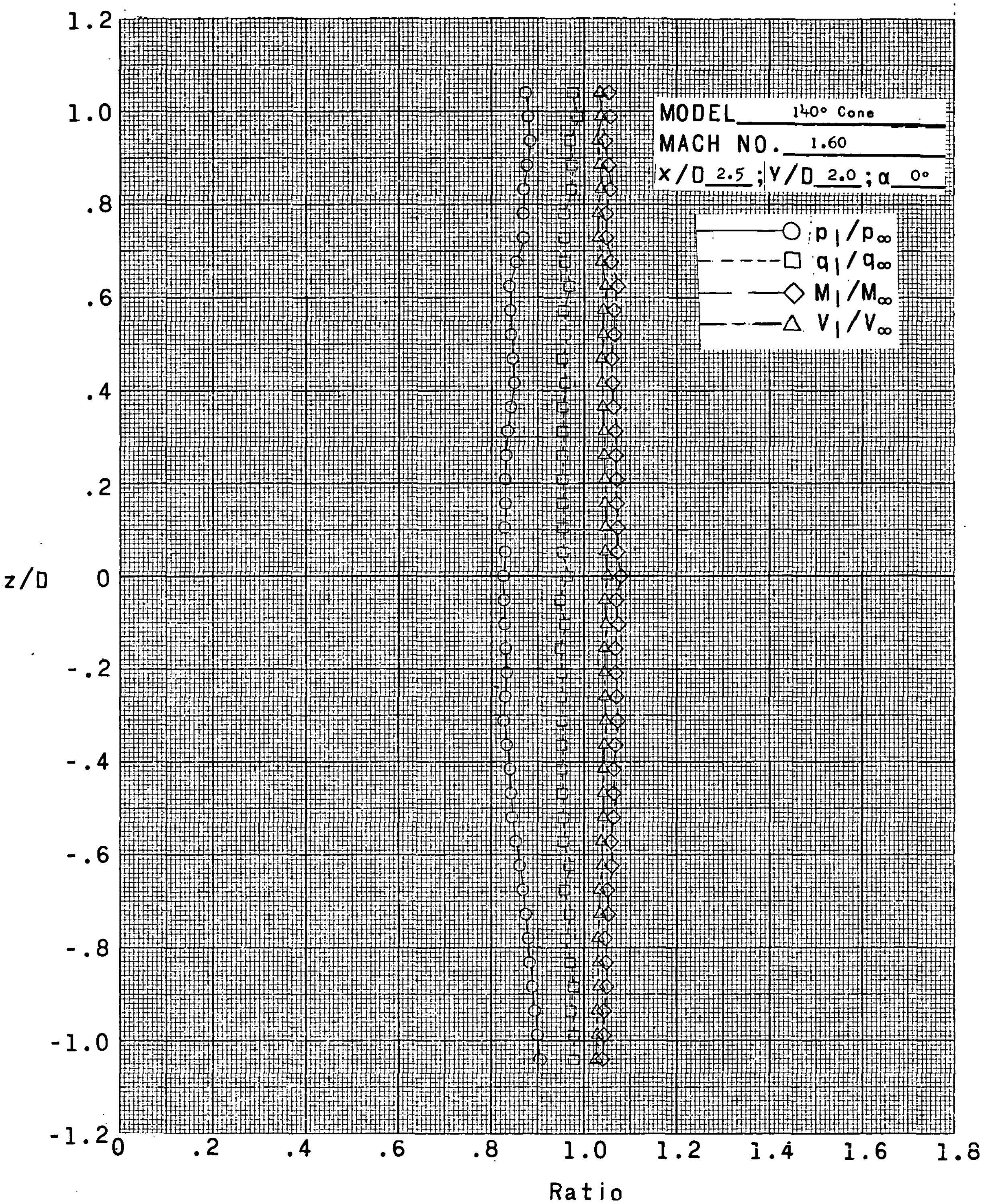
(c) x/D = 2.0; y/D = 0; α = 0°.

Figure 5.- Continued.



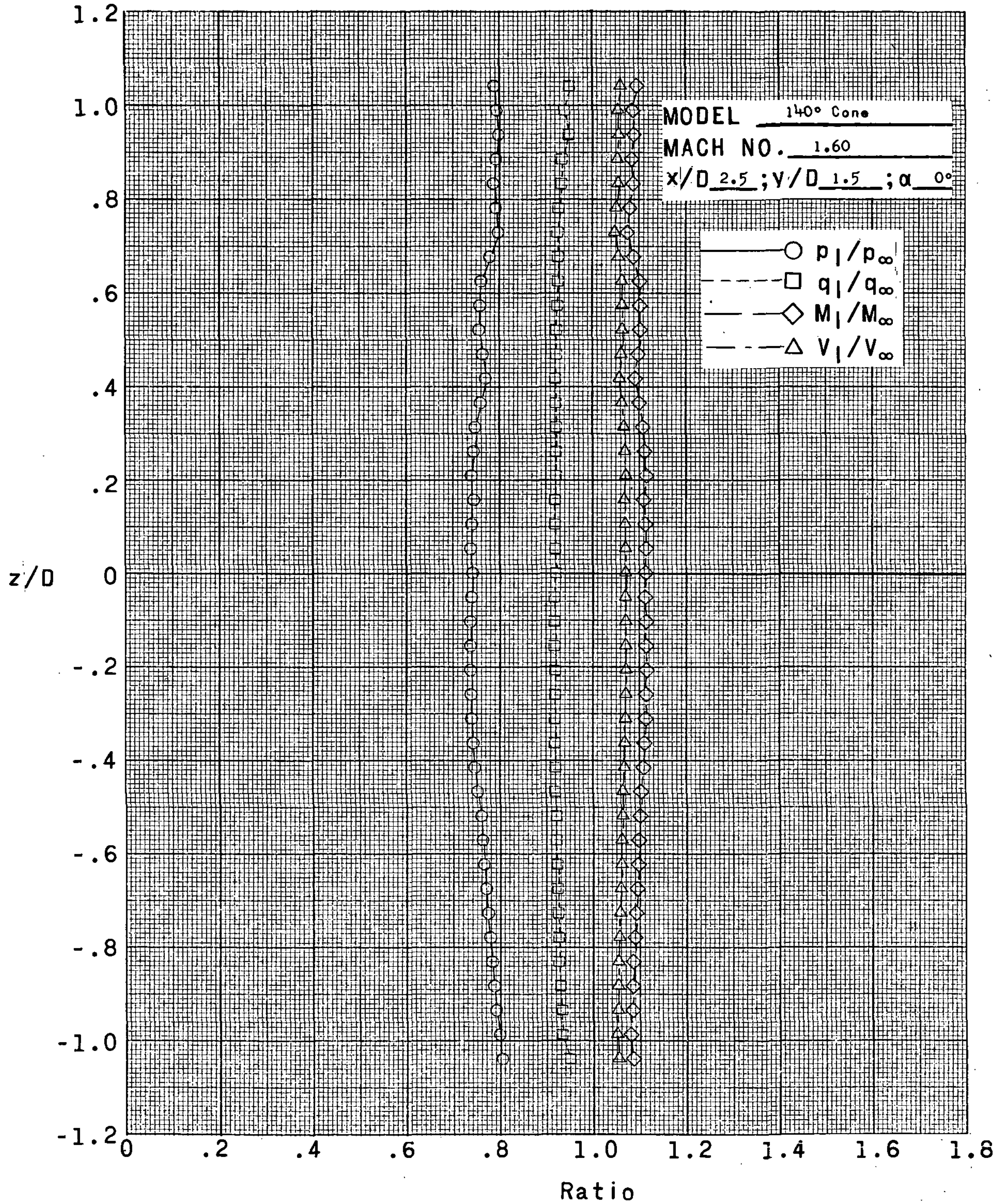
(d) $x/D = 2.5$; $y/D = 3.0$; $\alpha = 0^0$.

Figure 5.- Continued.



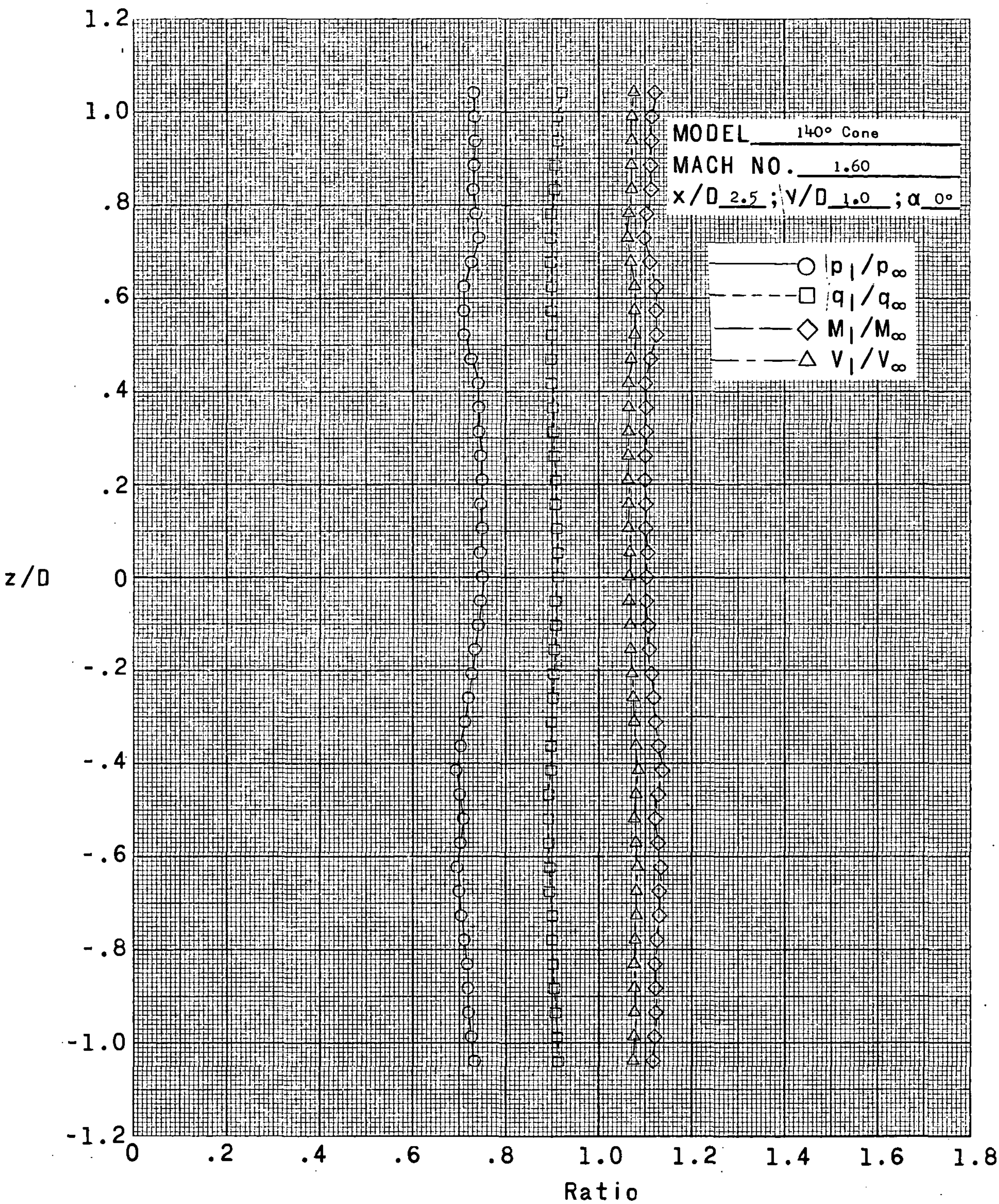
(e) $x/D = 2.5$; $y/D = 2.0$; $\alpha = 0^{0}$.

Figure 5.- Continued.



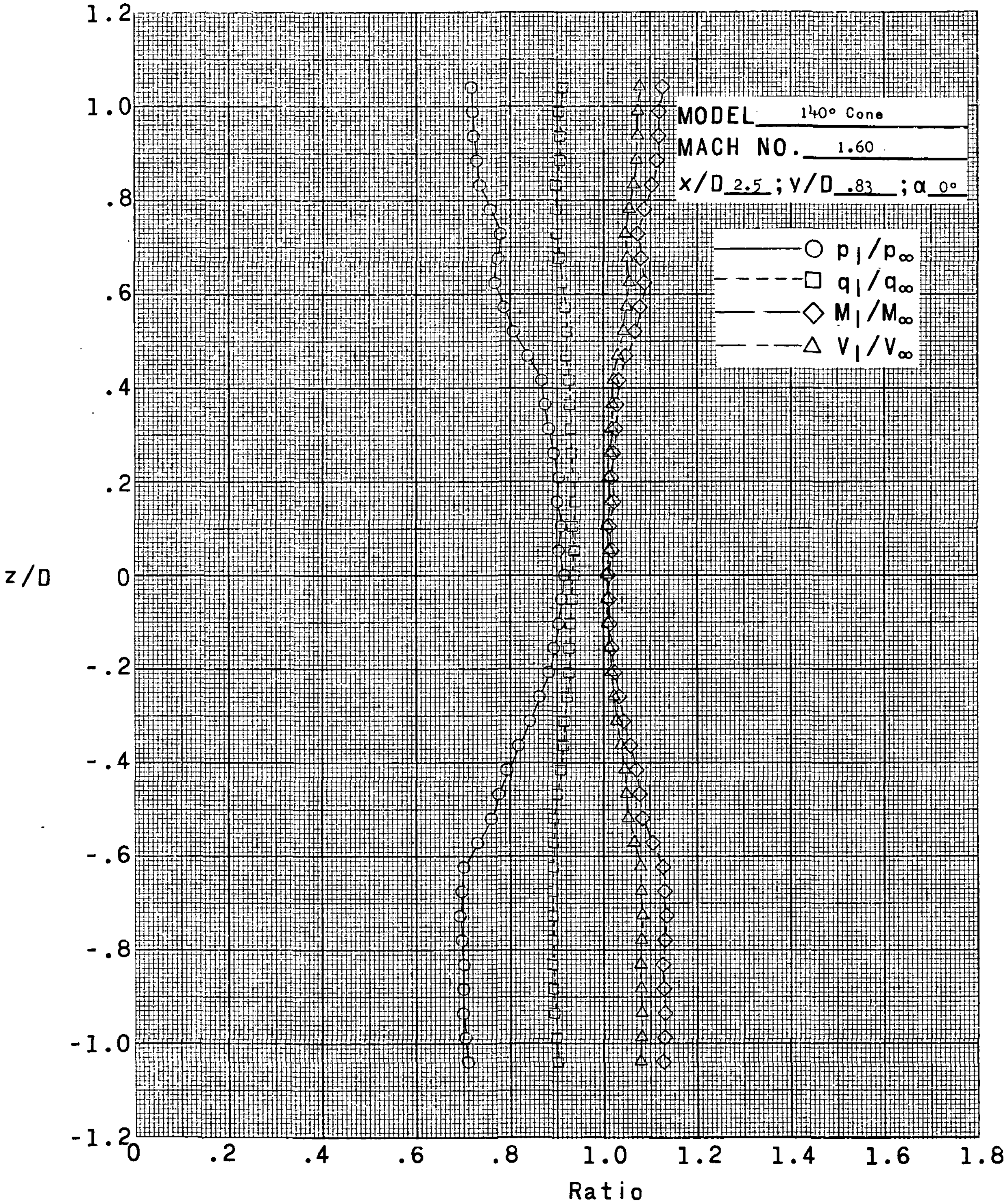
(f) $x/D = 2.5$; $y/D = 1.5$; $\alpha = 0^0$.

Figure 5.- Continued.



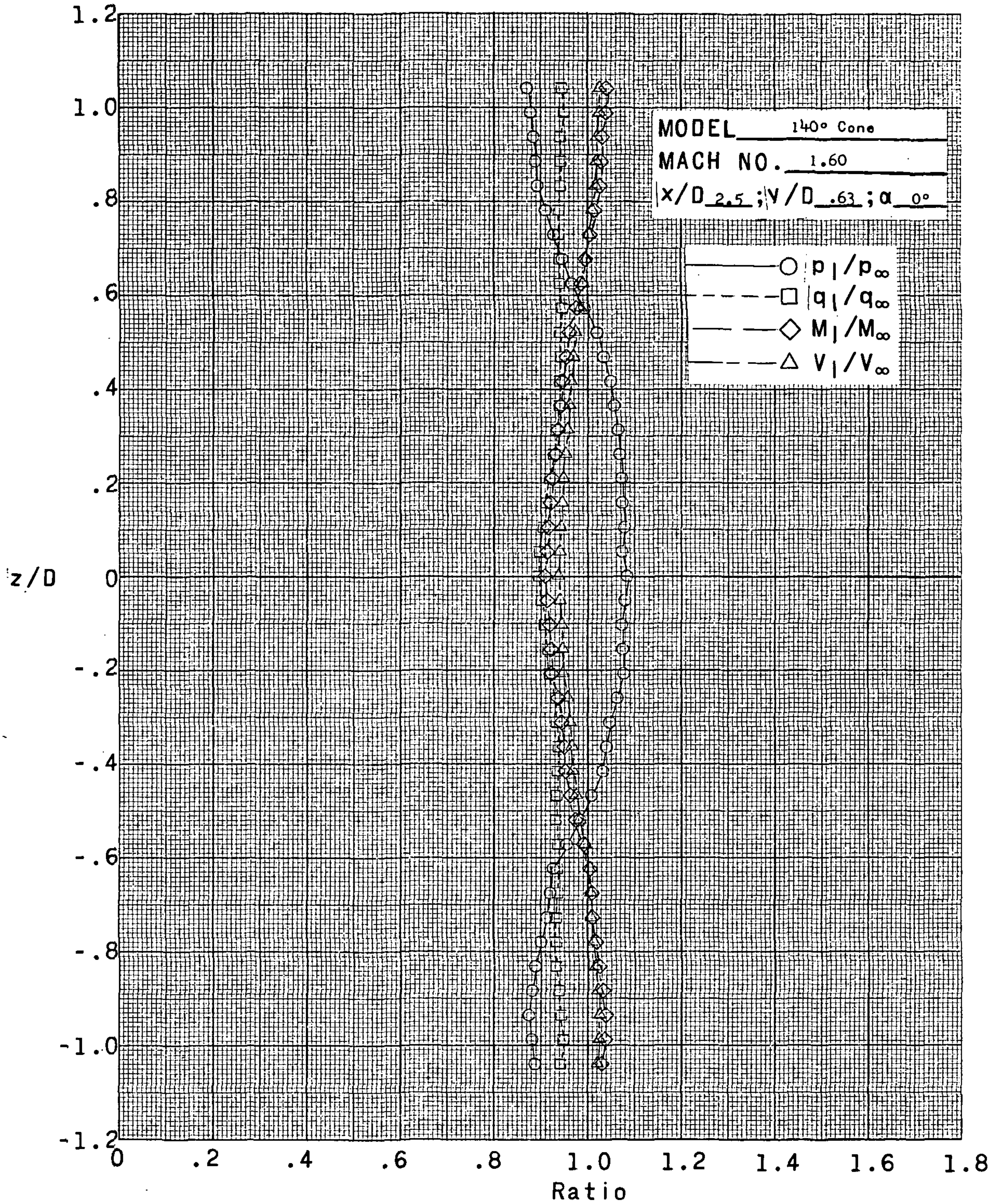
(g) x/D = 2.5; y/D = 1.0; α = 0°.

Figure 5.- Continued.



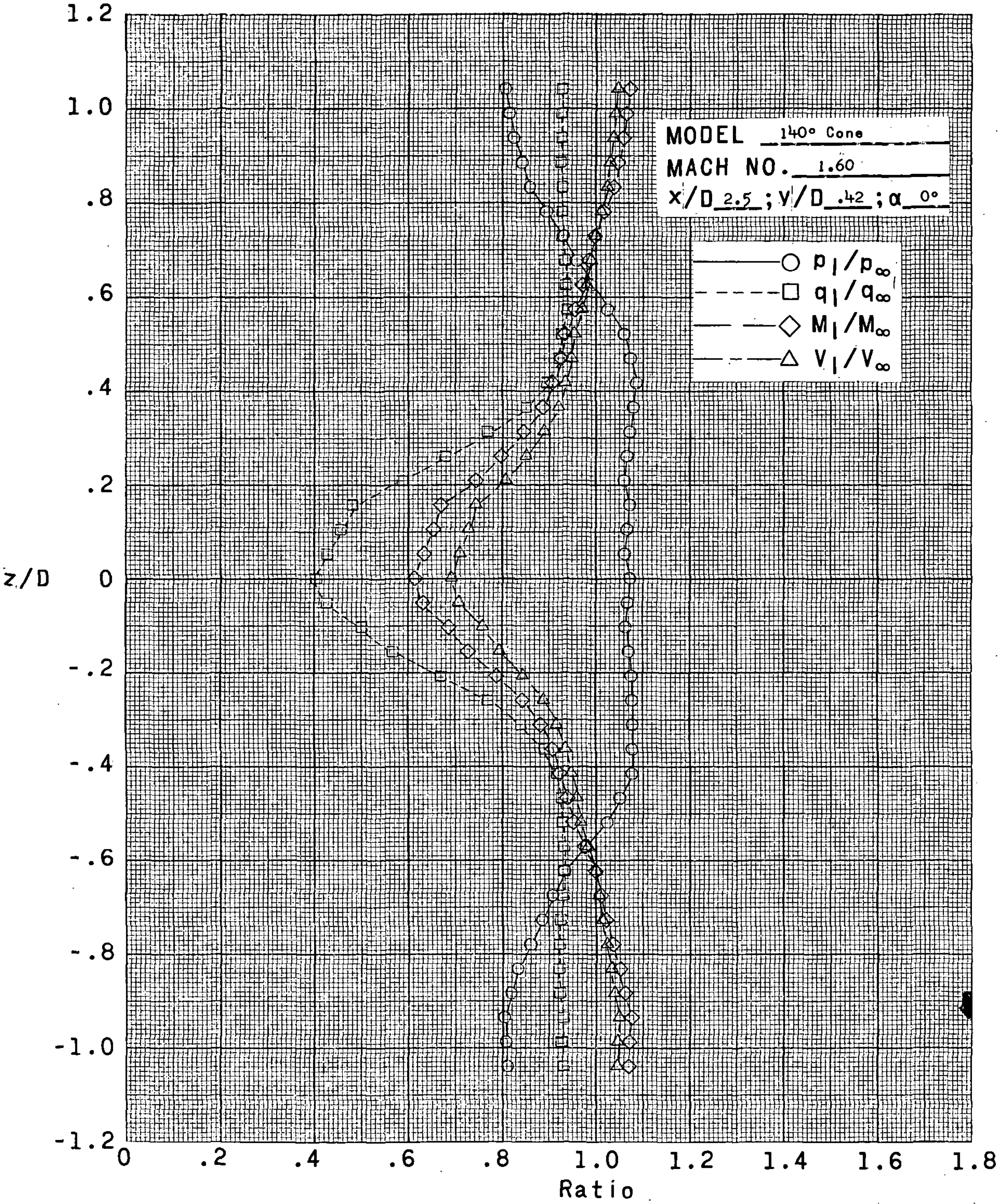
(h) $x/D = 2.5$; $y/D = 0.83$; $\alpha = 0^0$.

Figure 5.- Continued.



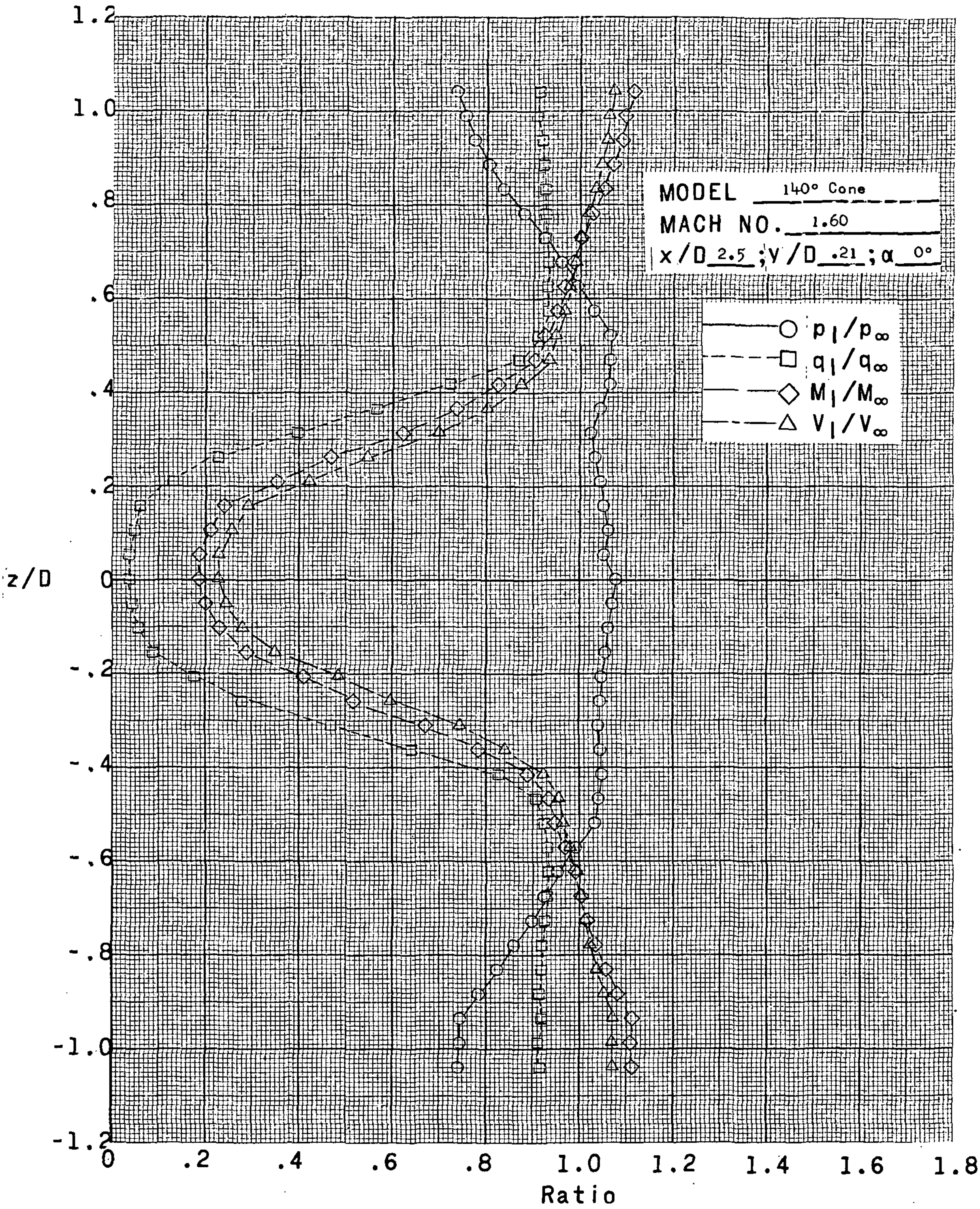
(i) $x/D = 2.5$; $y/D = 0.63$; $\alpha = 0^0$.

Figure 5.- Continued.



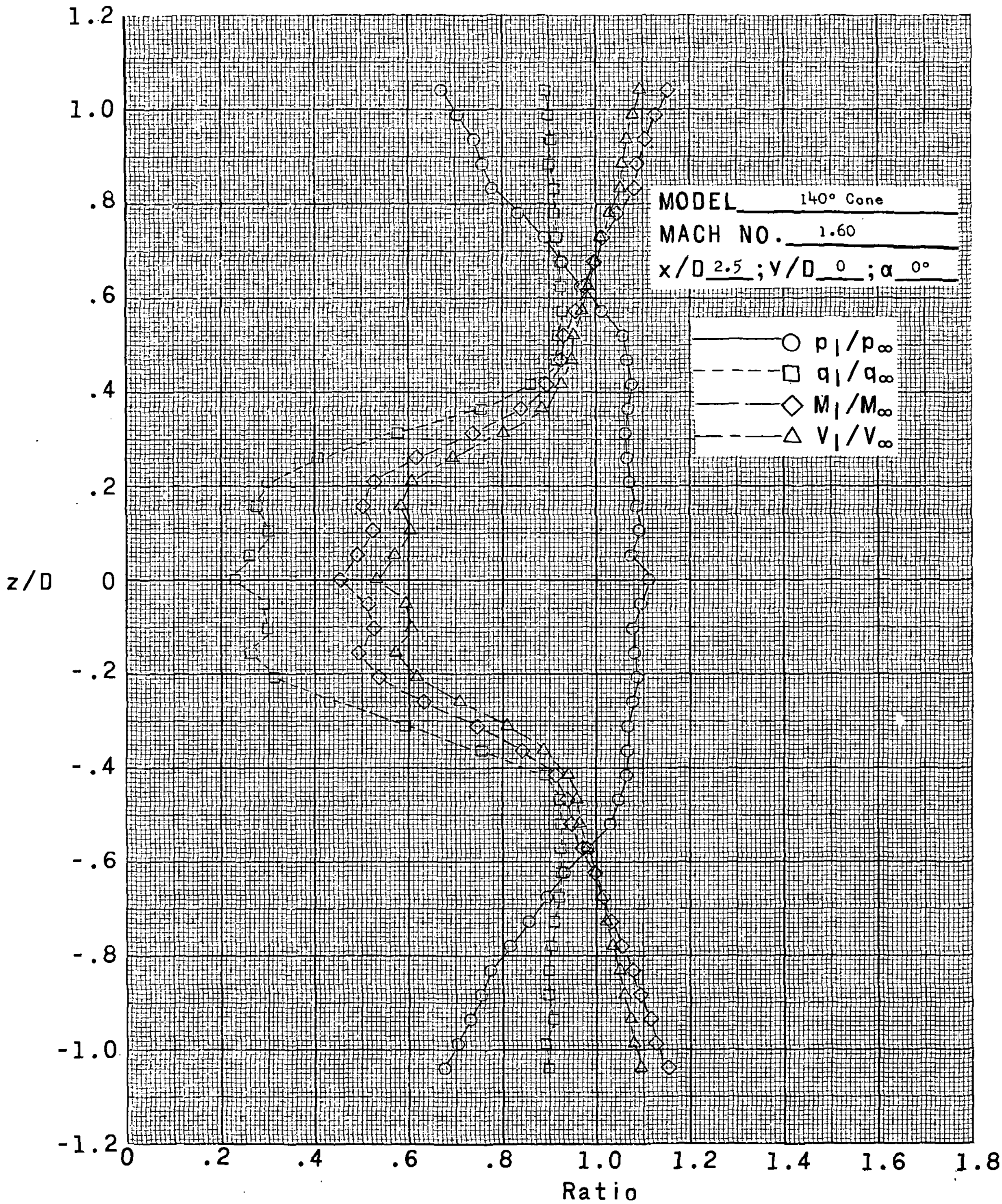
(j) x/D = 2.5; y/D = 0.42; α = 0°.

Figure 5.- Continued.



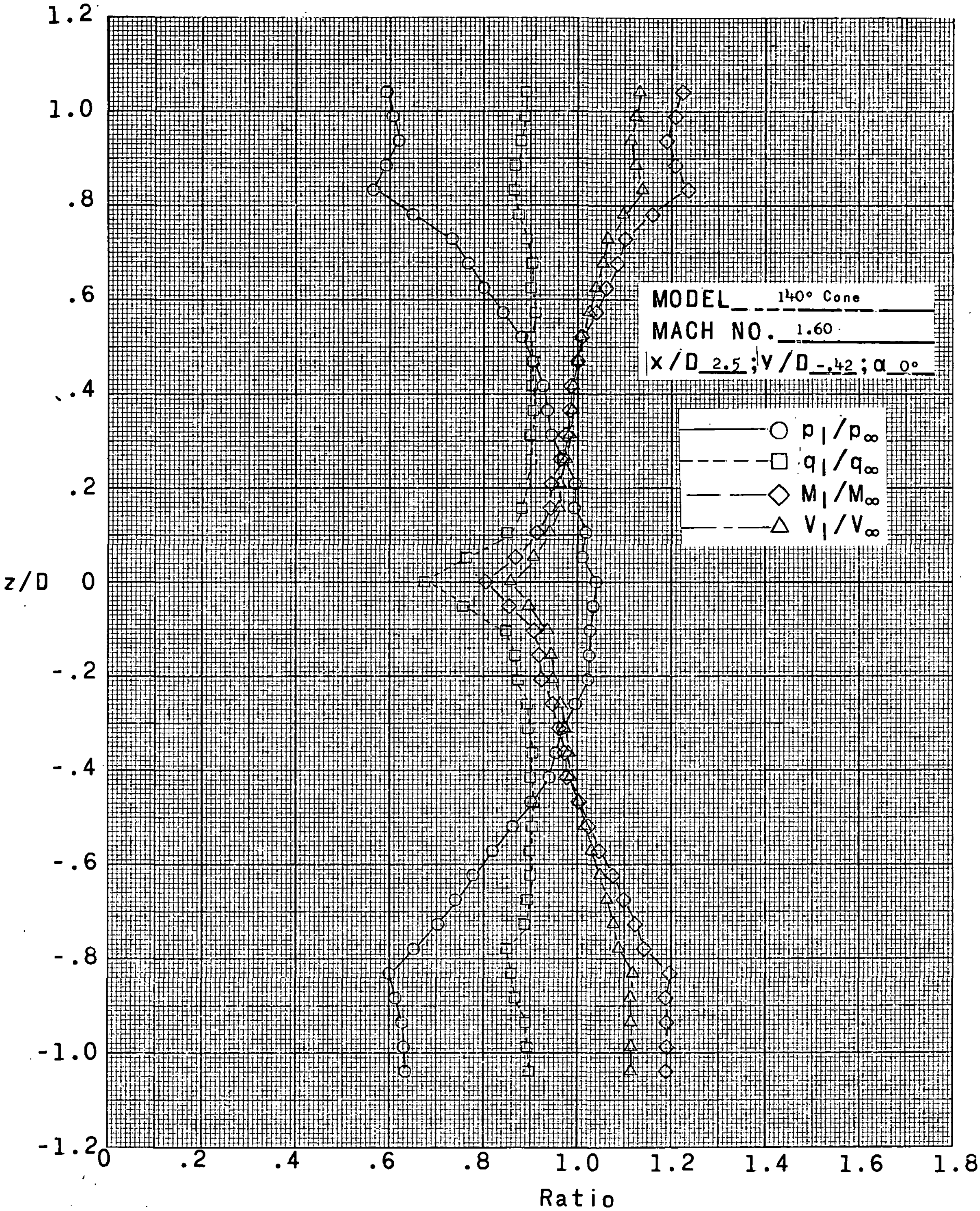
(k) $x/D = 2.5$; $y/D = 0.21$; $\alpha = 0^0$.

Figure 5.- Continued.



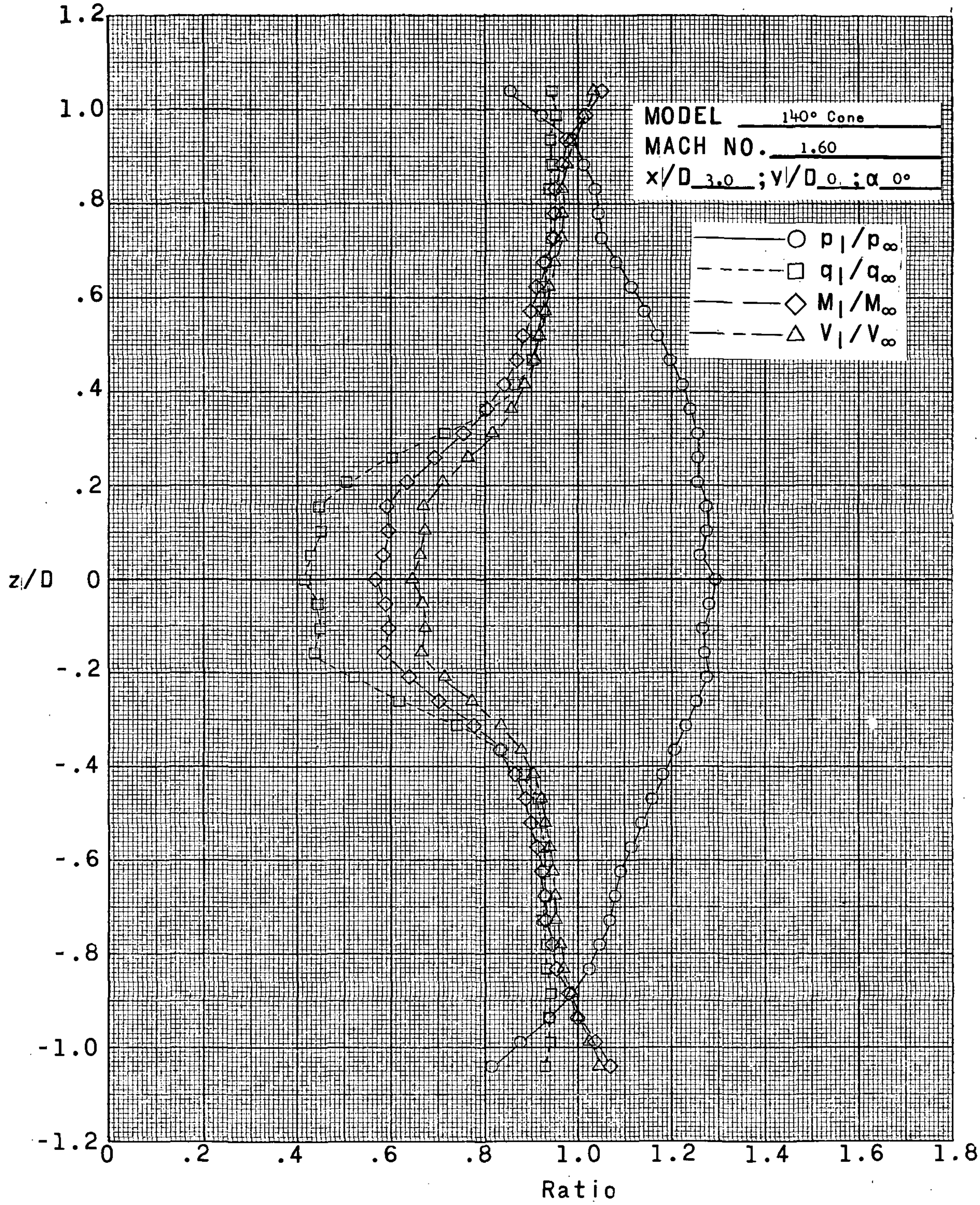
(l) $x/D = 2.5$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 5.- Continued.



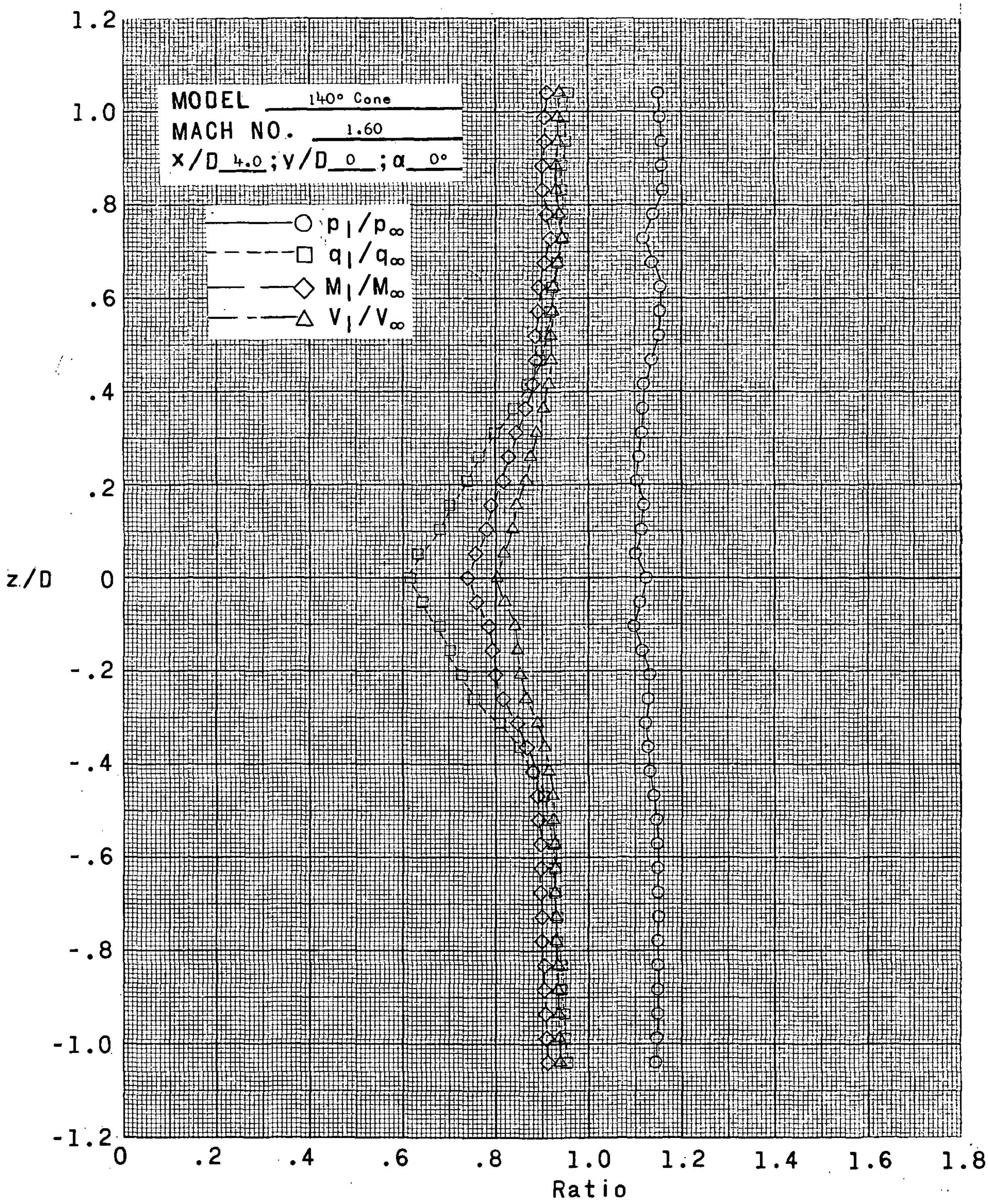
(m) $x/D = 2.5$; $y/D = -0.42$; $\alpha = 0^0$.

Figure 5.- Continued.



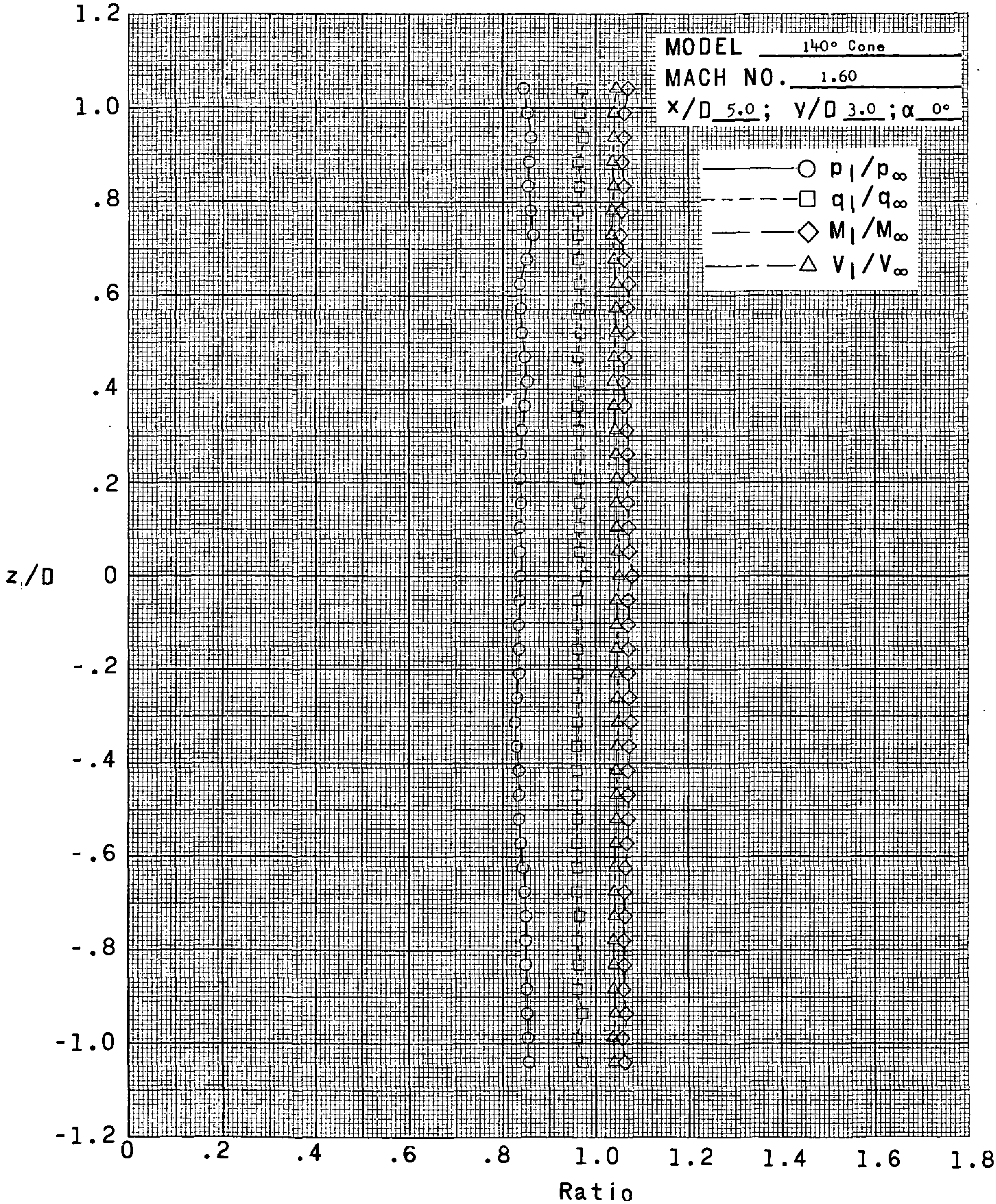
(n) $x/D = 3.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 5.- Continued.



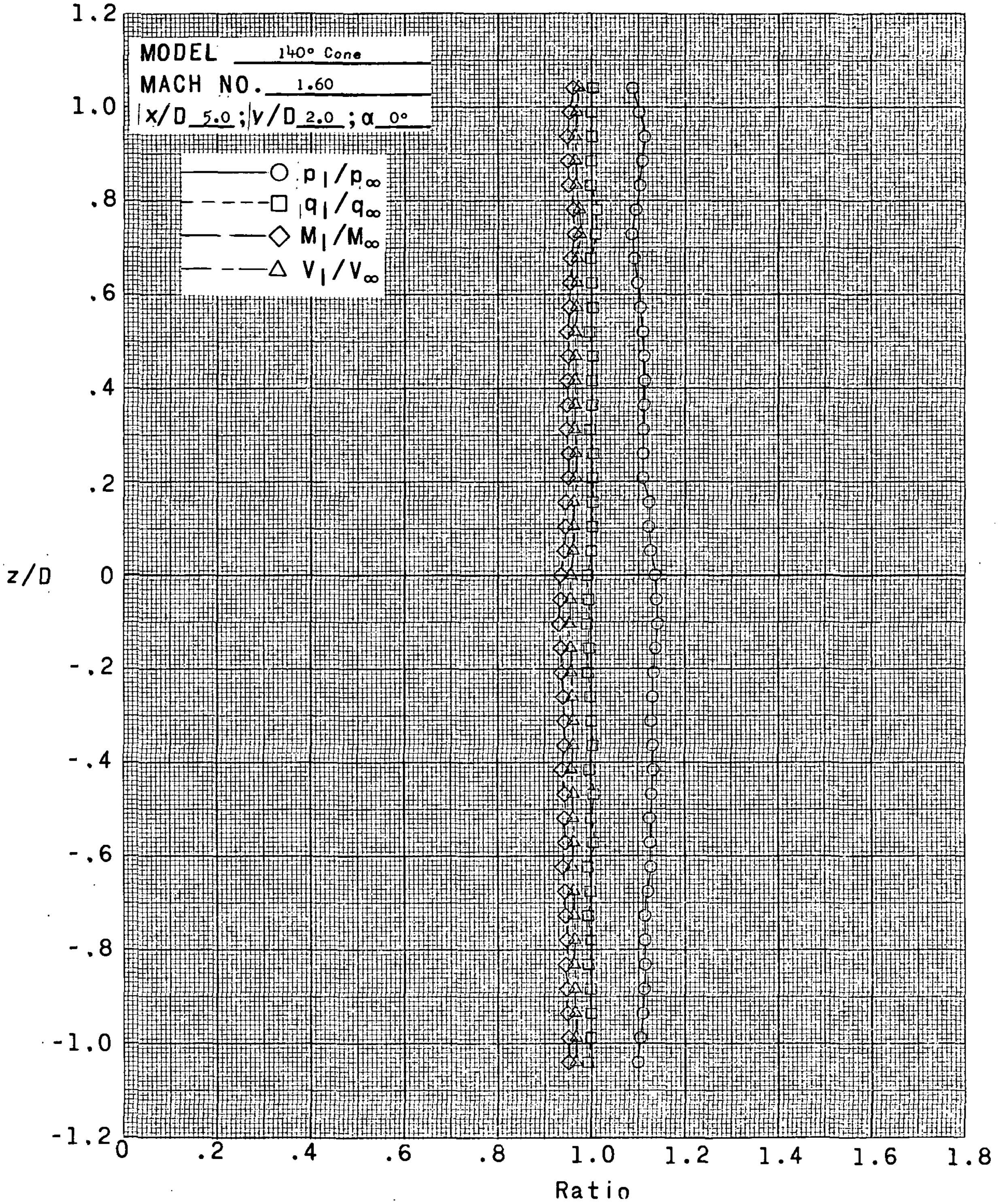
(o) $x/D = 4.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 5.- Continued.



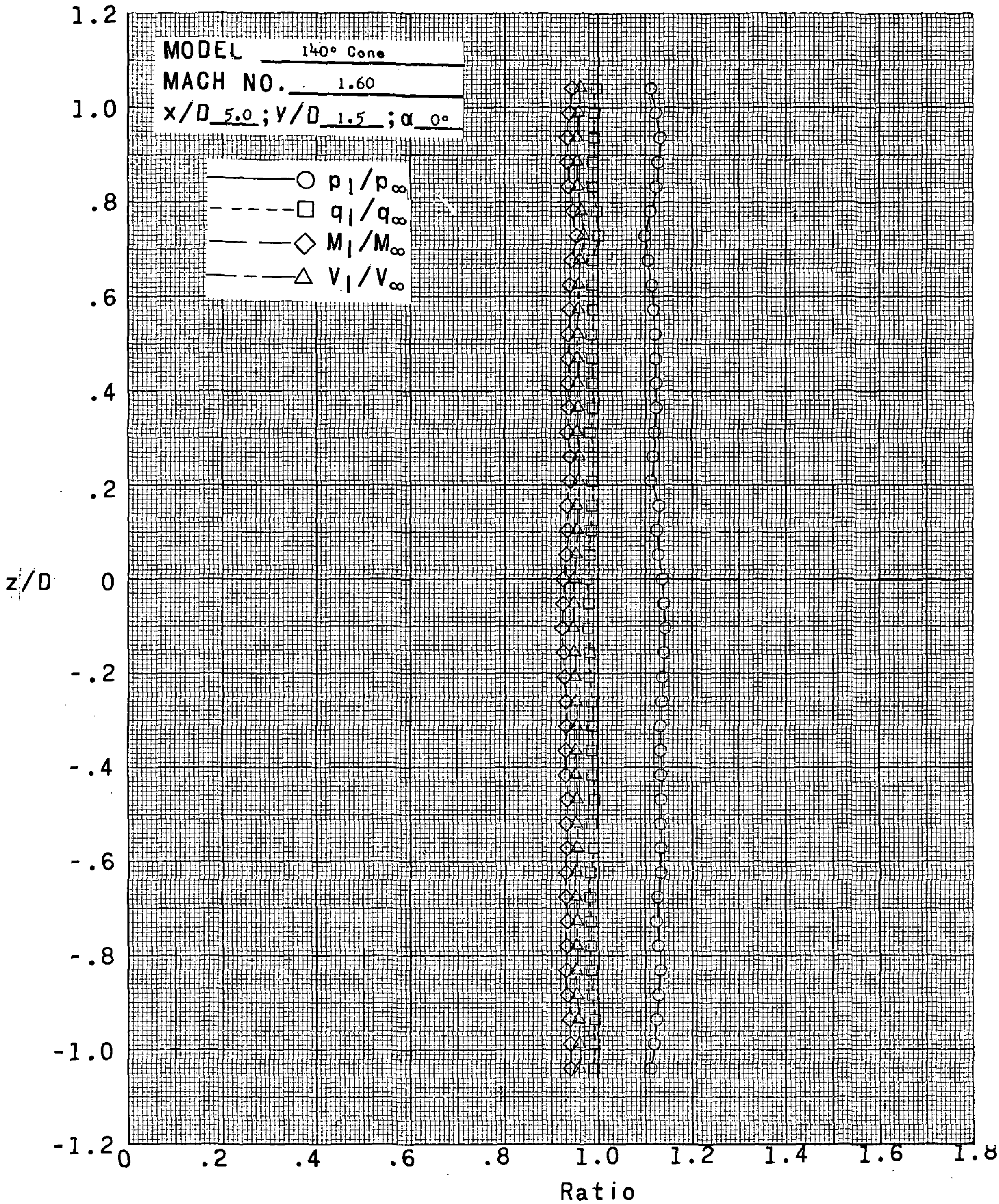
(p) $x/D = 5.0$; $y/D = 3.0$; $\alpha = 0^{0}$.

Figure 5.- Continued.



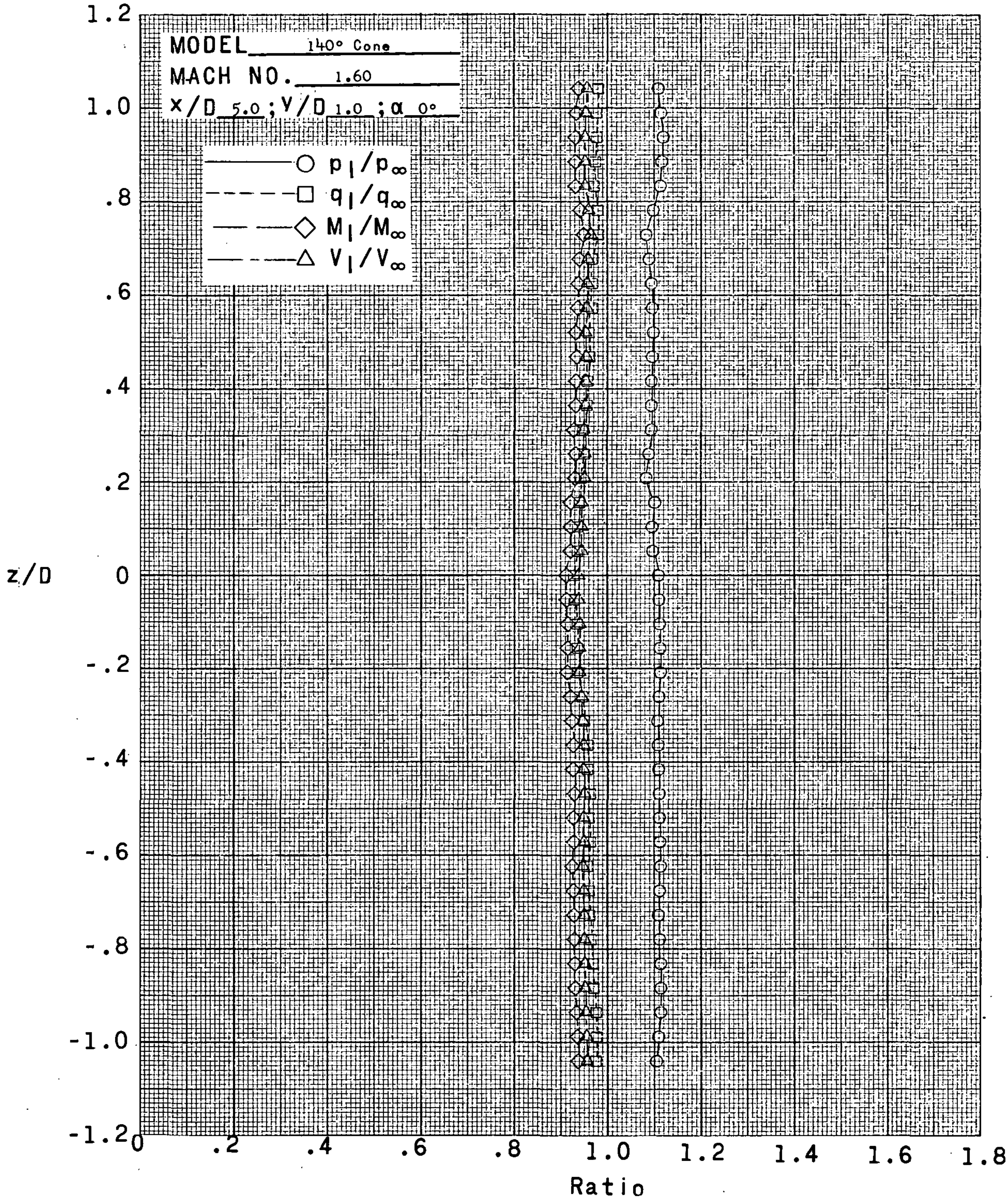
(q) $x/D = 5.0$; $y/D = 2.0$; $\alpha = 0^{0}$.

Figure 5.- Continued.



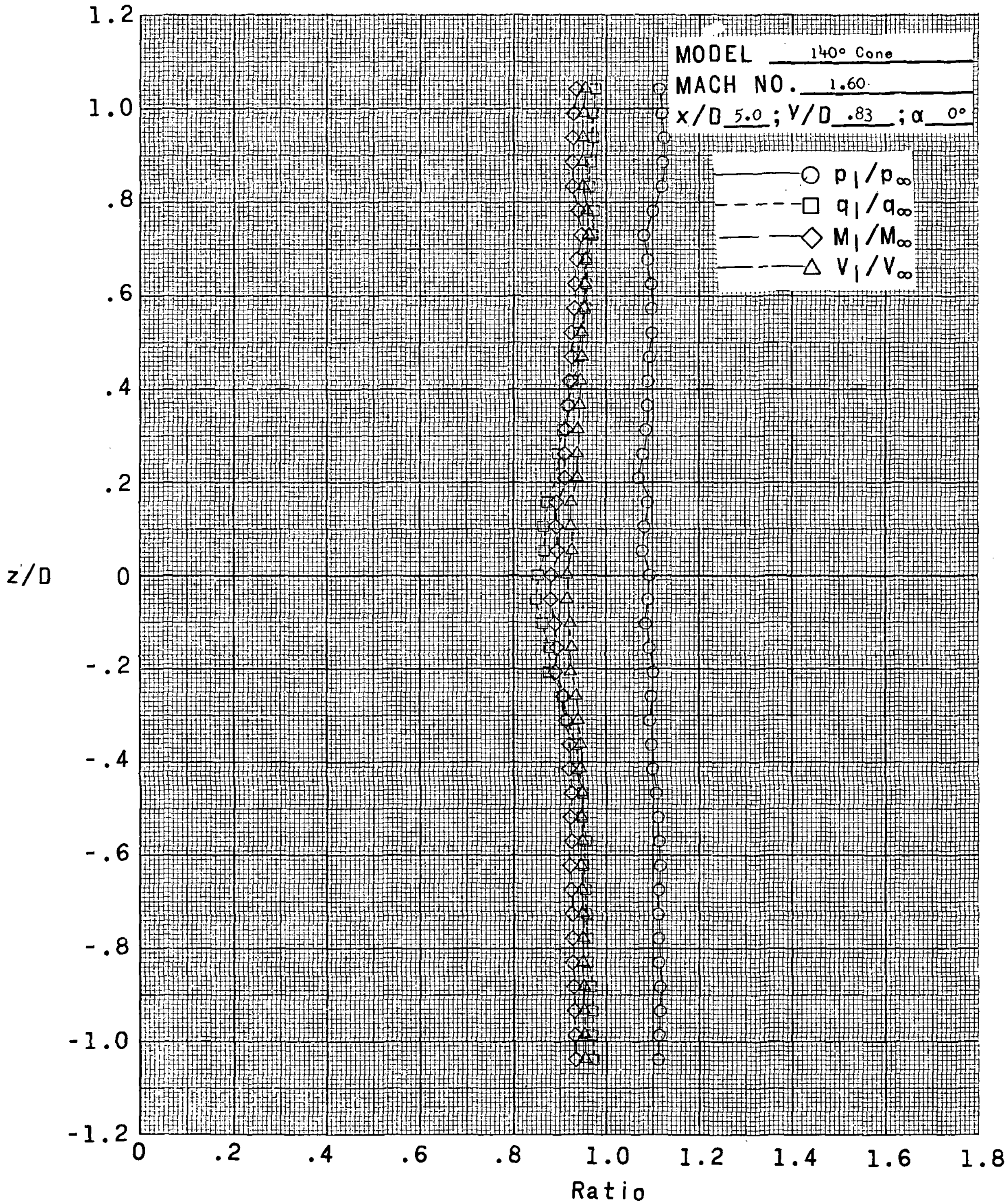
(r) $x/D = 5.0$; $y/D = 1.5$; $\alpha = 0^0$.

Figure 5.- Continued.



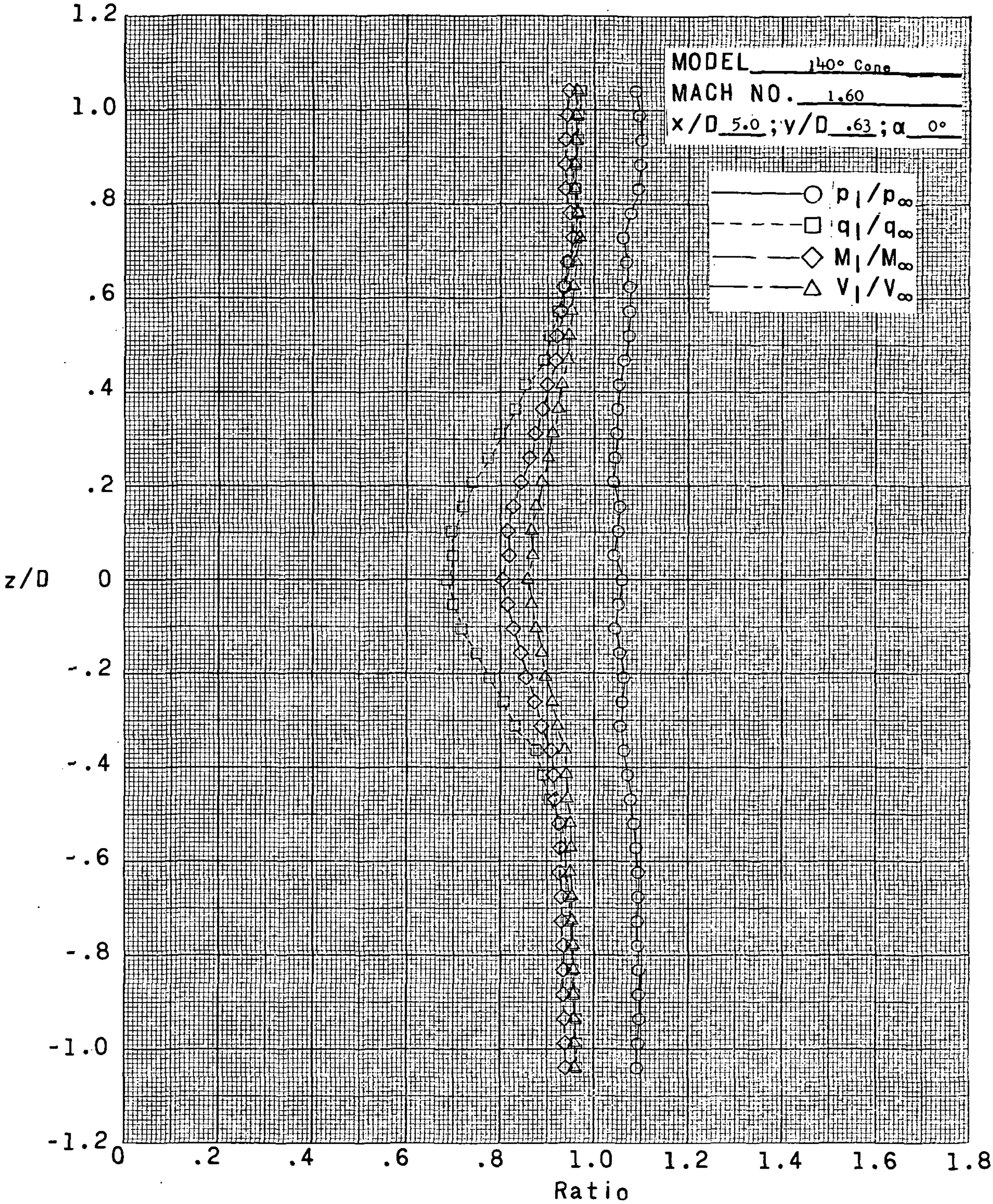
(s) $x/D = 5.0$; $y/D = 1.0$; $\alpha = 0^{0}$.

Figure 5.- Continued.



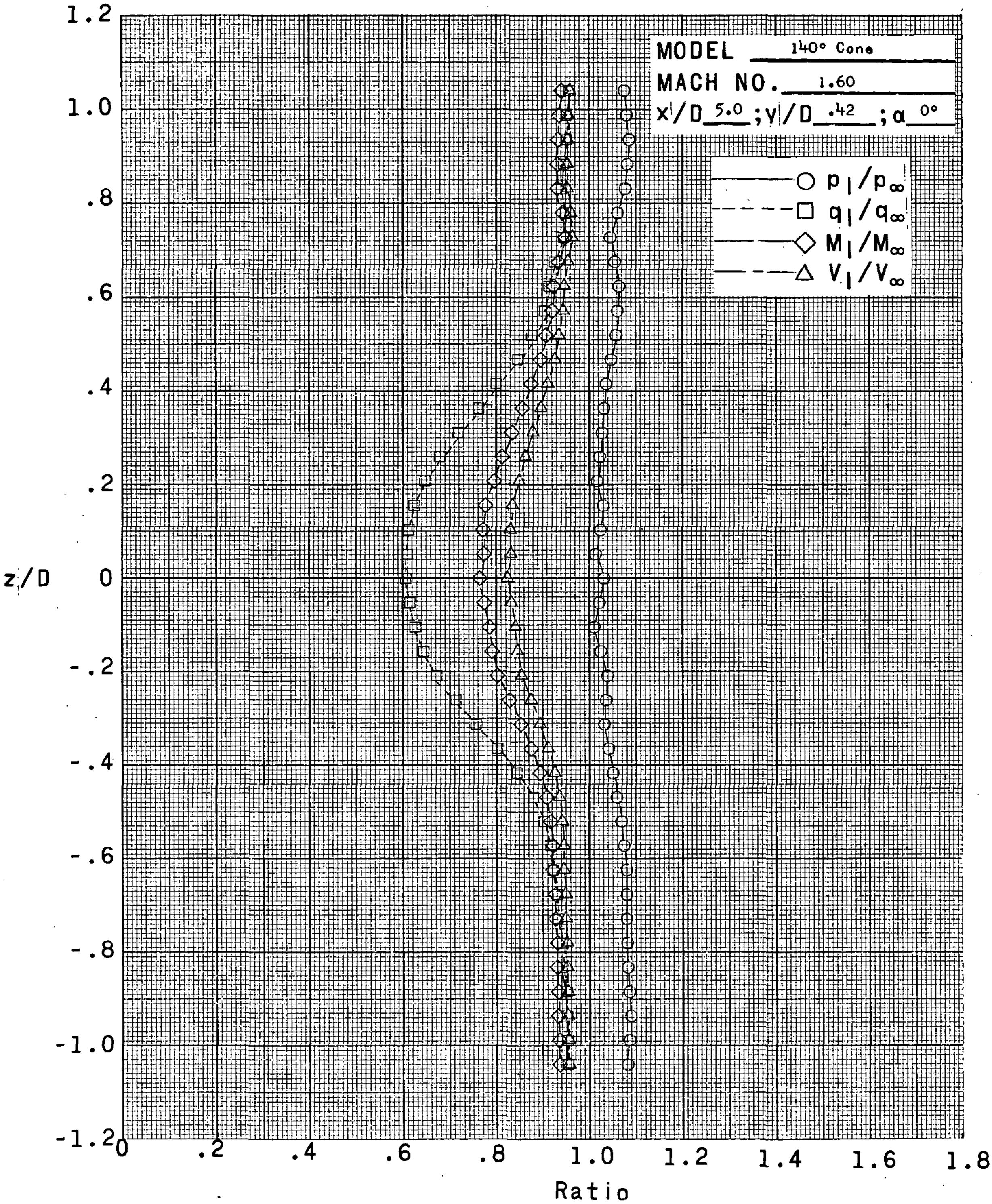
(t) $x/D = 5.0$; $y/D = 0.83$; $\alpha = 0^{\circ}$.

Figure 5.- Continued.



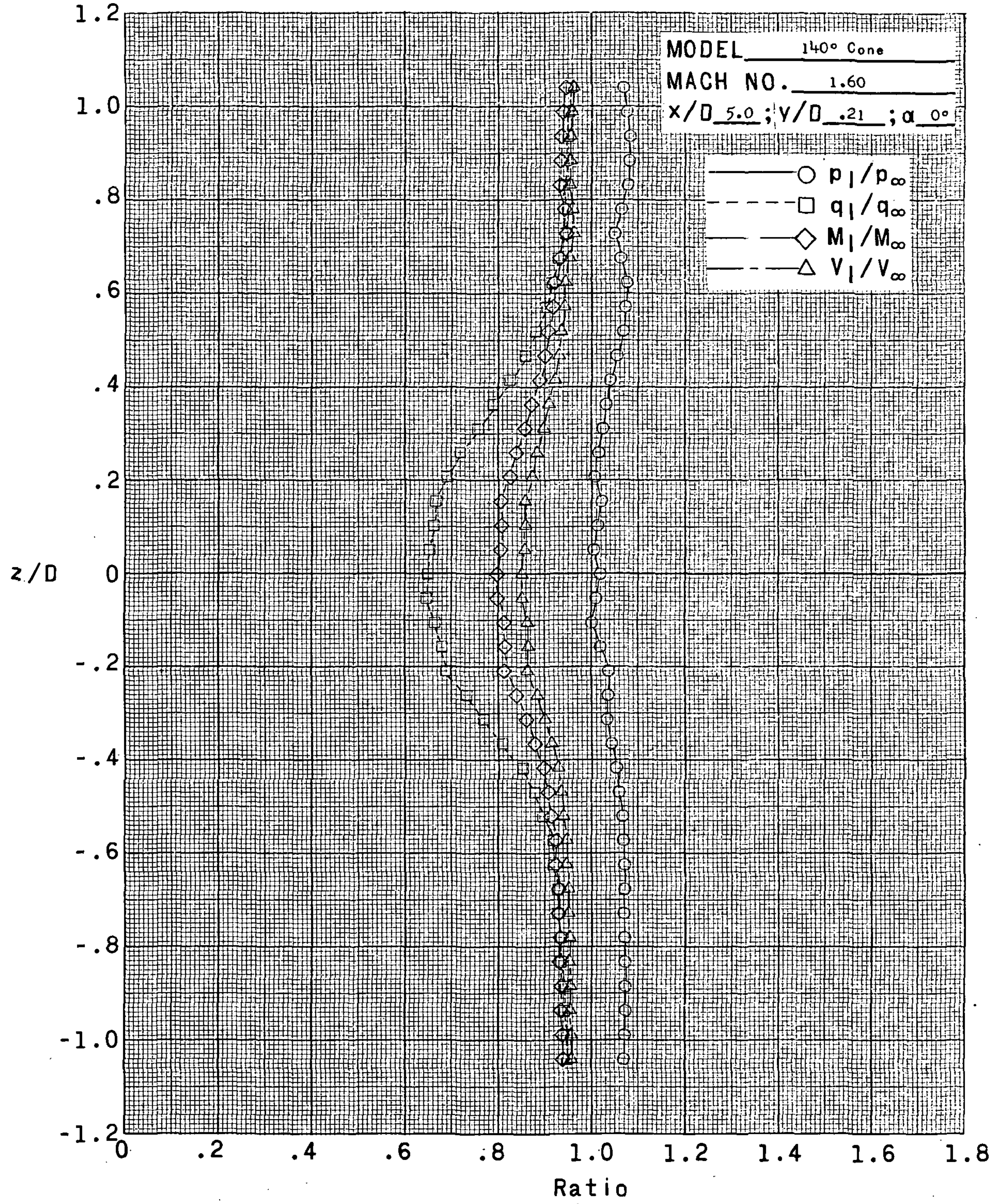
(u) x/D = 5.0; y/D = 0.63; α = 0°.

Figure 5.- Continued.



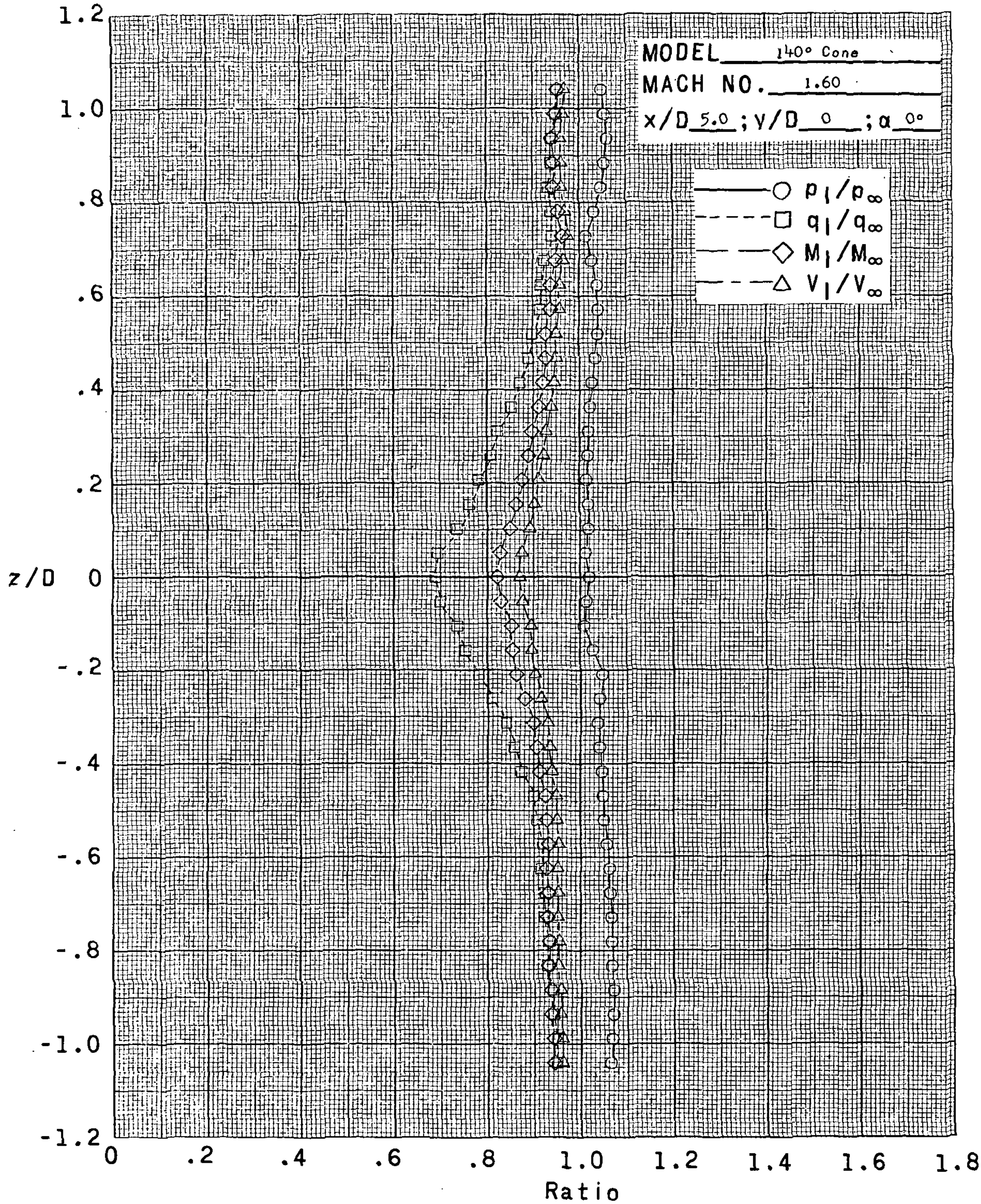
(v) x/D = 5.0; y/D = 0.42; α = 0°.

Figure 5.- Continued.



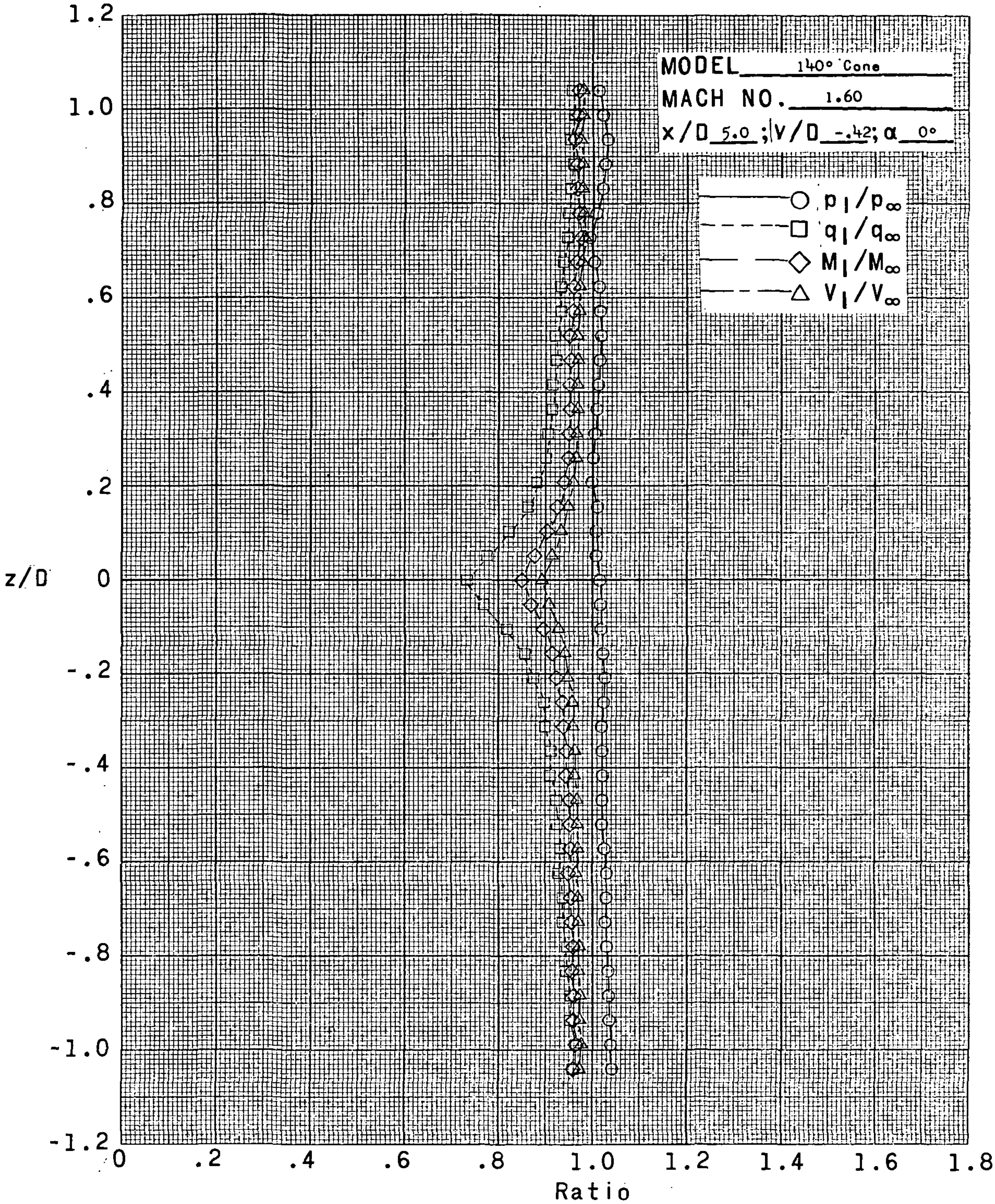
(w) $x/D = 5.0$; $y/D = 0.21$; $\alpha = 0^0$.

Figure 5.- Continued.



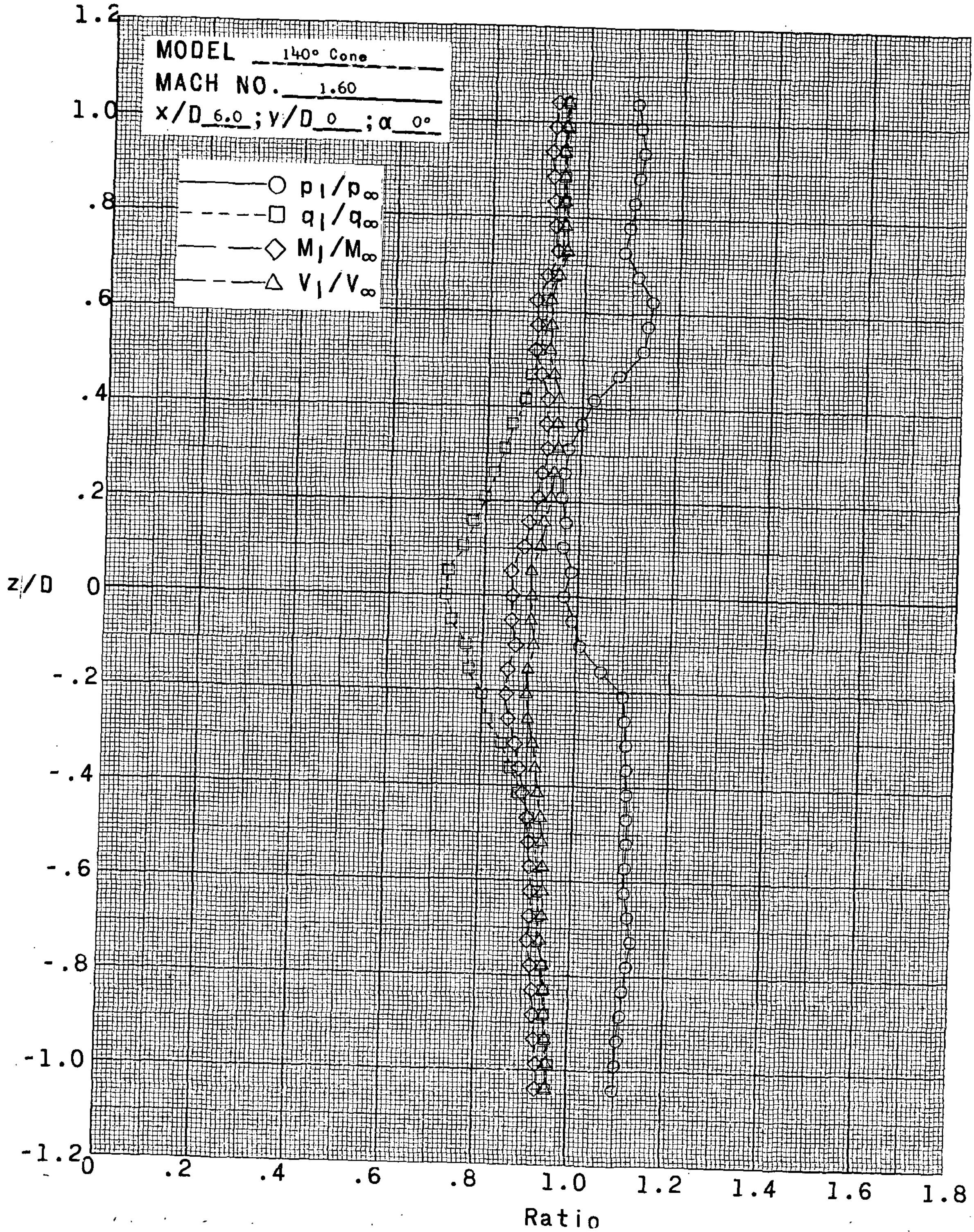
(x) x/D = 5.0; y/D = 0; α = 0°.

Figure 5.- Continued.



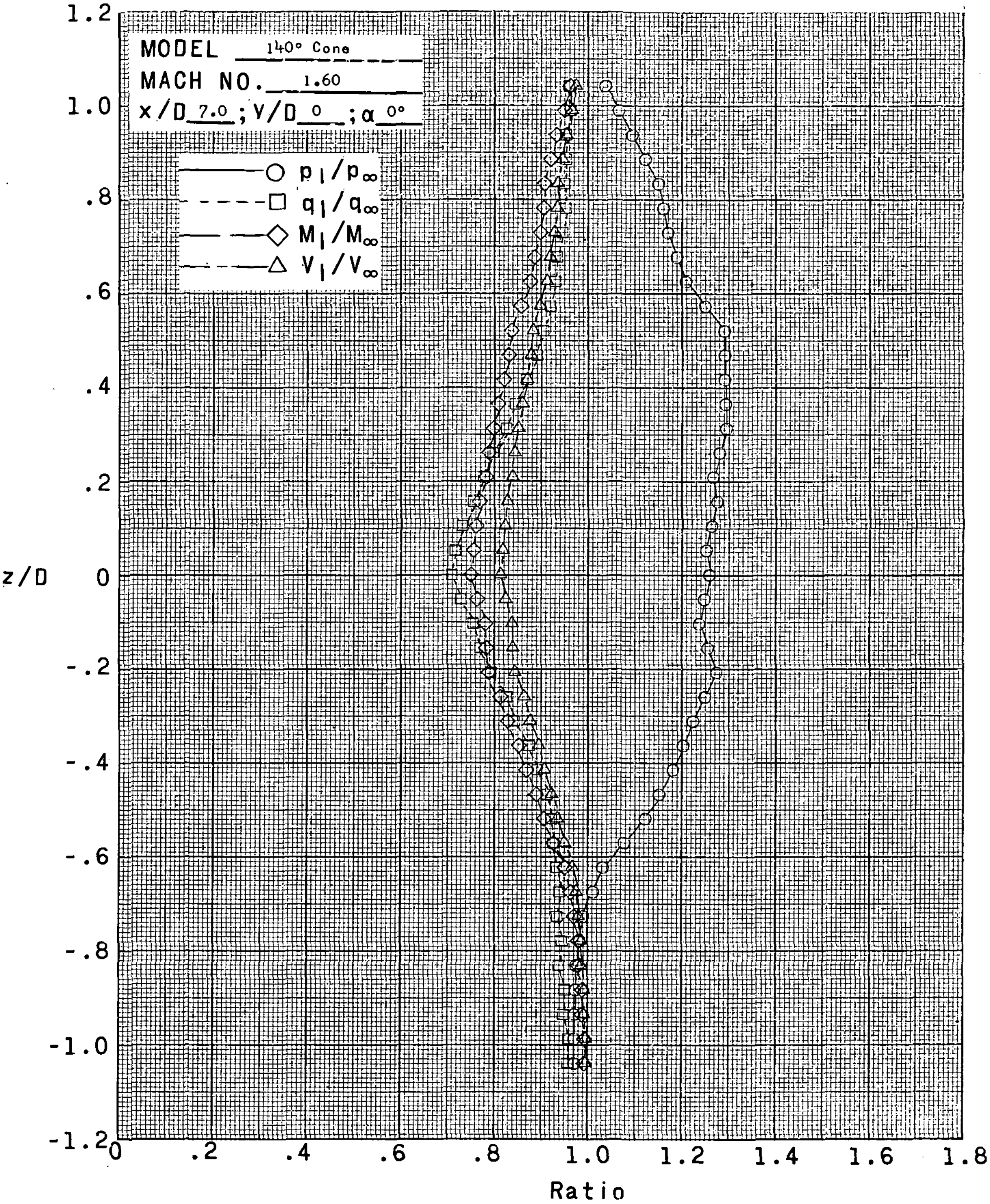
(y) $x/D = 5.0$; $y/D = -0.42$; $\alpha = 0^{0}$.

Figure 5.- Continued.



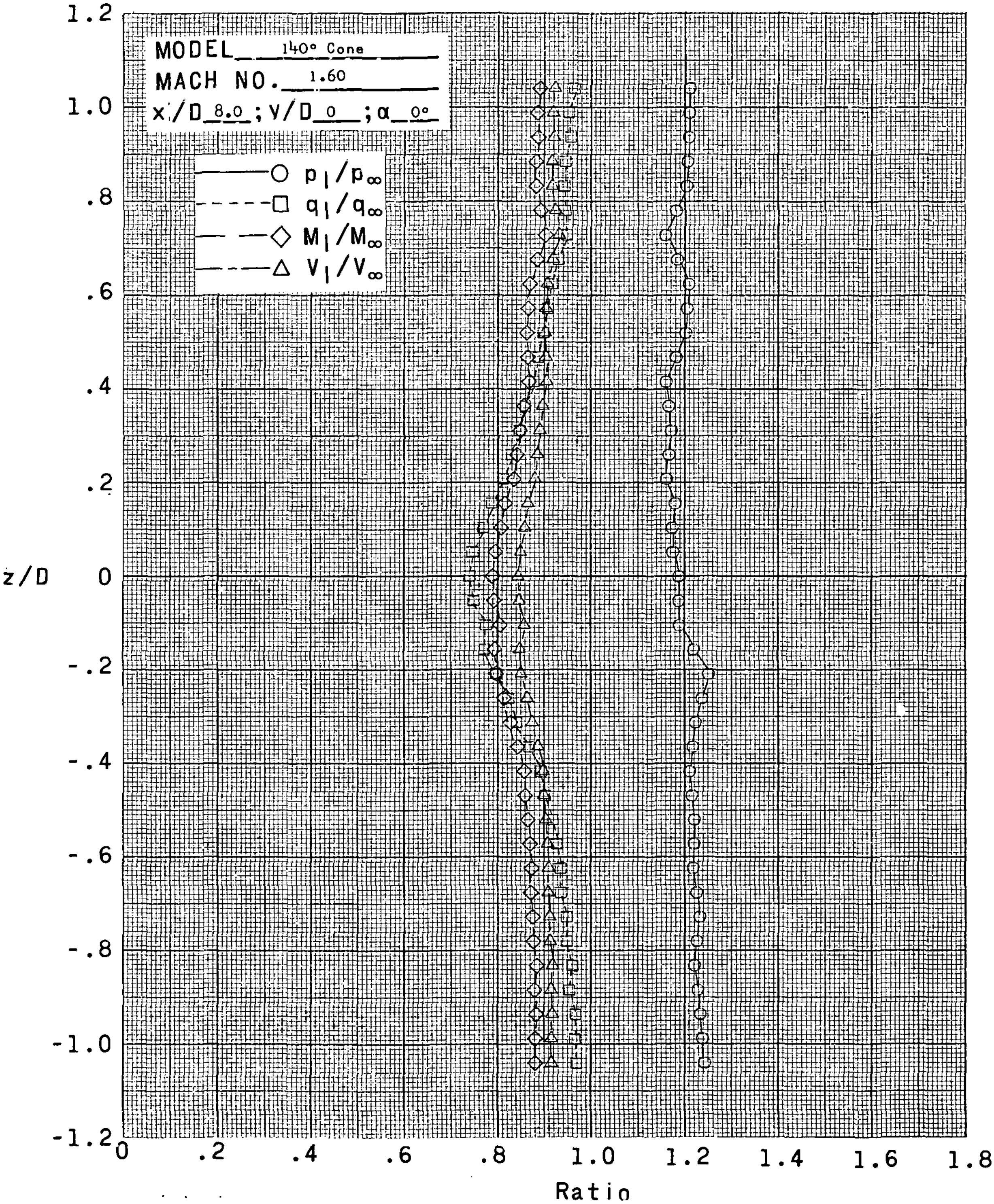
(z) $x/D = 6.0$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 5.- Continued.



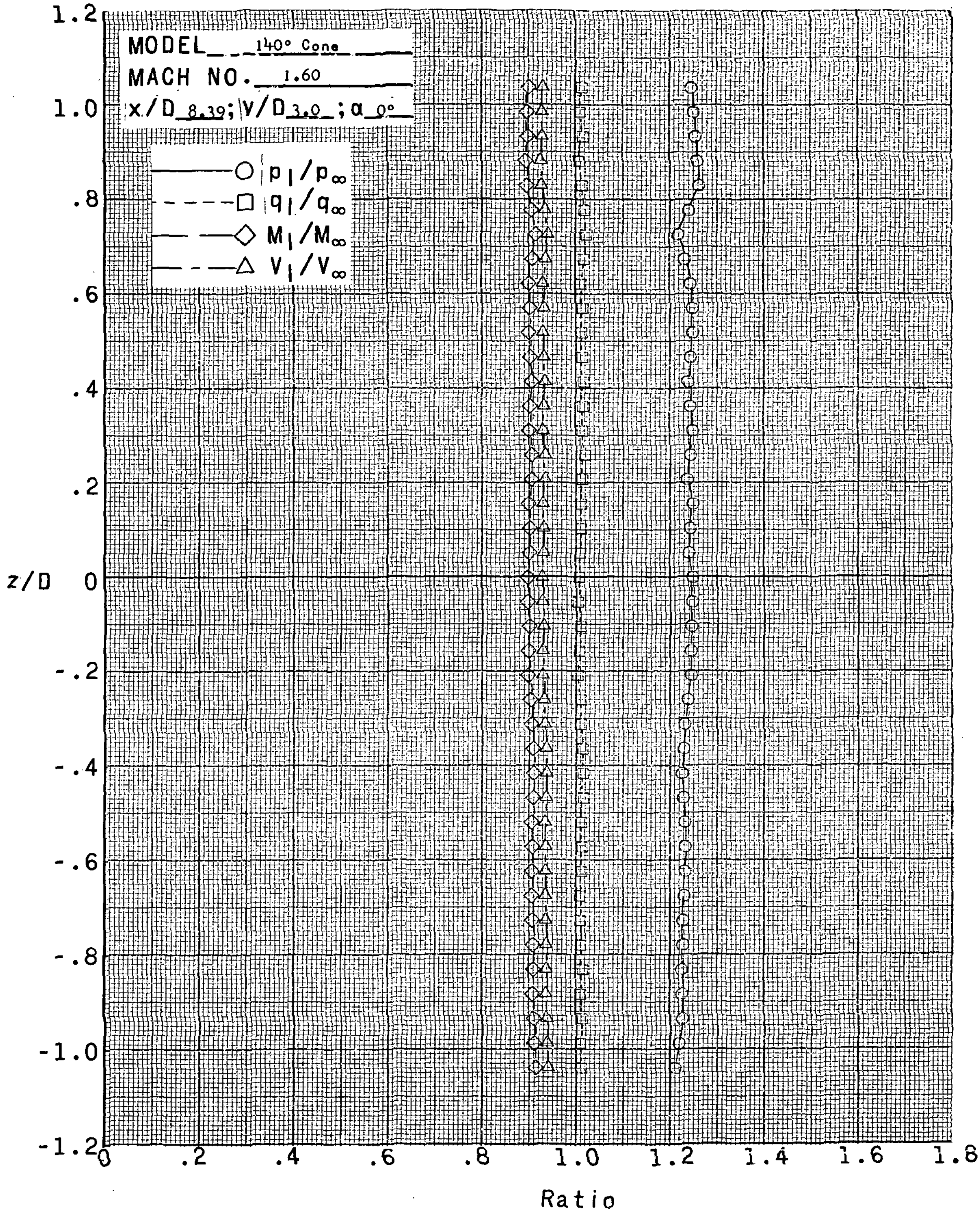
(aa) x/D = 7.0; y/D = 0; α = 0°.

Figure 5.- Continued.



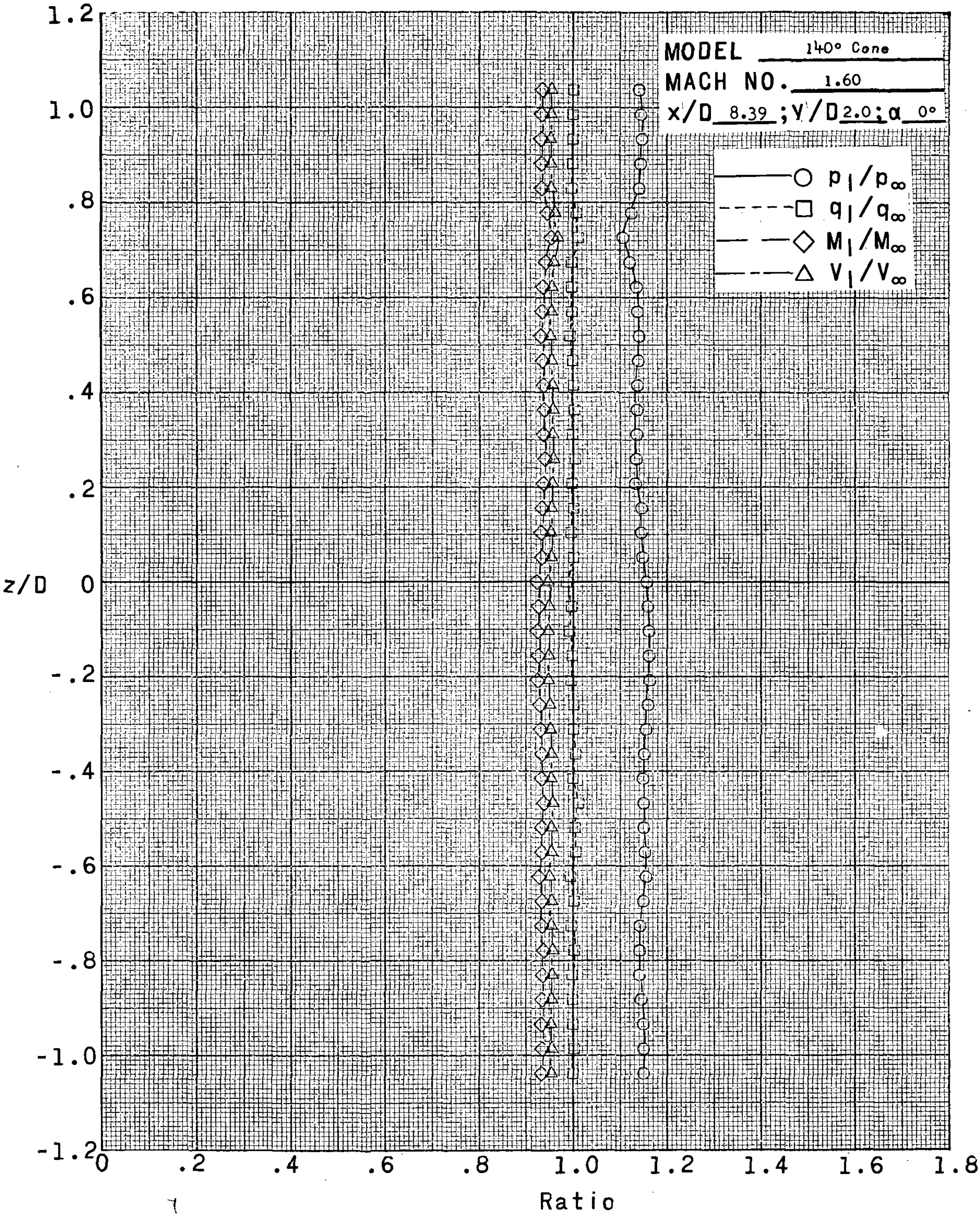
(bb) x/D = 8.0; y/D = 0; α = 0°.

Figure 5.- Continued.



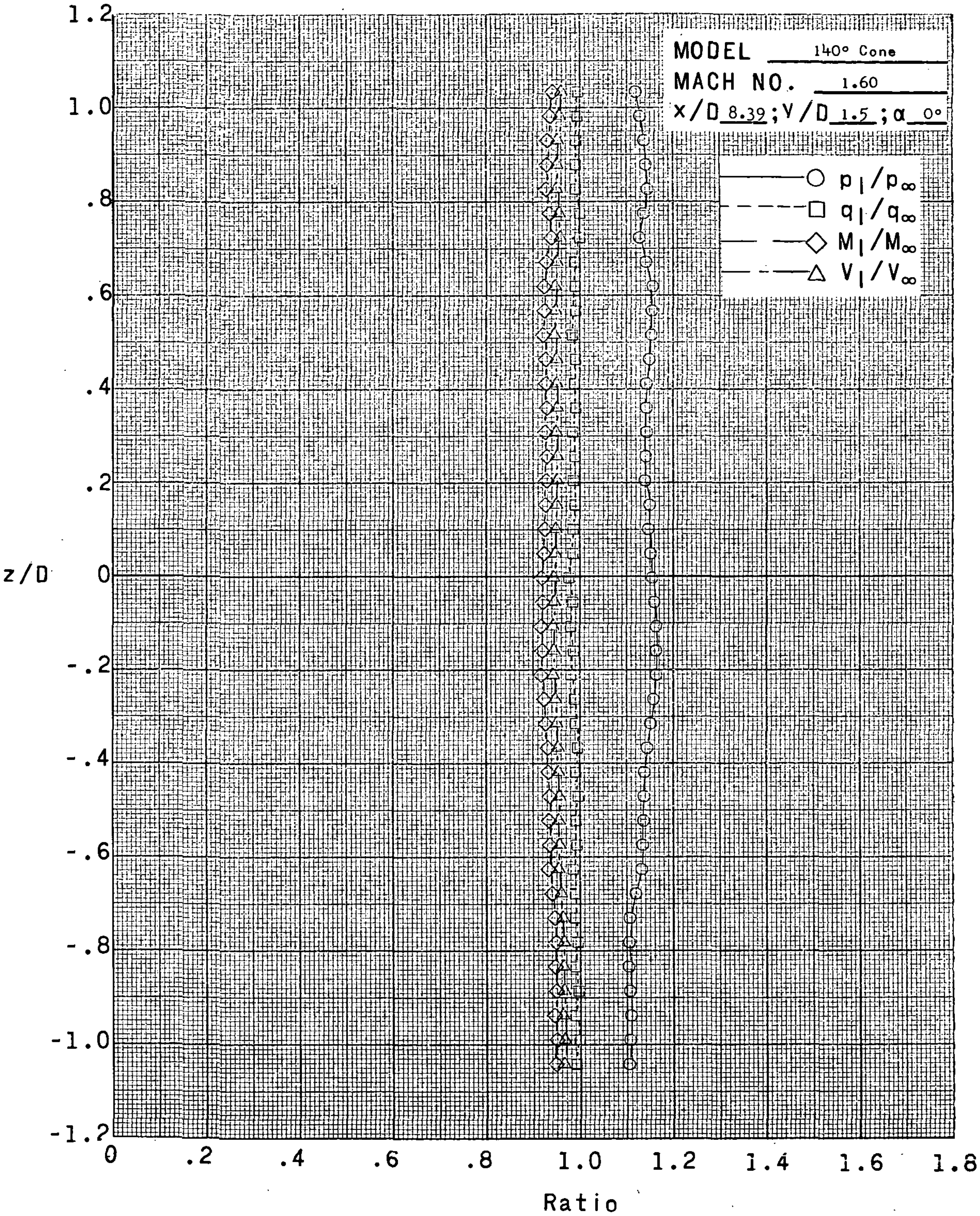
(cc) $x/D = 8.39$; $y/D = 3.0$; $\alpha = 0°$.

Figure 5.- Continued.



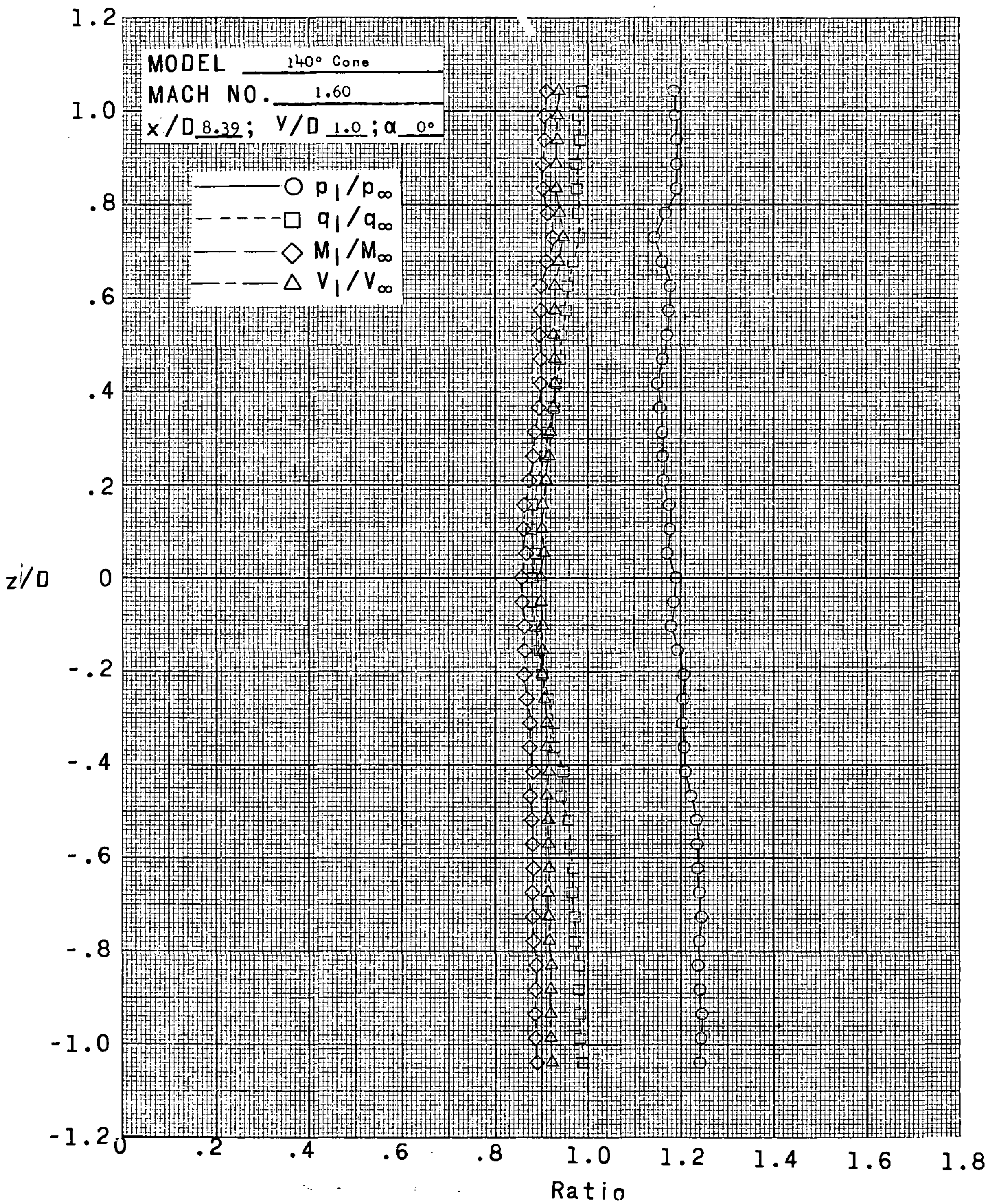
(dd) $x/D = 8.39$; $y/D = 2.0$; $\alpha = 0^{\circ}$.

Figure 5.- Continued.



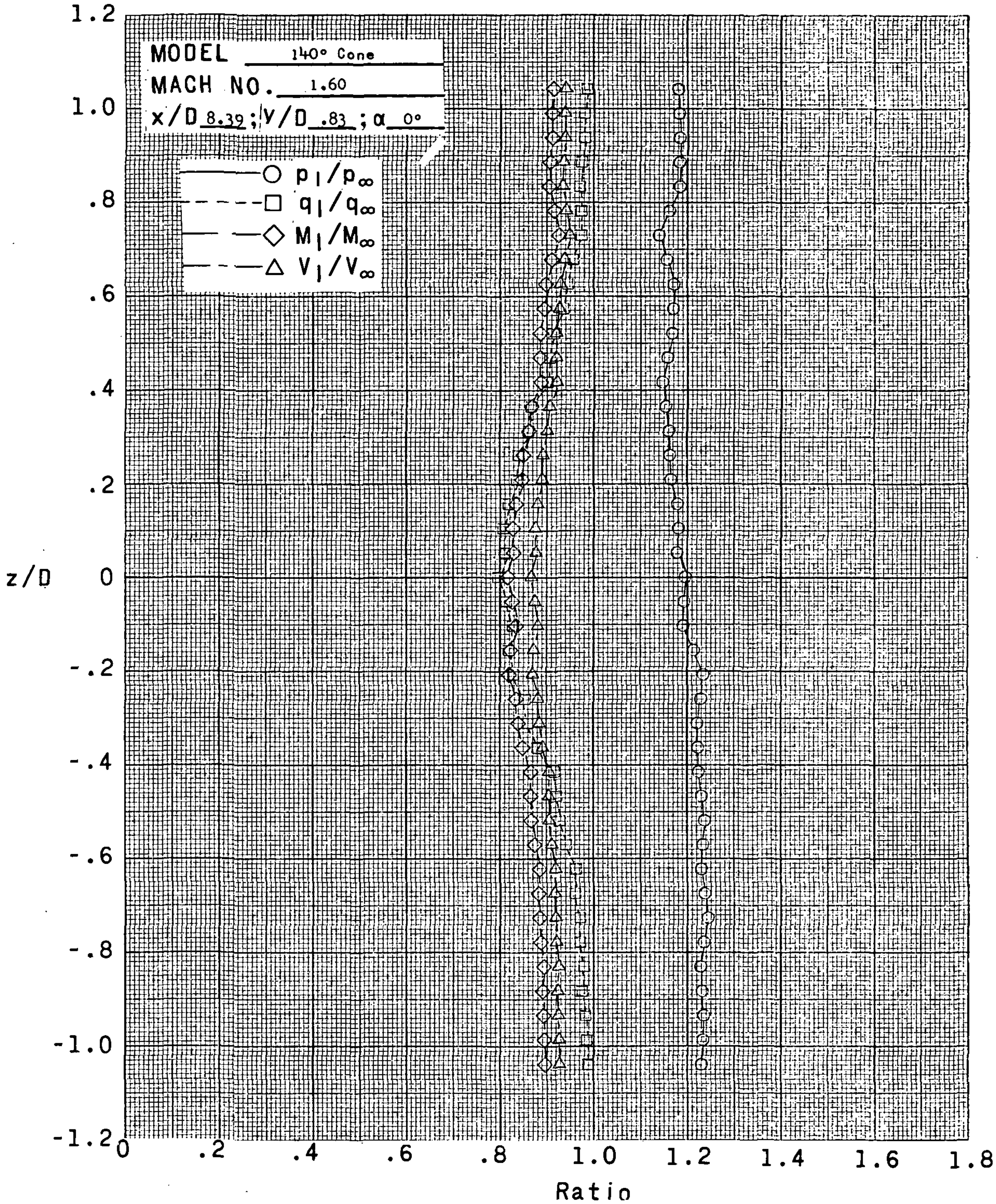
(ee) x/D = 8.39; y/D = 1.5; α = 0°.

Figure 5.- Continued.



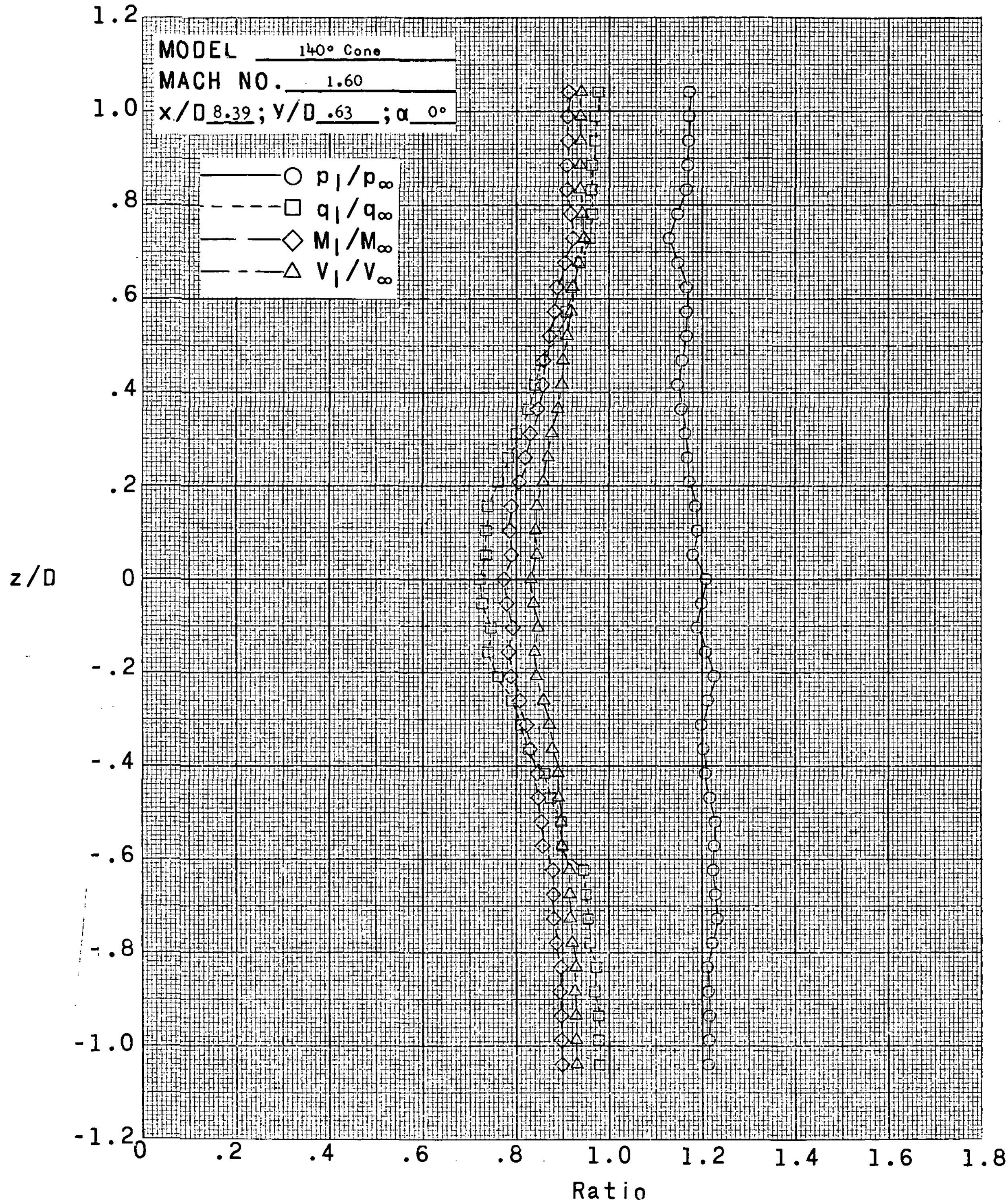
(ff) $x/D = 8.39$; $y/D = 1.0$; $\alpha = 0^{0}$.

Figure 5.- Continued.



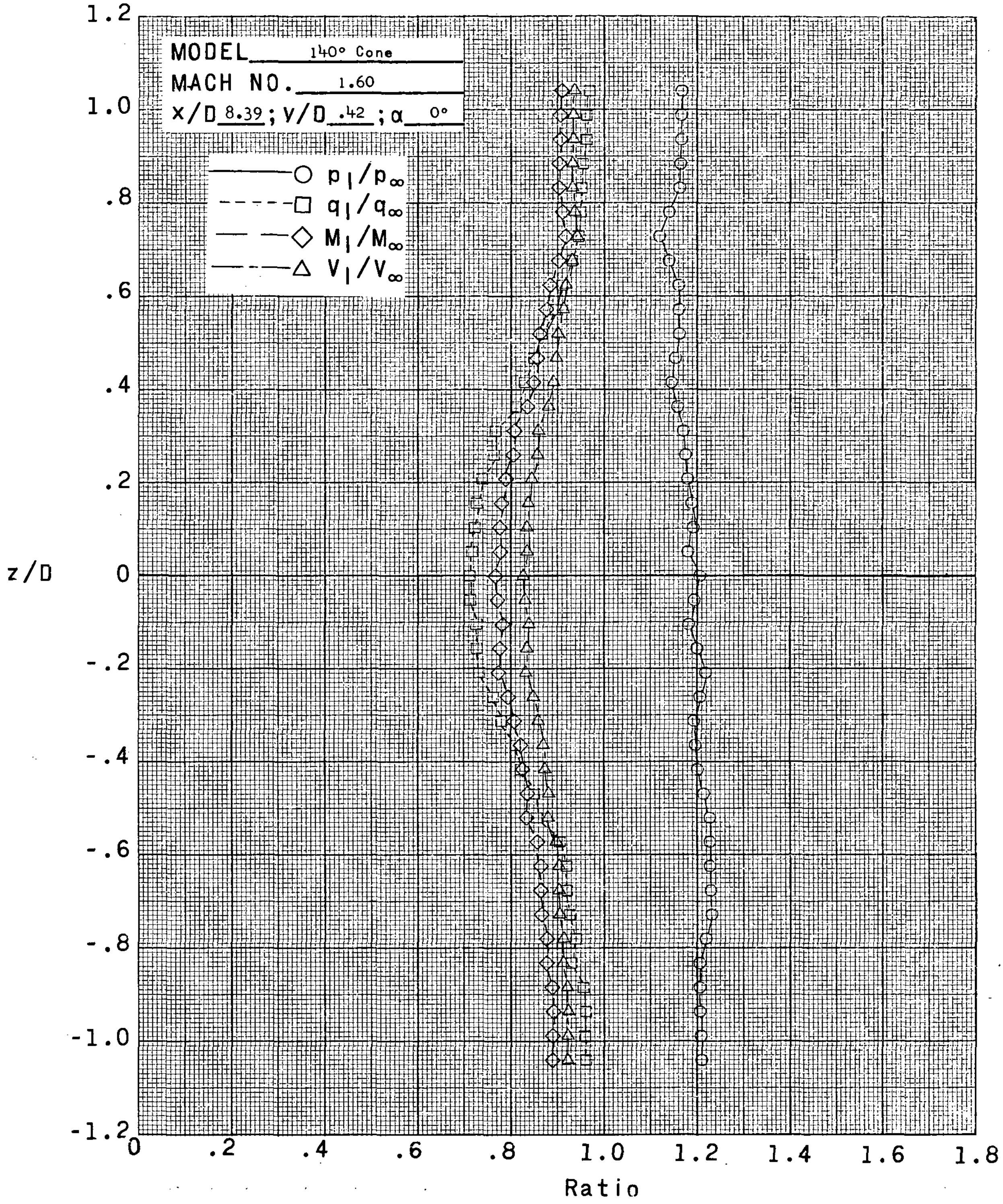
(gg) $x/D = 8.39$; $y/D = 0.83$; $\alpha = 0^{o}$.

Figure 5.- Continued.



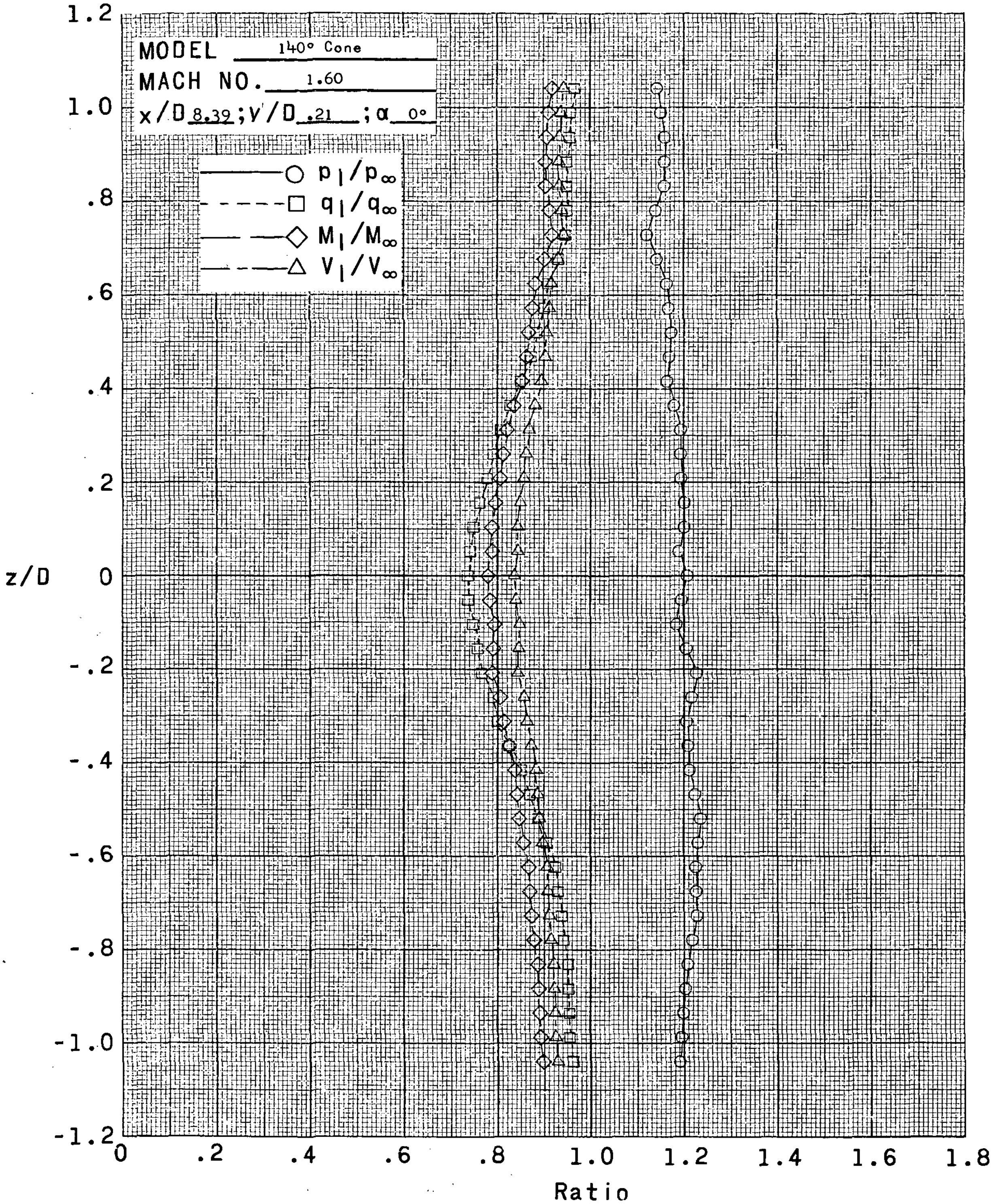
(hh) $x/D = 8.39$; $y/D = 0.63$; $\alpha = 0^0$.

Figure 5.- Continued.



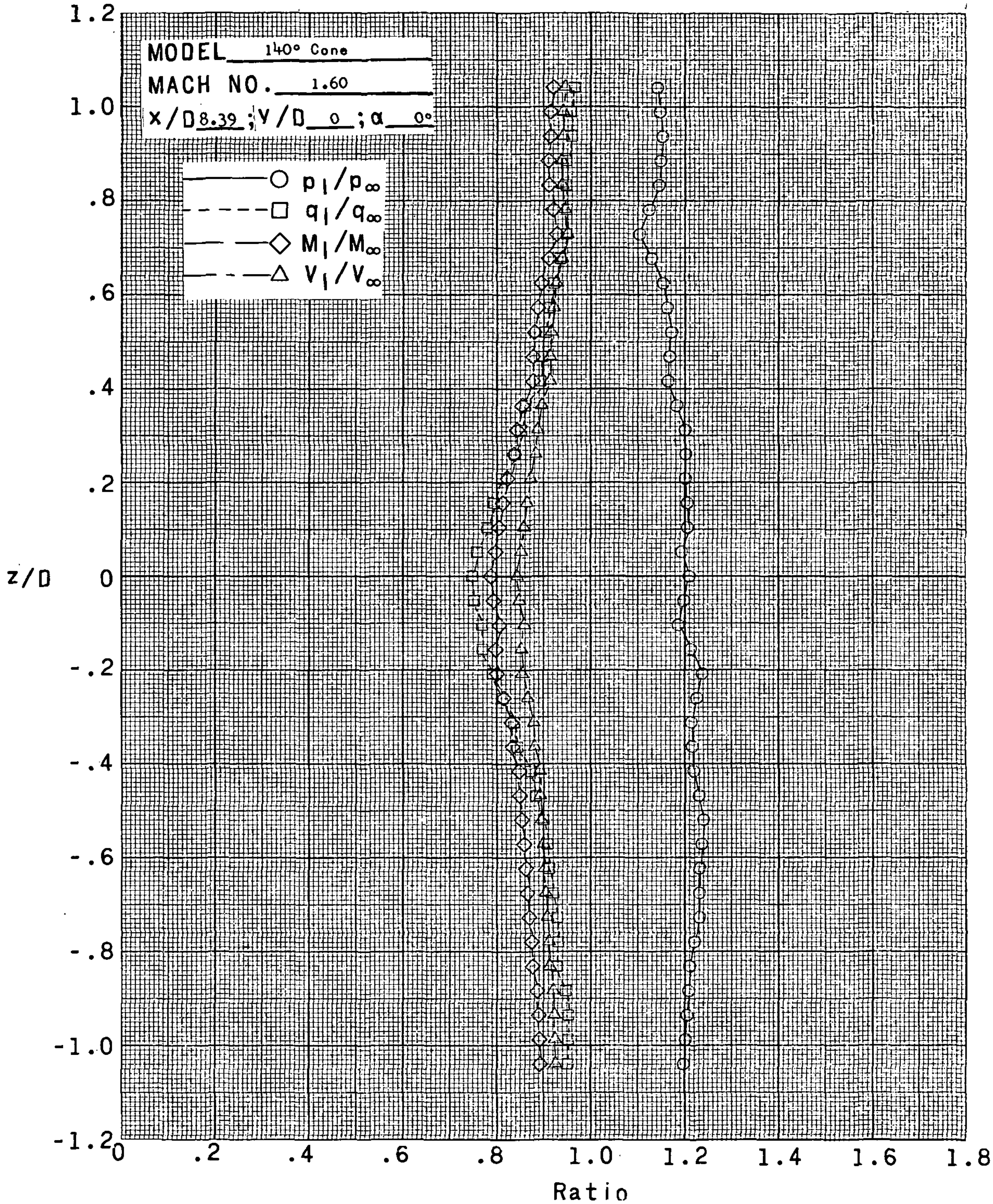
(ii) $x/D = 8.39$; $y/D = 0.42$; $\alpha = 0^0$.

Figure 5.- Continued.



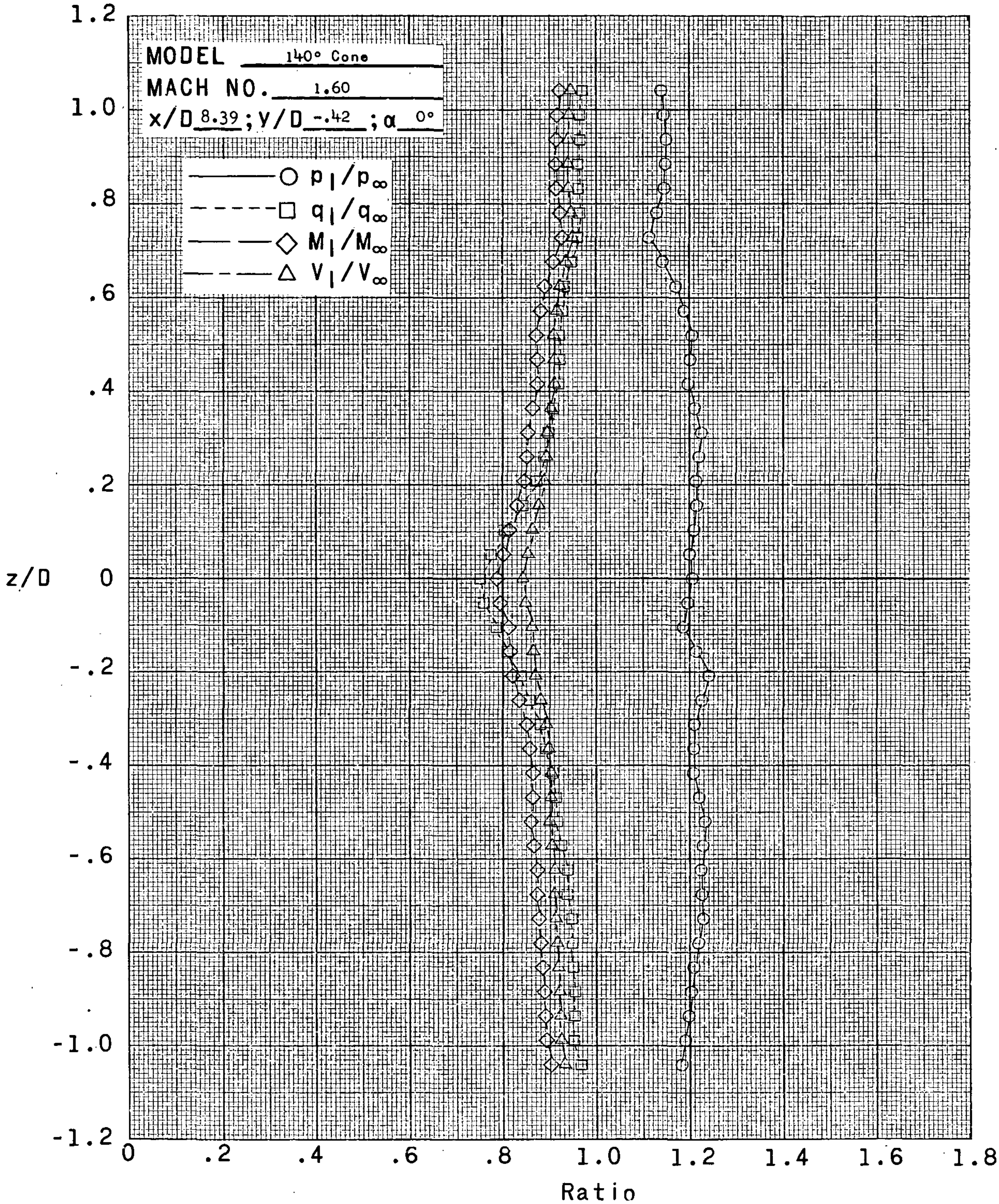
(jj) $x/D = 8.39$; $y/D = 0.21$; $\alpha = 0^0$.

Figure 5.- Continued.



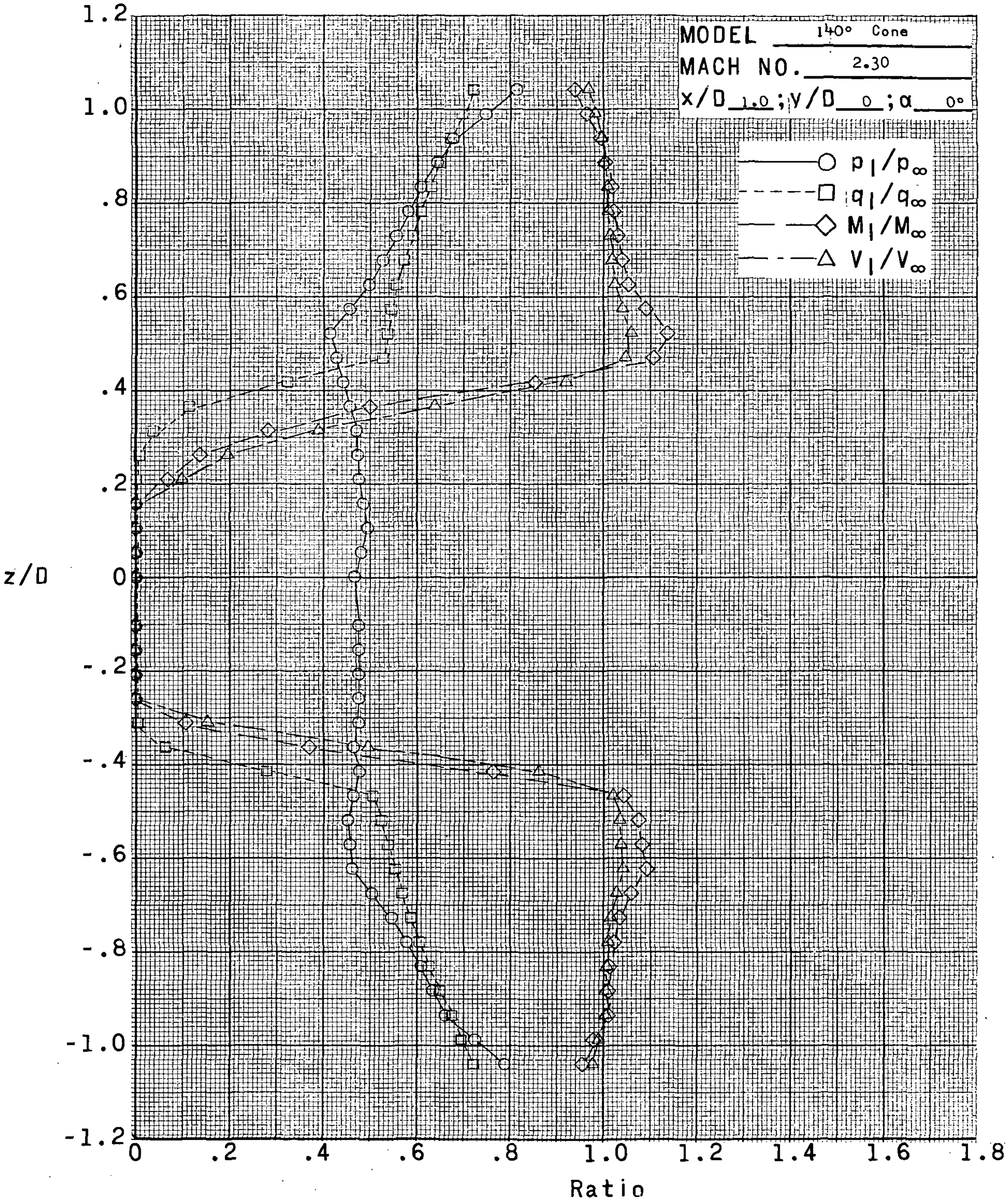
(kk) $x/D = 8.39$; $y/D = 0$; $\alpha = 0^o$.

Figure 5.- Continued.



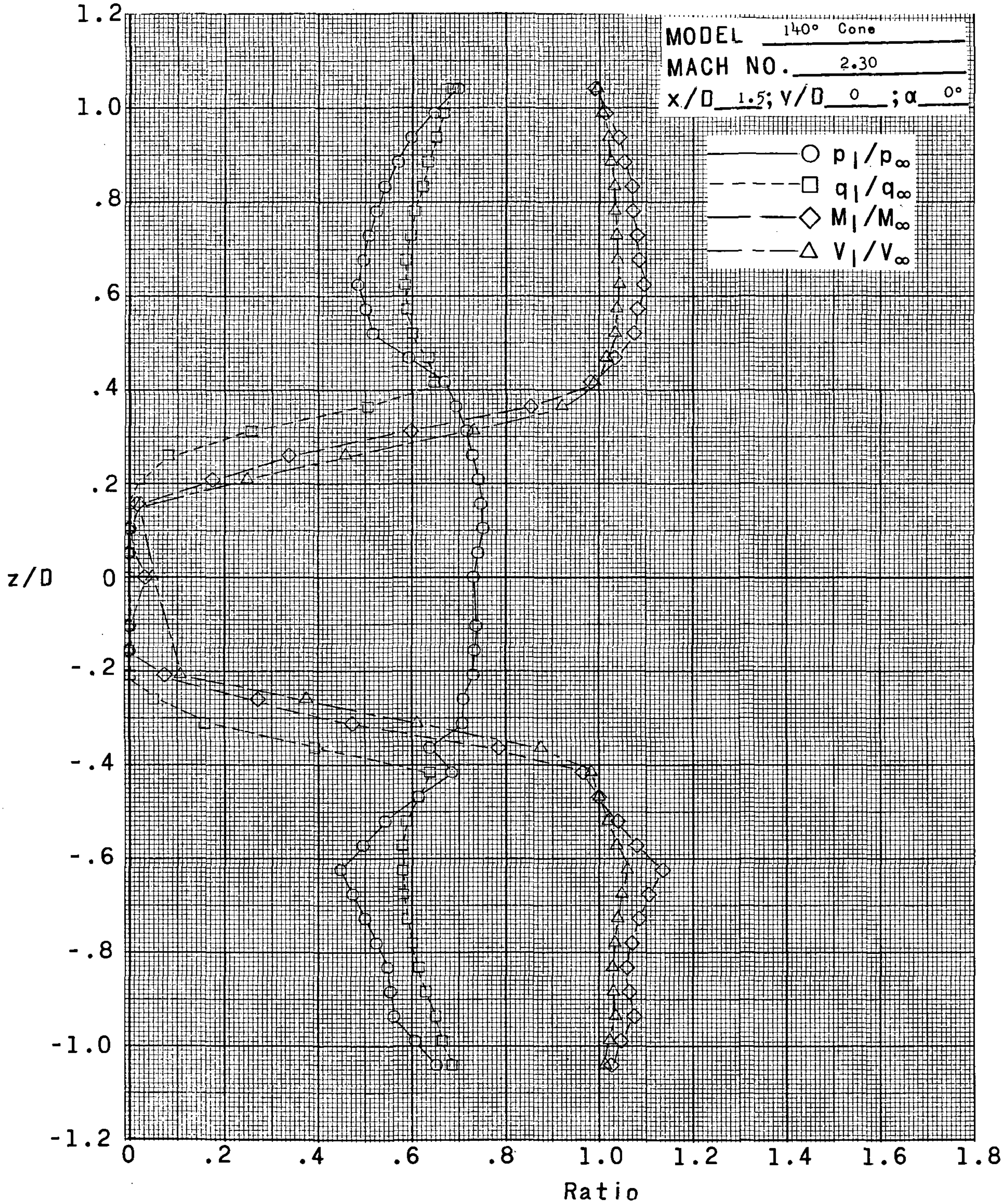
(ll) x/D = 8.39; y/D = -0.42; α = 0°.

Figure 5.- Concluded.



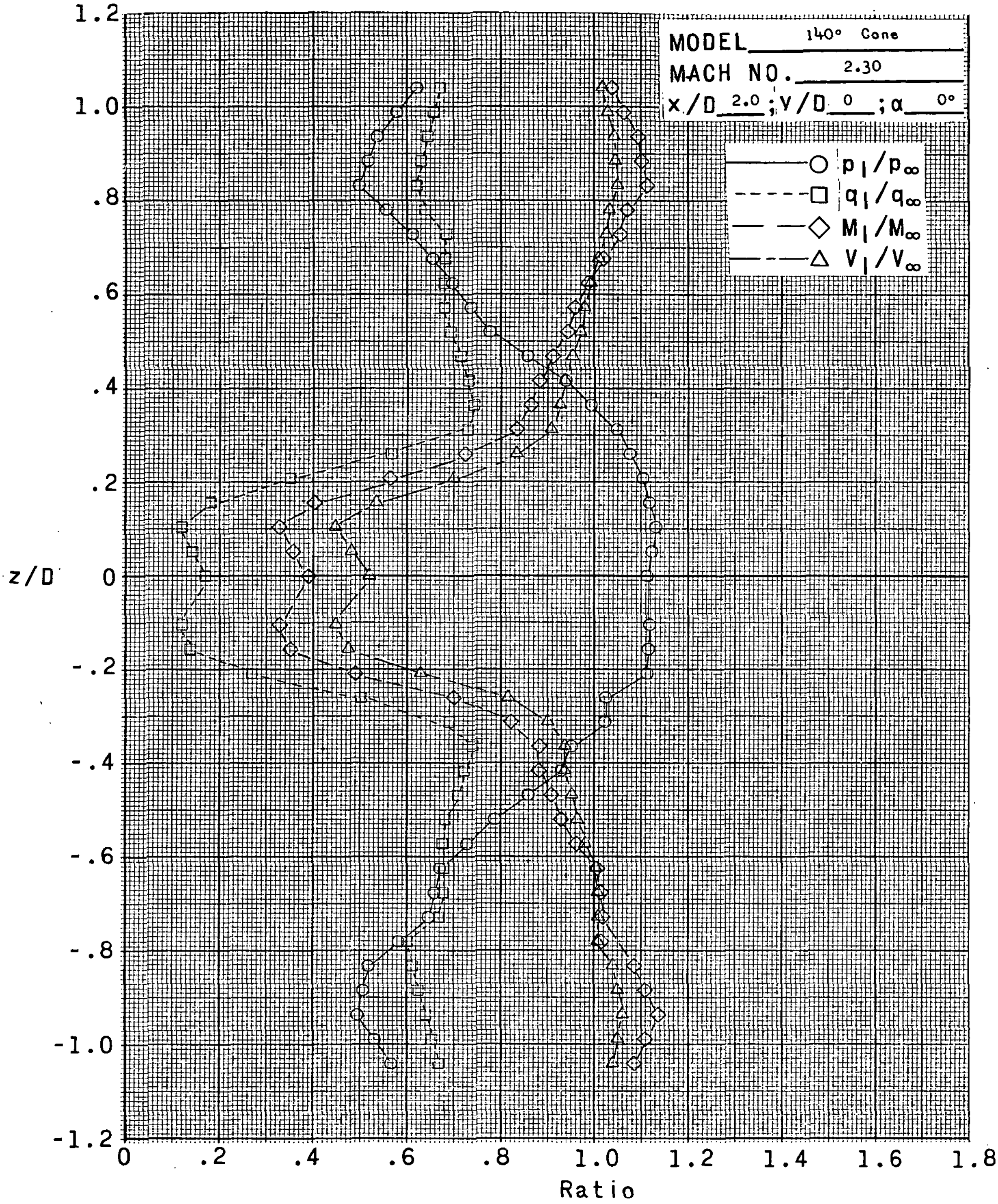
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 6.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D in wake of 140^0-included-angle cone at Mach number of 2.30 and Reynolds number of 5.42×10^6 per meter (1.65×10^6 per foot).



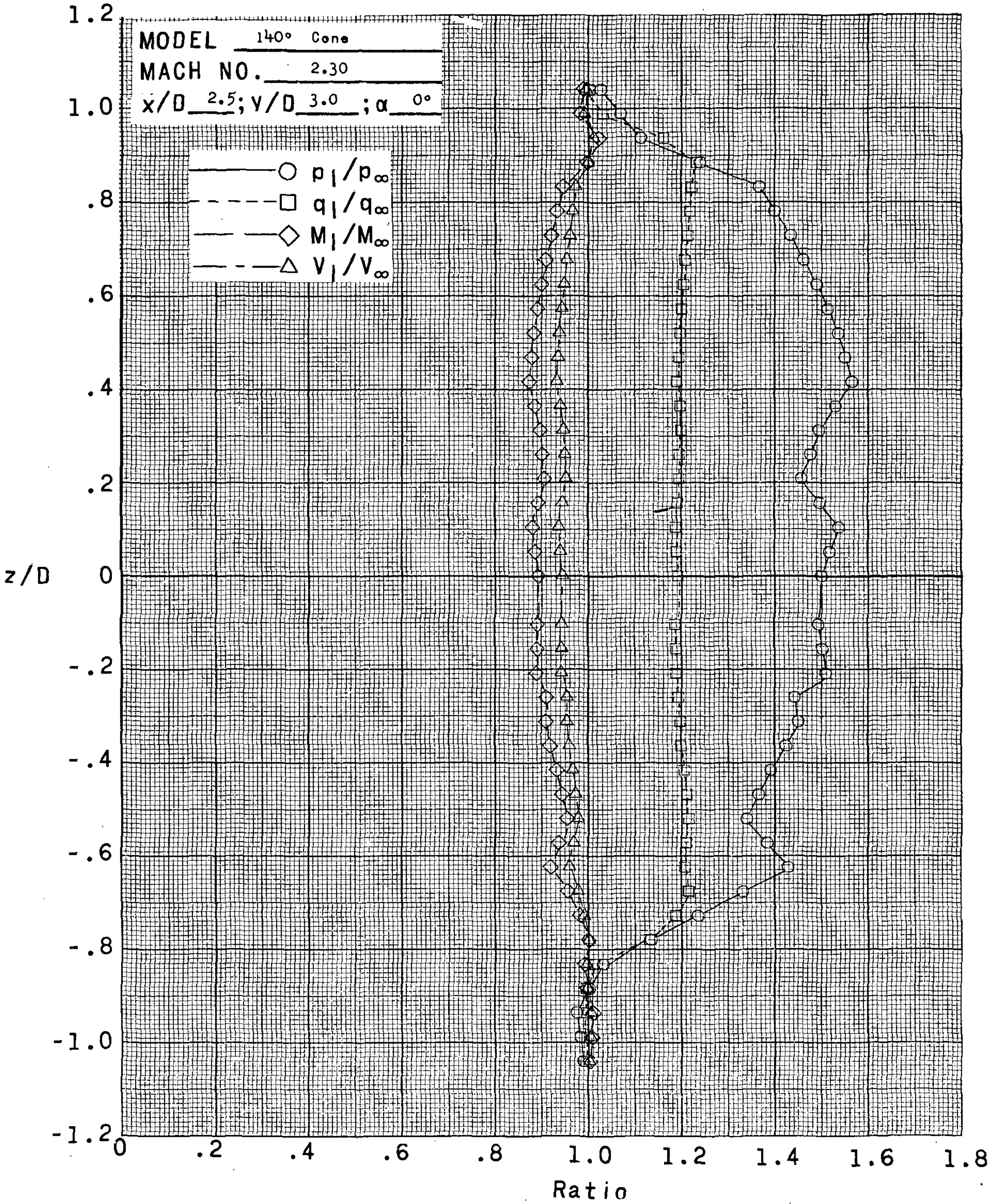
(b) x/D = 1.5; y/D = 0; α = 0°.

Figure 6.- Continued.



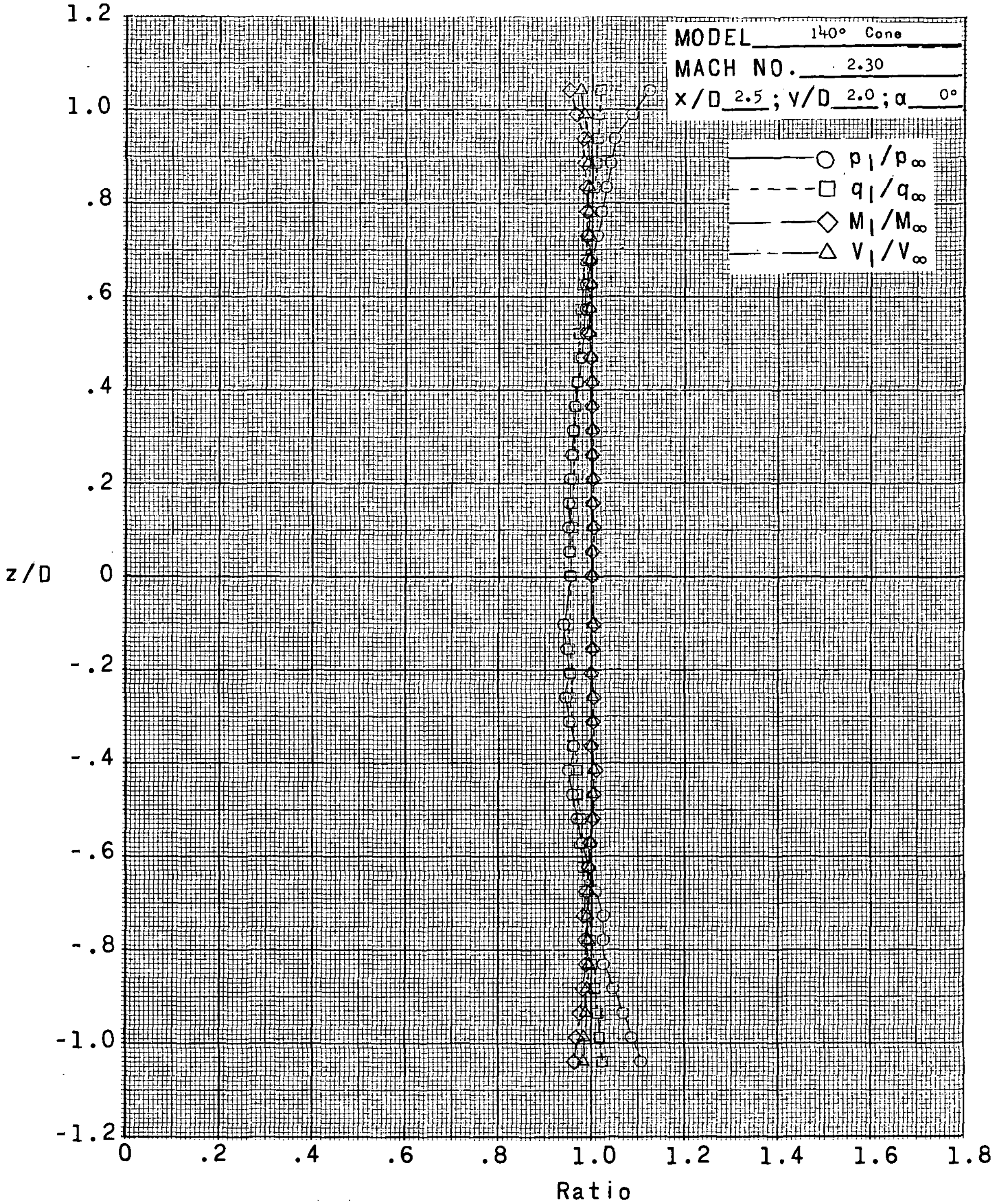
(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 6.- Continued.



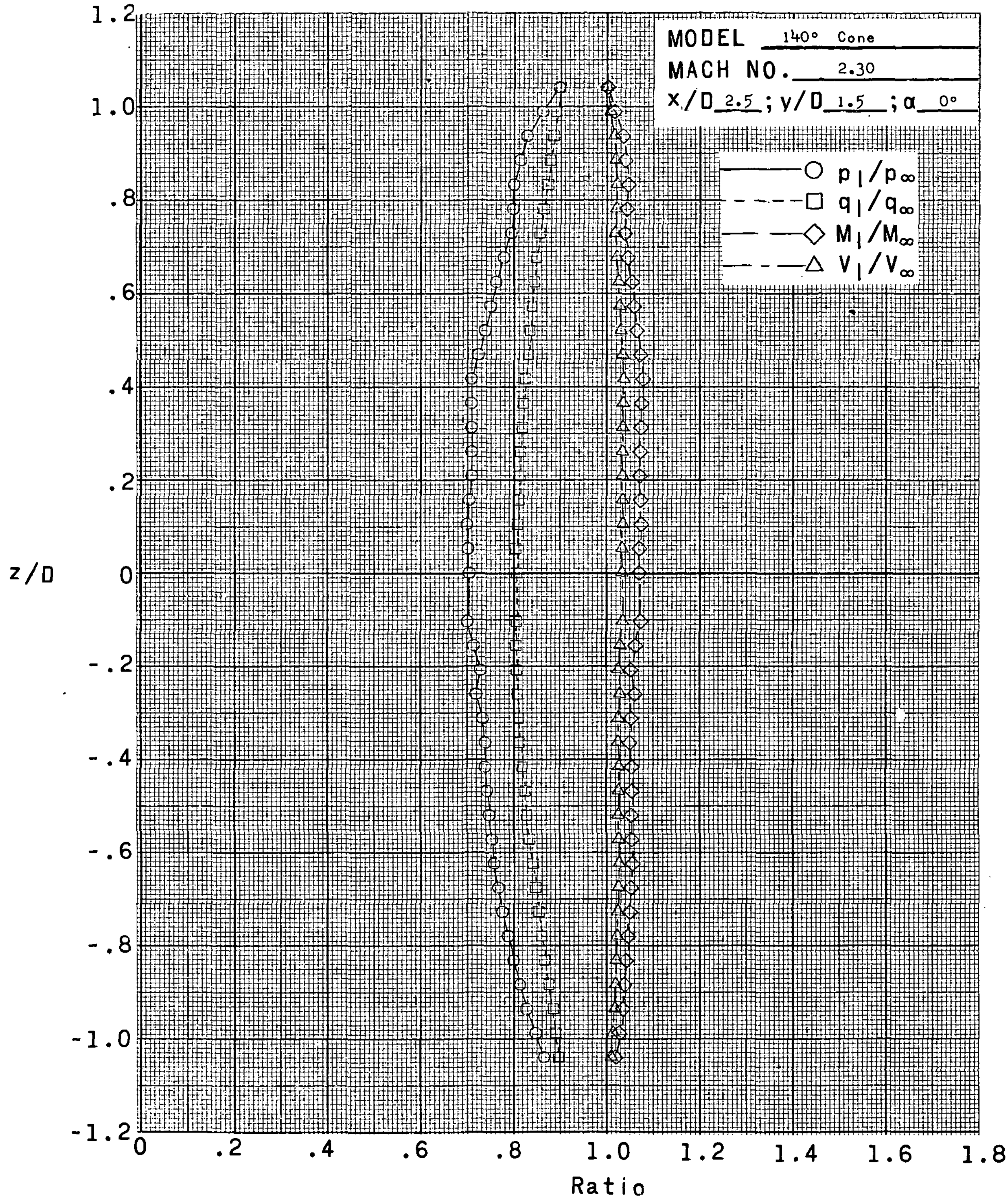
(d) $x/D = 2.5$; $y/D = 3.0$; $\alpha = 0^{\circ}$.

Figure 6.- Continued.



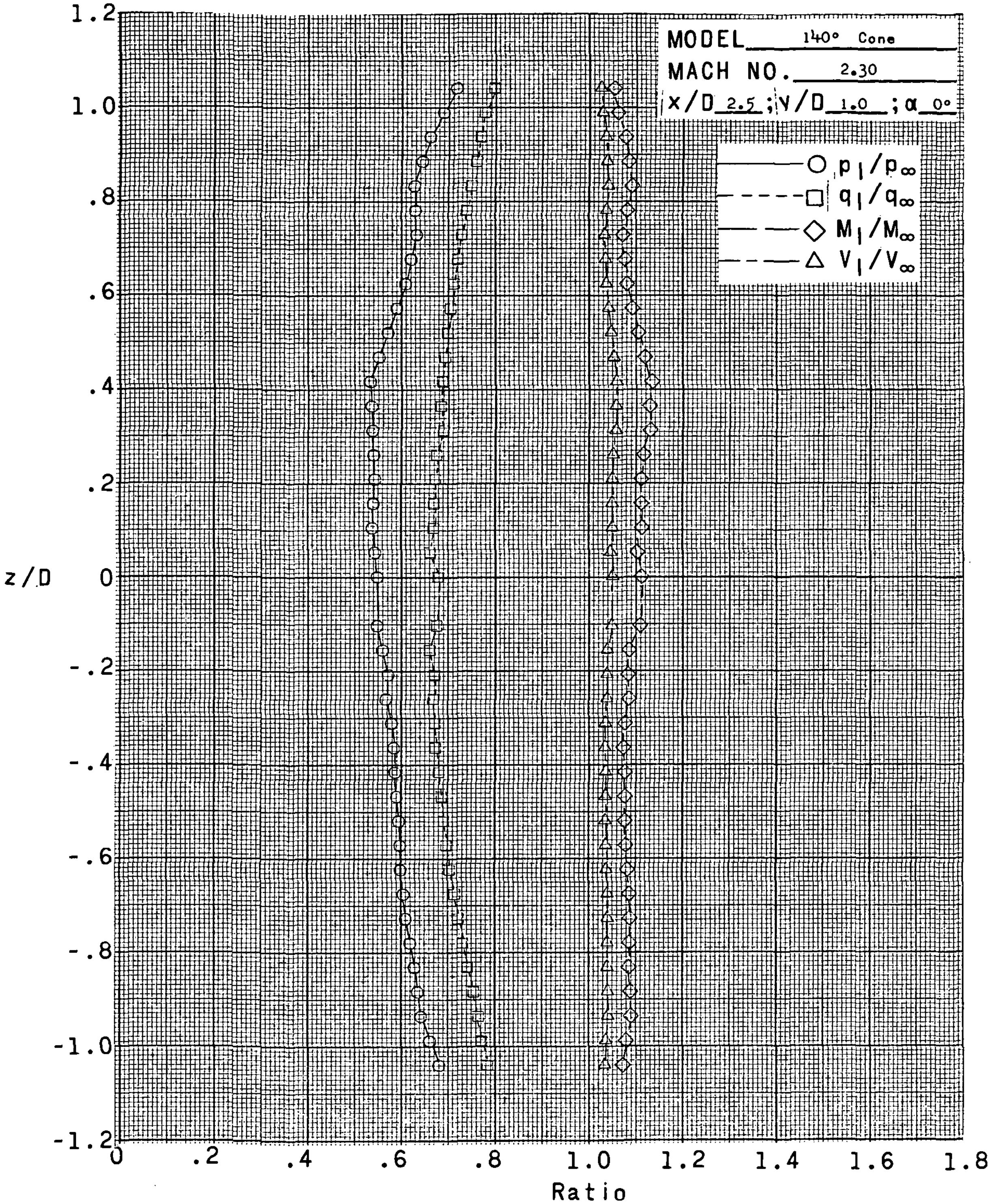
(e) x/D = 2.5; y/D = 2.0; α = 0°.

Figure 6.- Continued.



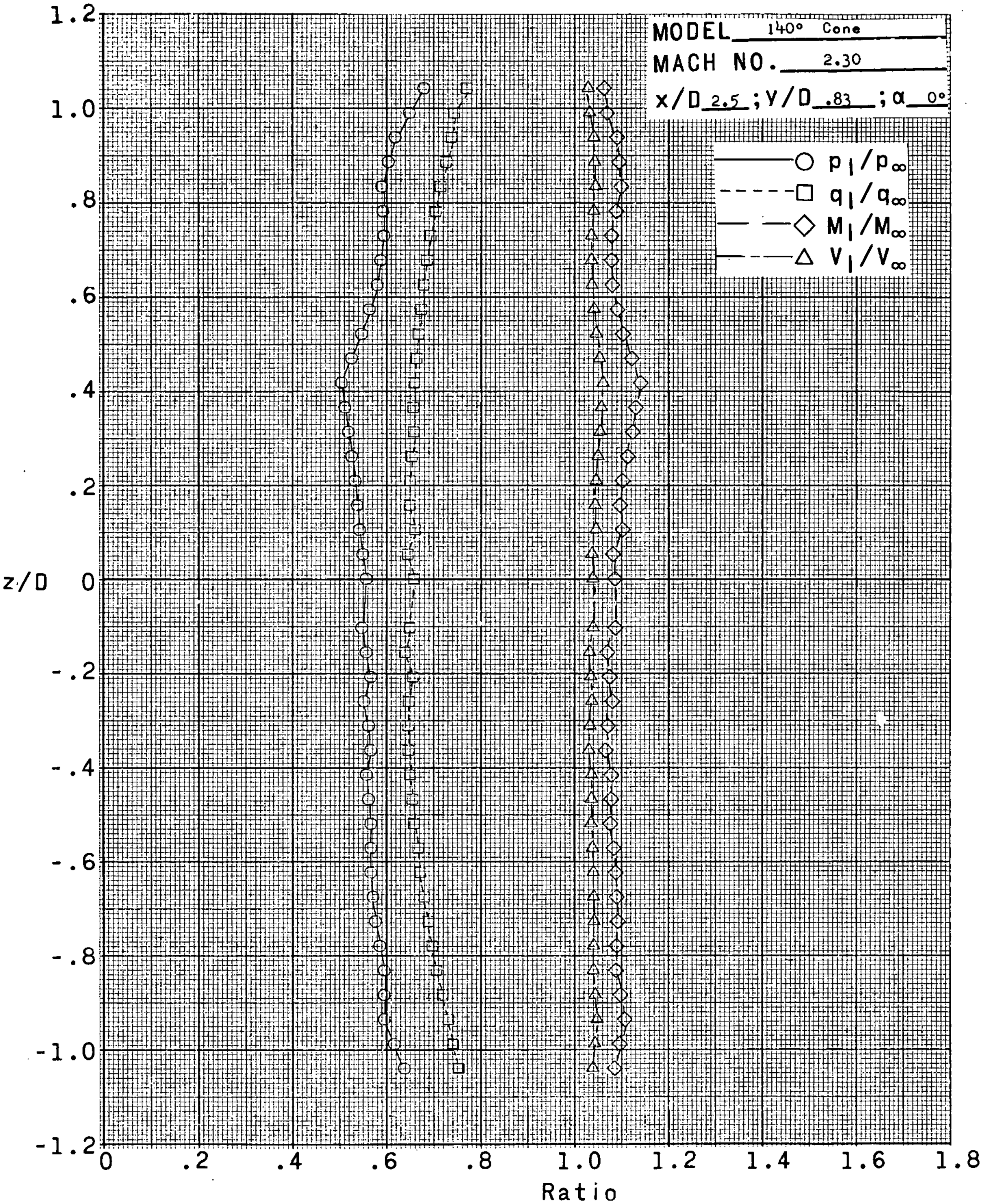
(f) x/D = 2.5; y/D = 1.5; α = 0°.

Figure 6.- Continued.



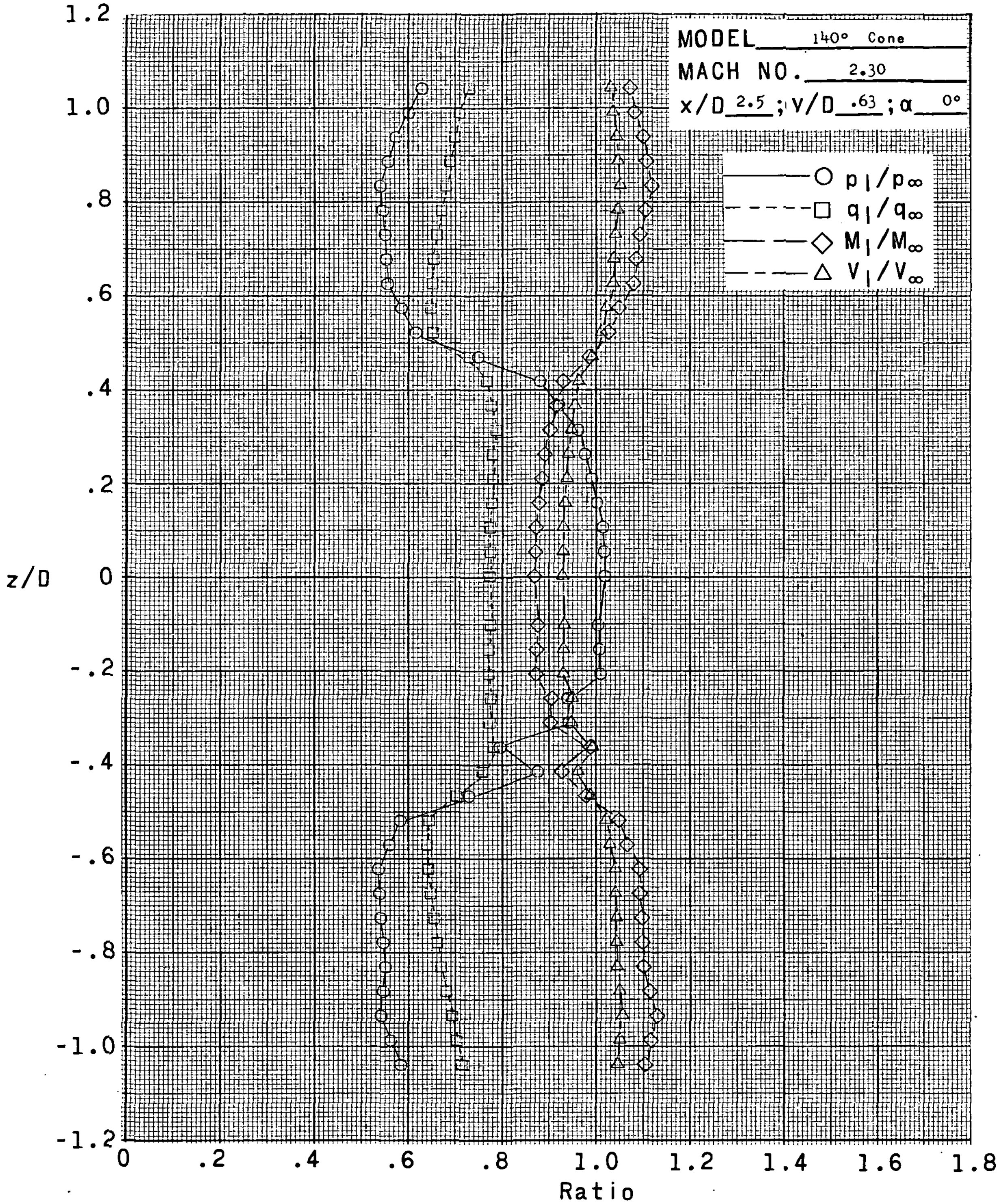
(g) x/D = 2.5; y/D = 1.0; α = 0°.

Figure 6.- Continued.



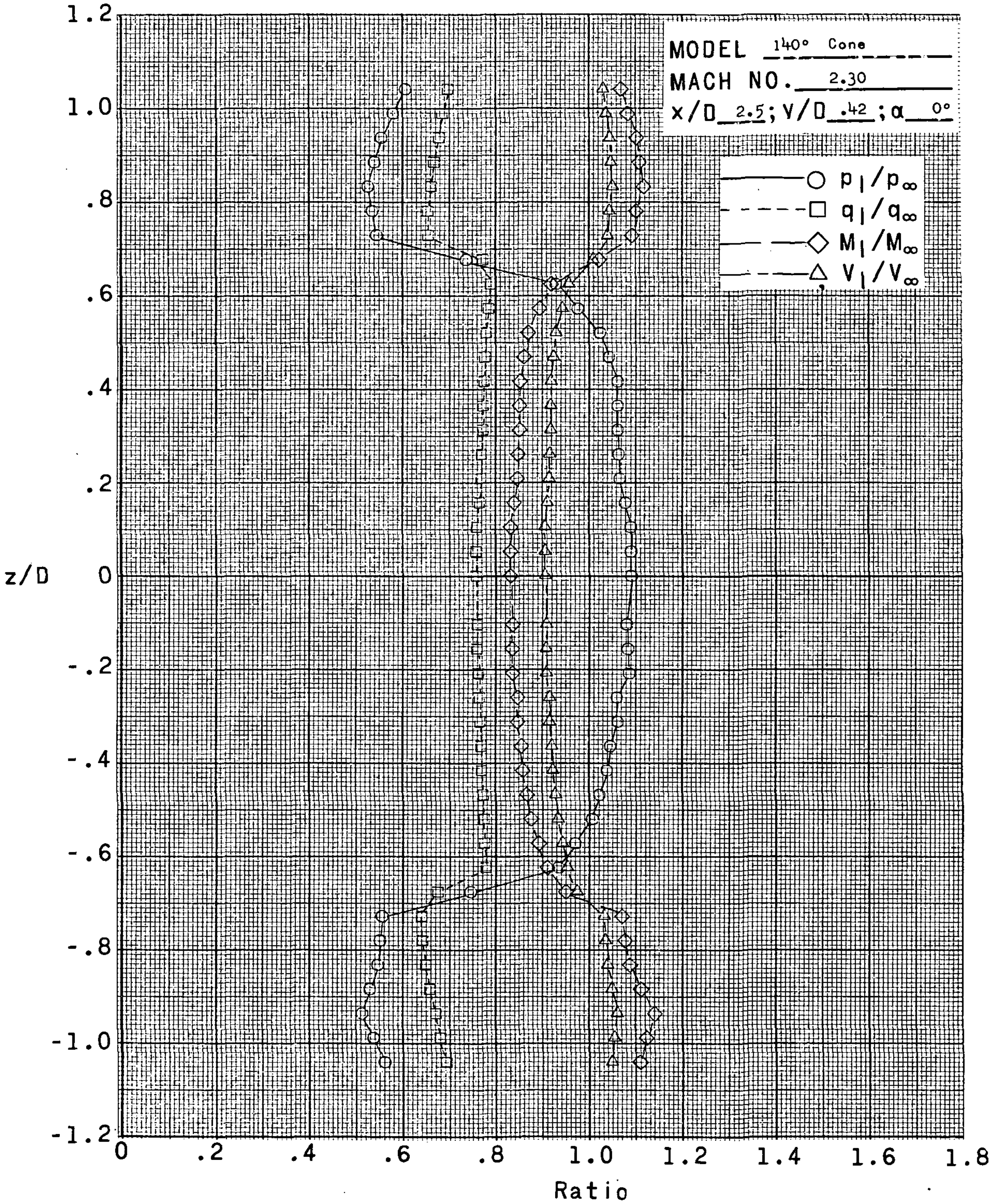
(h) $x/D = 2.5$; $y/D = 0.83$; $\alpha = 0^0$.

Figure 6.- Continued.



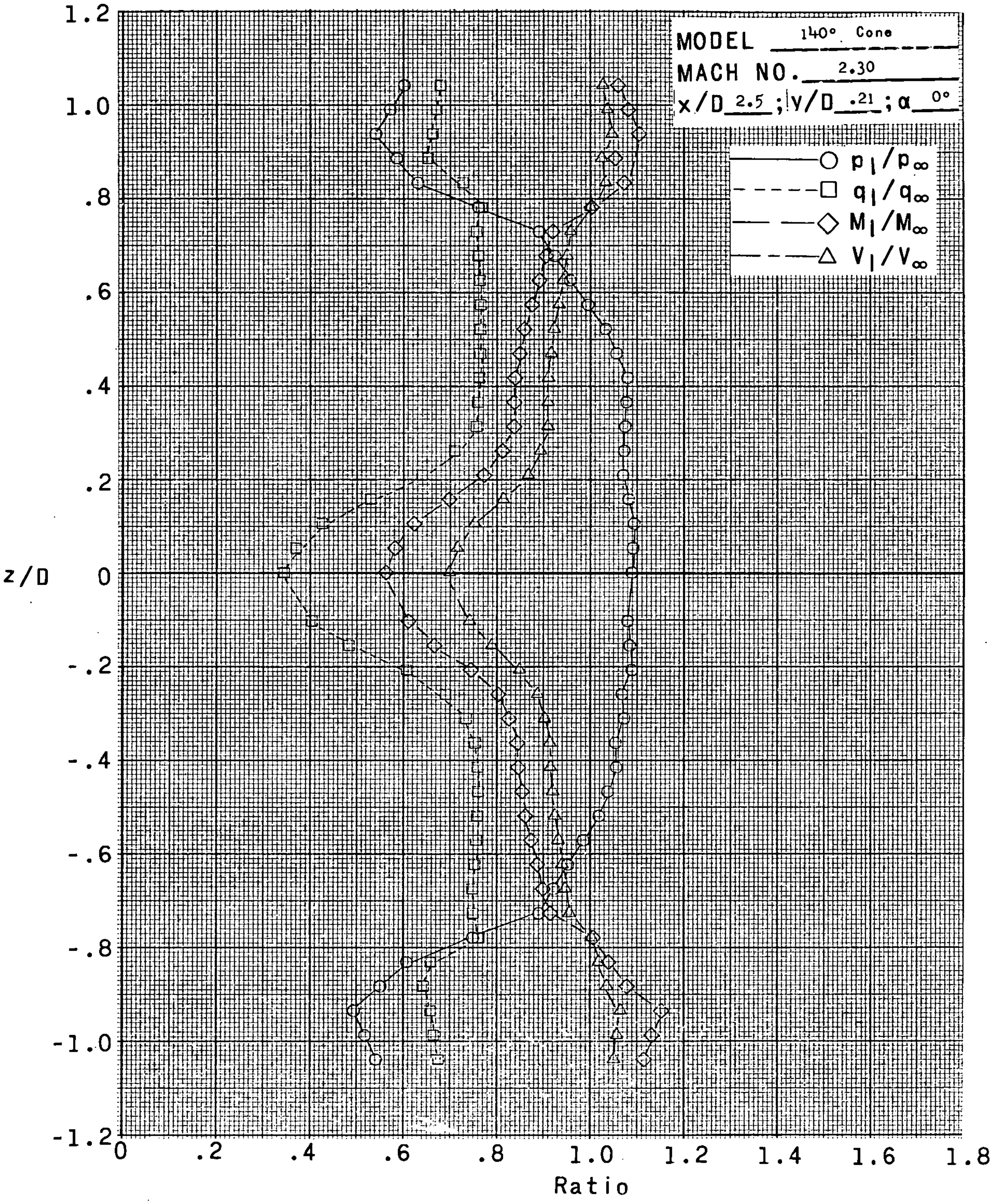
(i) $x/D = 2.5$; $y/D = 0.63$; $\alpha = 0^{0}$.

Figure 6.- Continued.



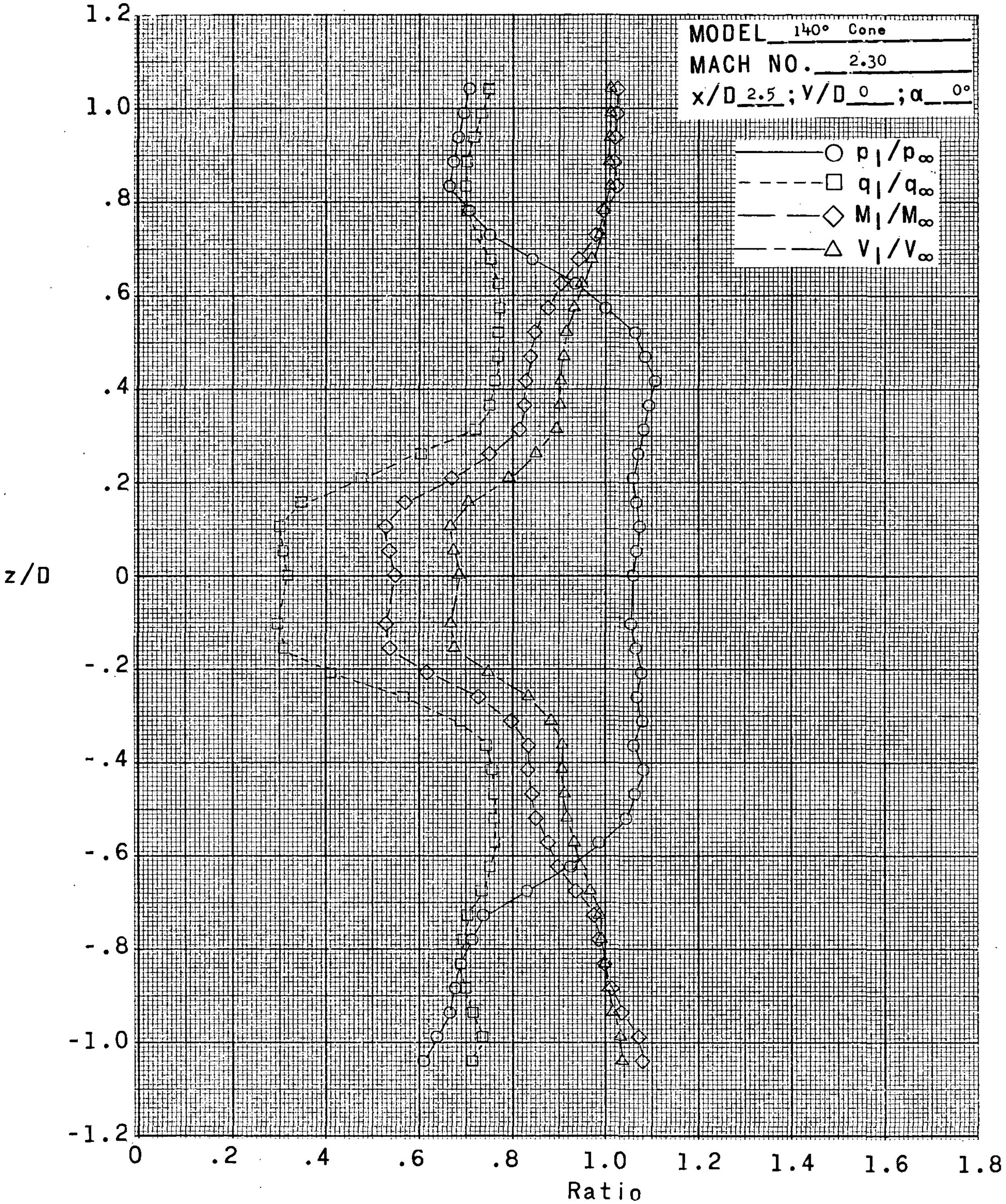
(j) $x/D = 2.5$; $y/D = 0.42$; $\alpha = 0^0$.

Figure 6.- Continued.



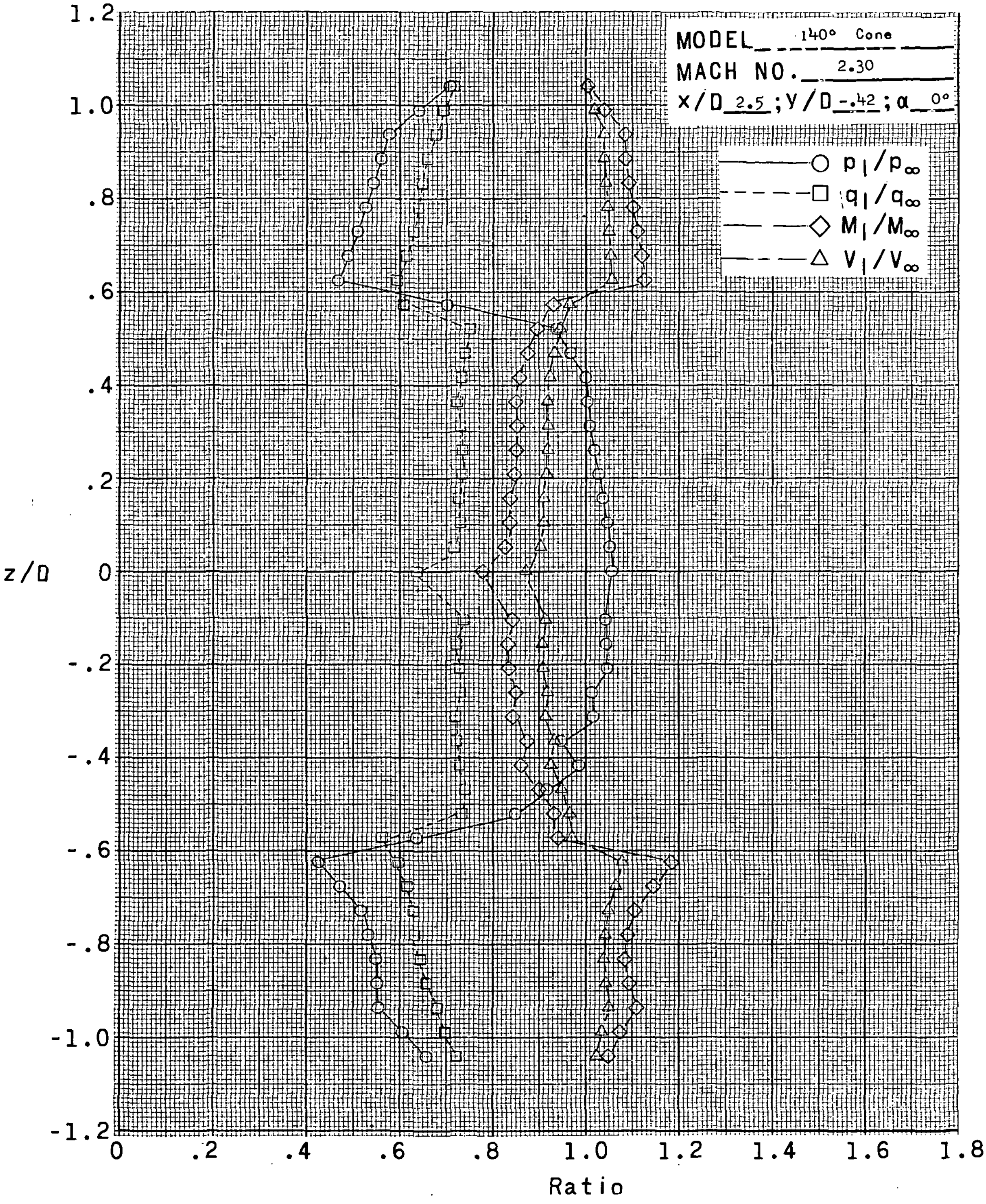
(k) $x/D = 2.5$; $y/D = 0.21$; $\alpha = 0^{0}$.

Figure 6.- Continued.



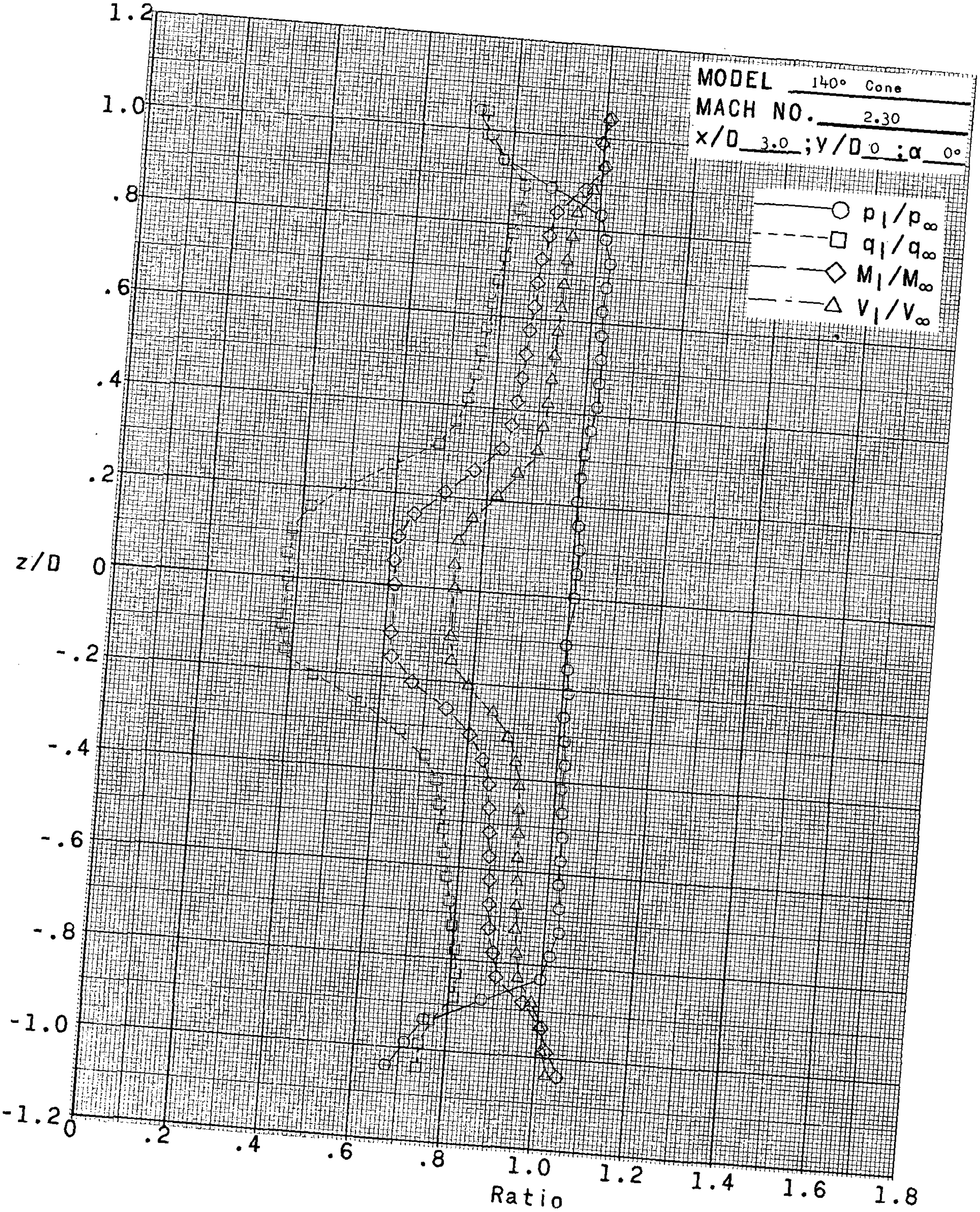
(l) $x/D = 2.5$; $y/D = 0$; $\alpha = 0^0$.

Figure 6.- Continued.



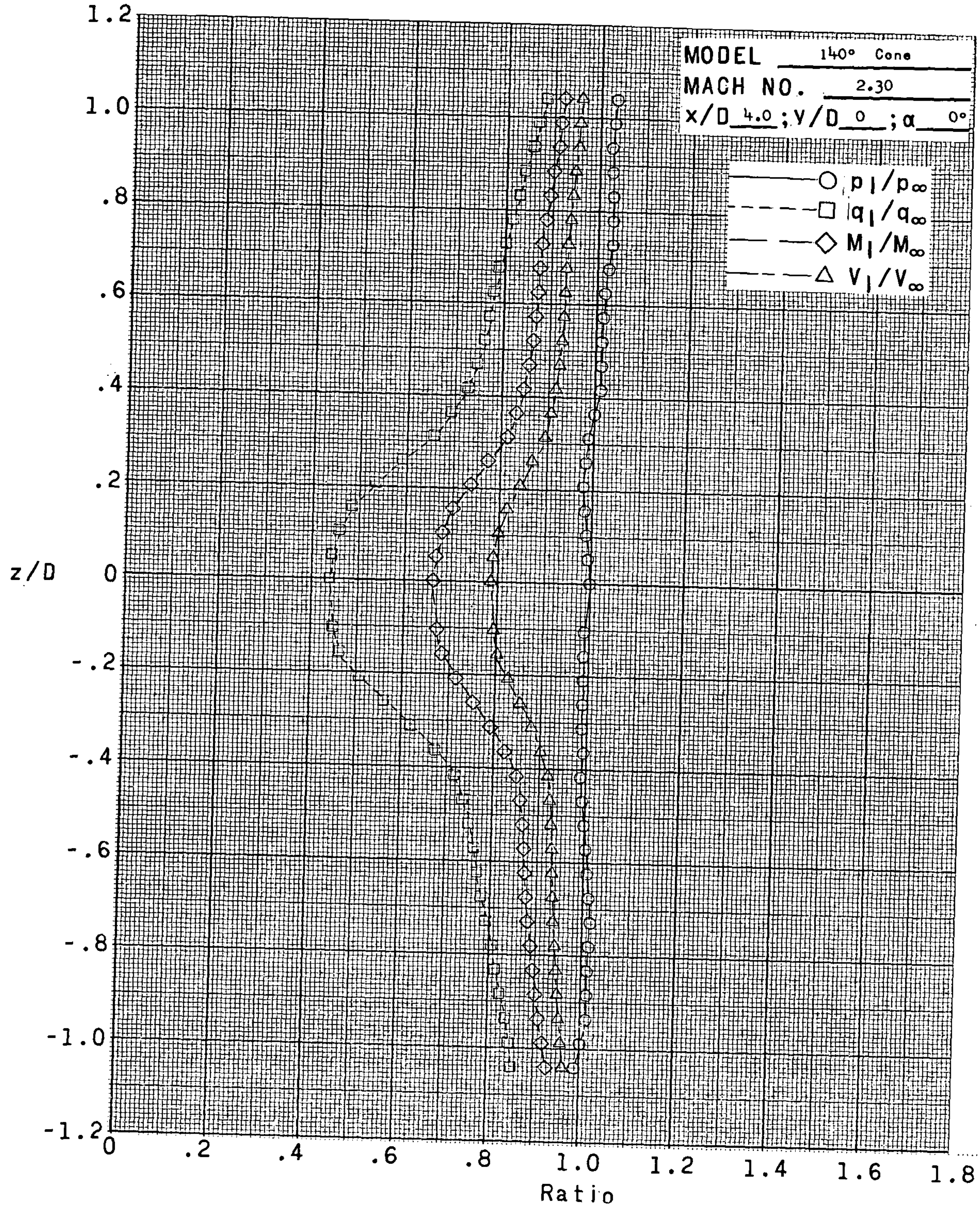
(m) x/D = 2.5; y/D = -0.42; α = 0°.

Figure 6.- Continued.



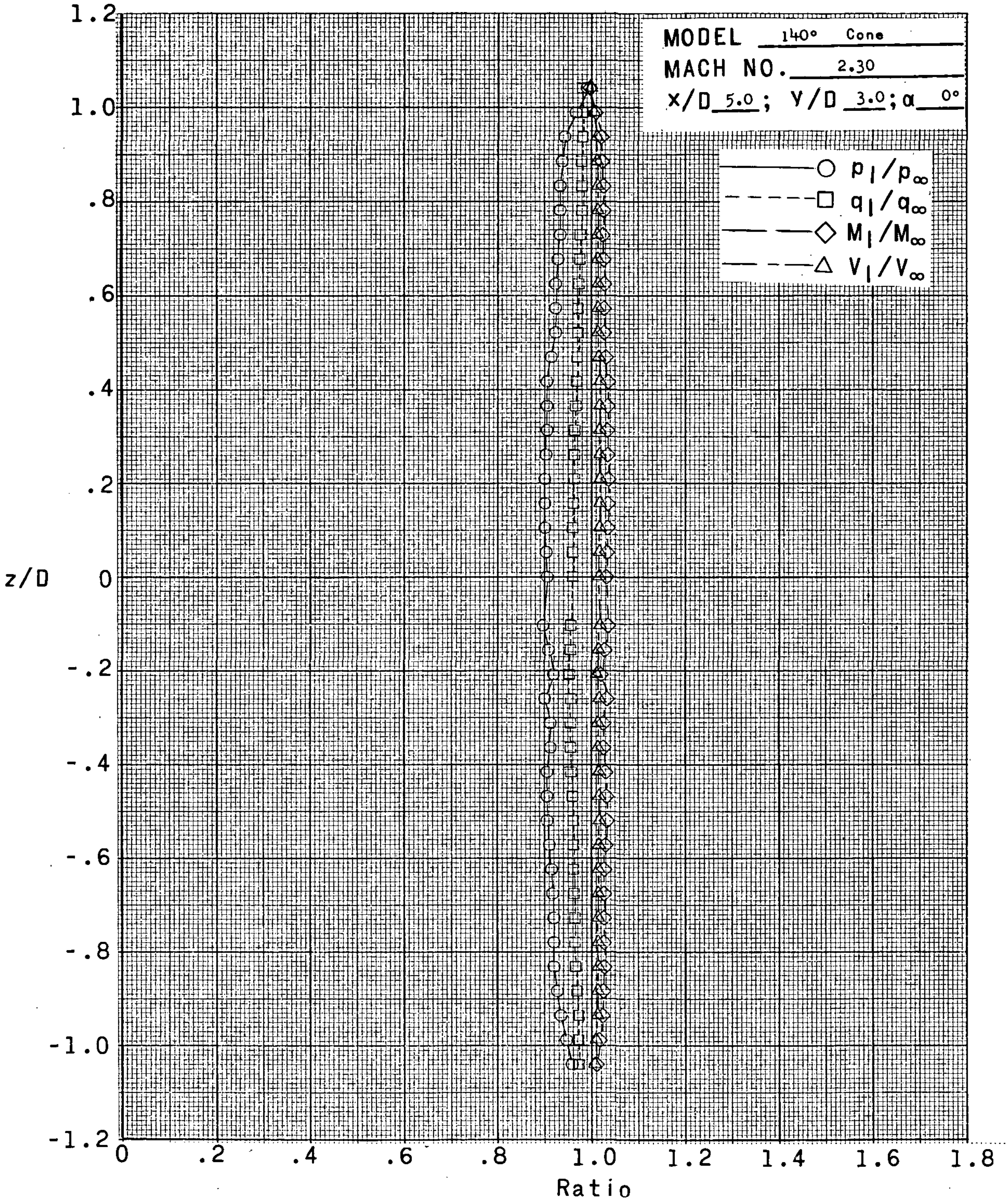
(n) x/D = 3.0; y/D = 0; α = 0°.

Figure 6.- Continued.



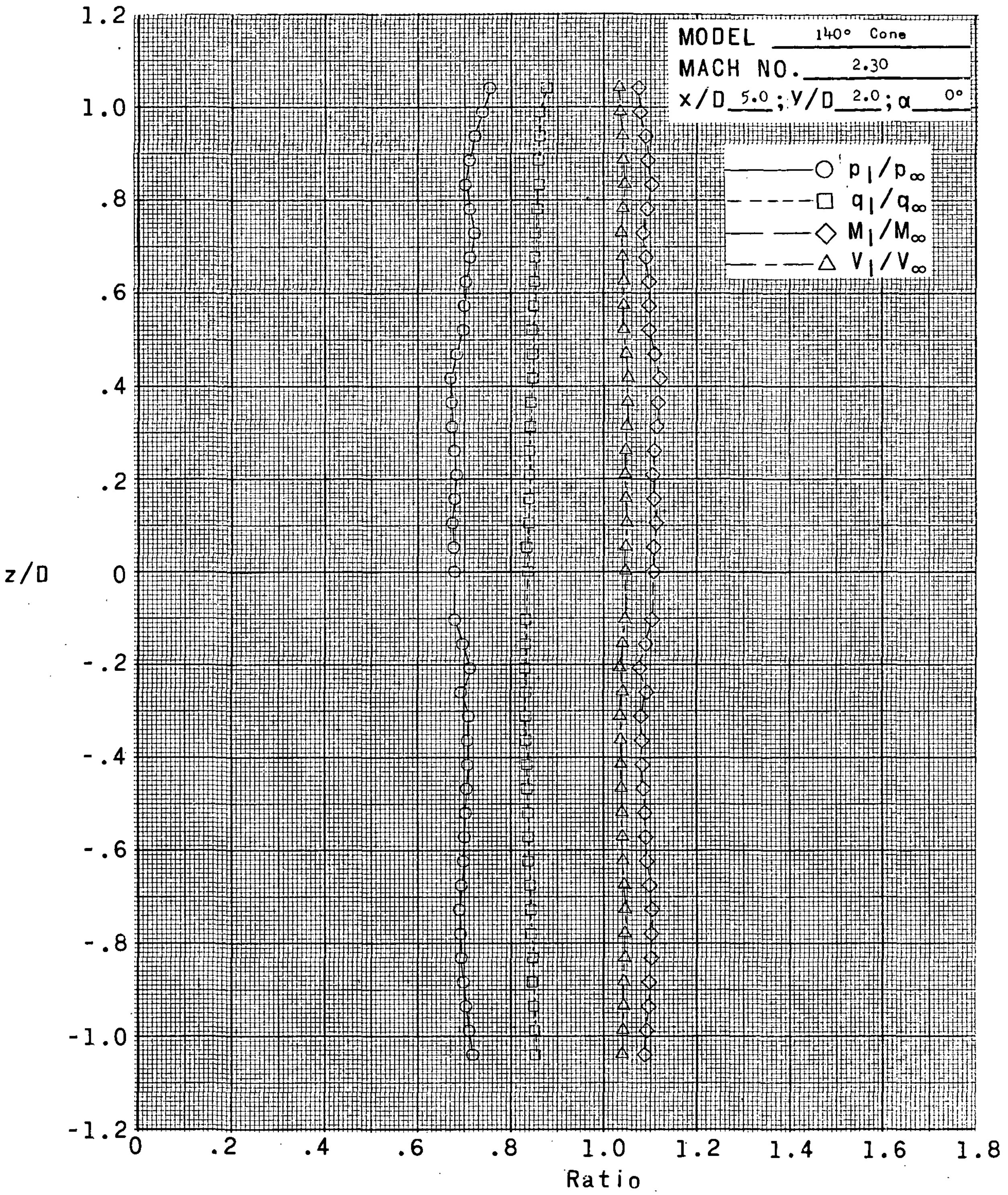
(o) $x/D = 4.0$; $y/D = 0$; $\alpha = 0^o$.

Figure 6.- Continued.



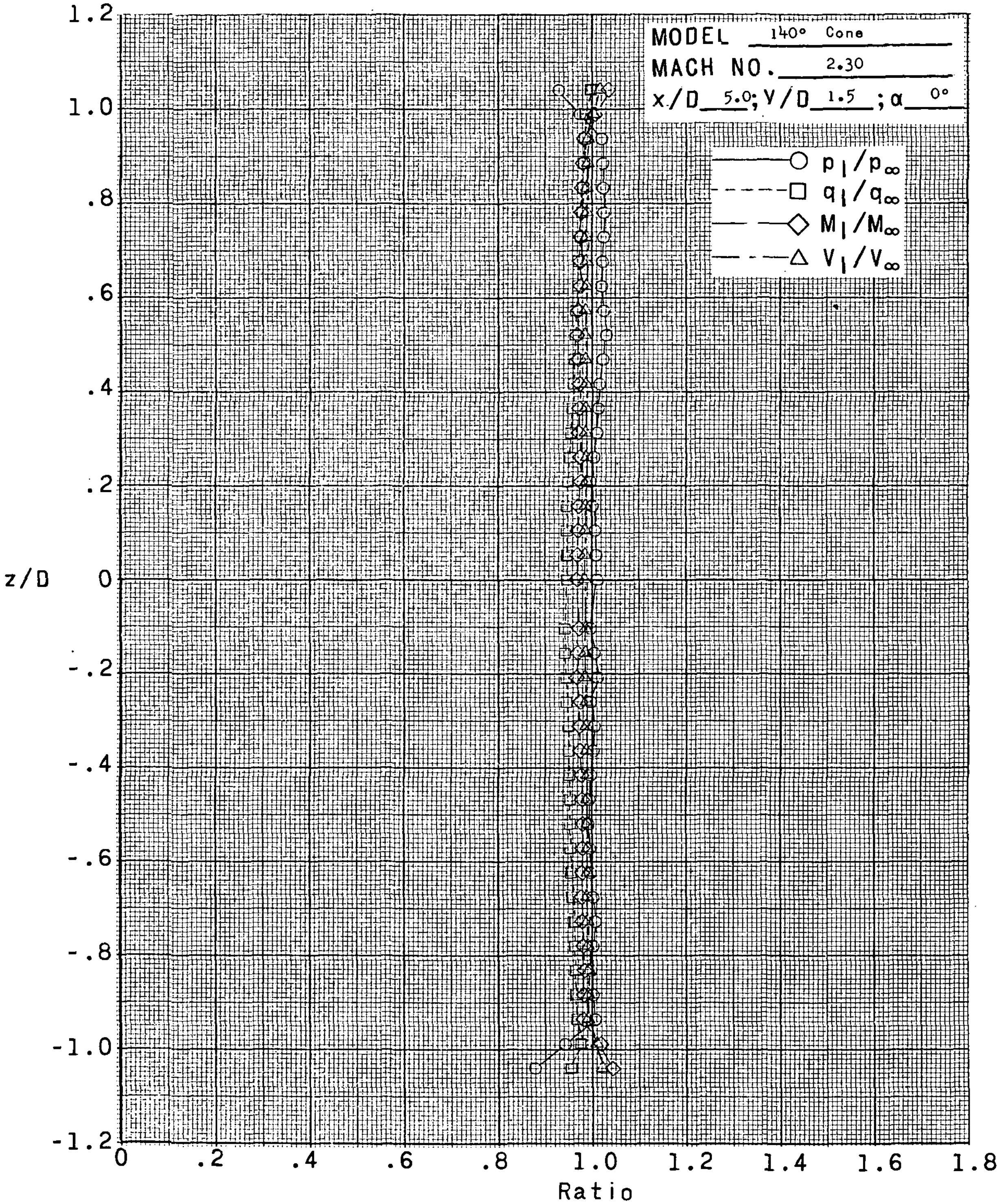
(p) $x/D = 5.0$; $y/D = 3.0$; $\alpha = 0^{\circ}$.

Figure 6.- Continued.



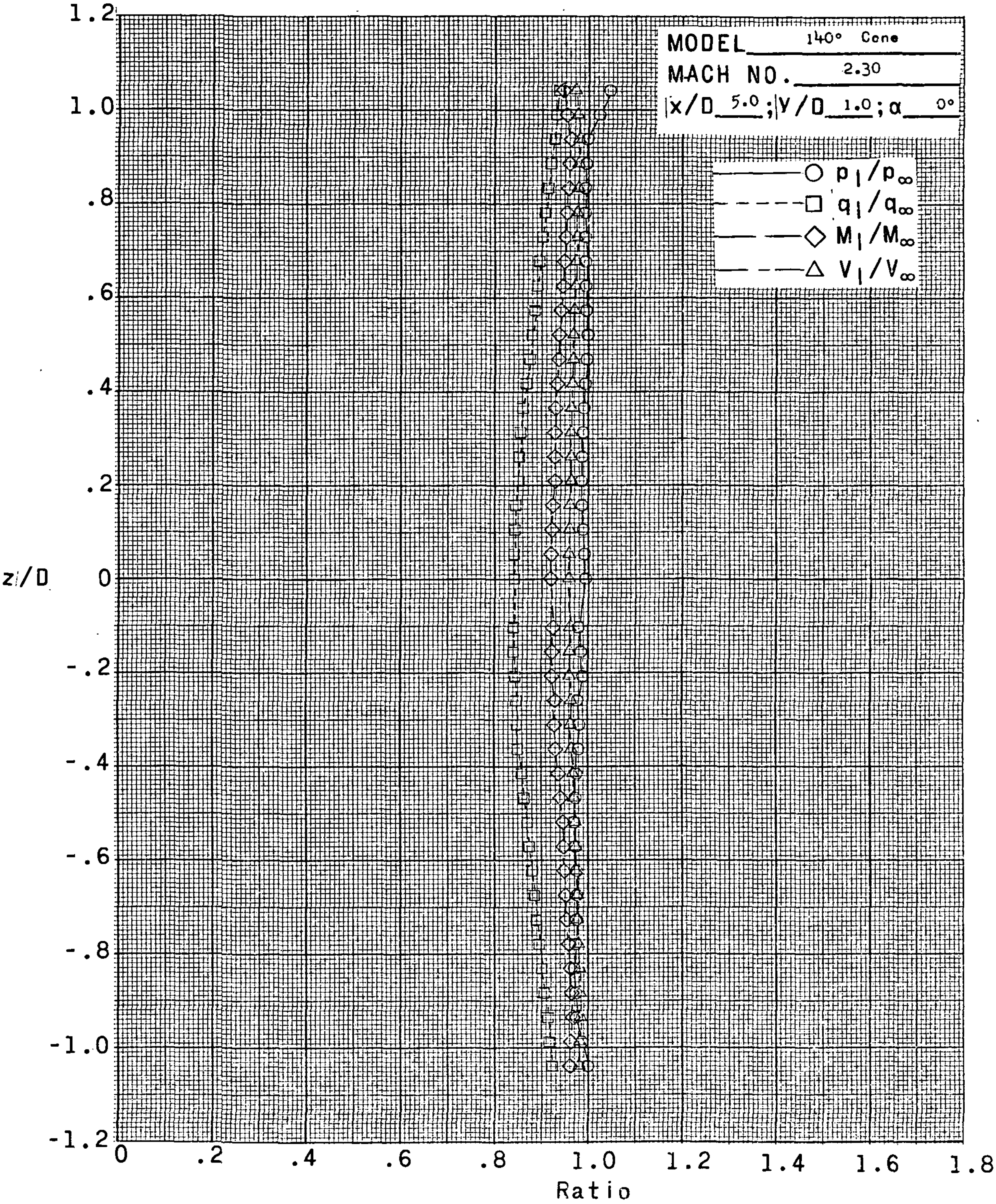
(q) $x/D = 5.0$; $y/D = 2.0$; $\alpha = 0^{0}$.

Figure 6.- Continued.



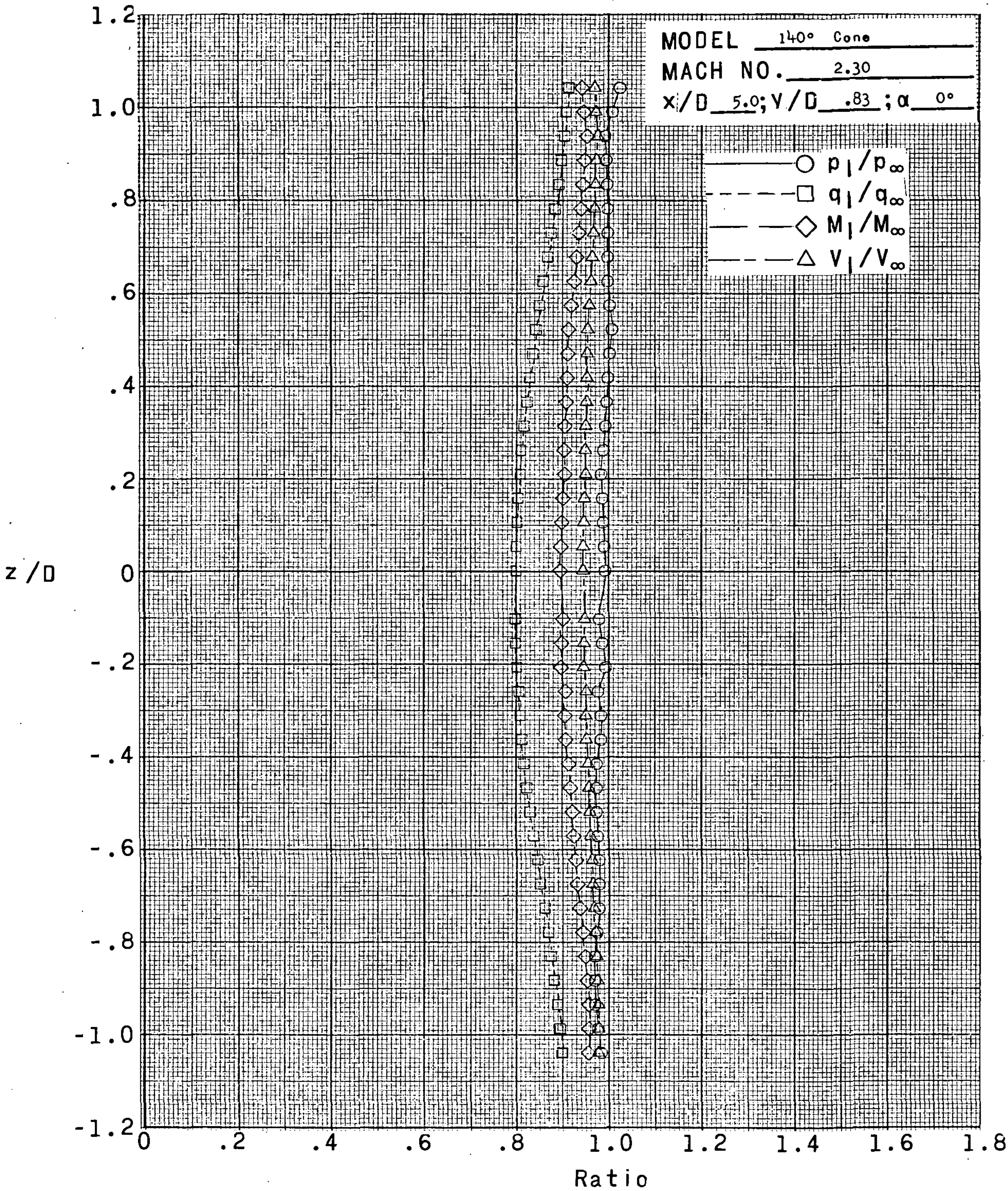
(r) $x/D = 5.0$; $y/D = 1.5$; $\alpha = 0^0$.

Figure 6.- Continued.



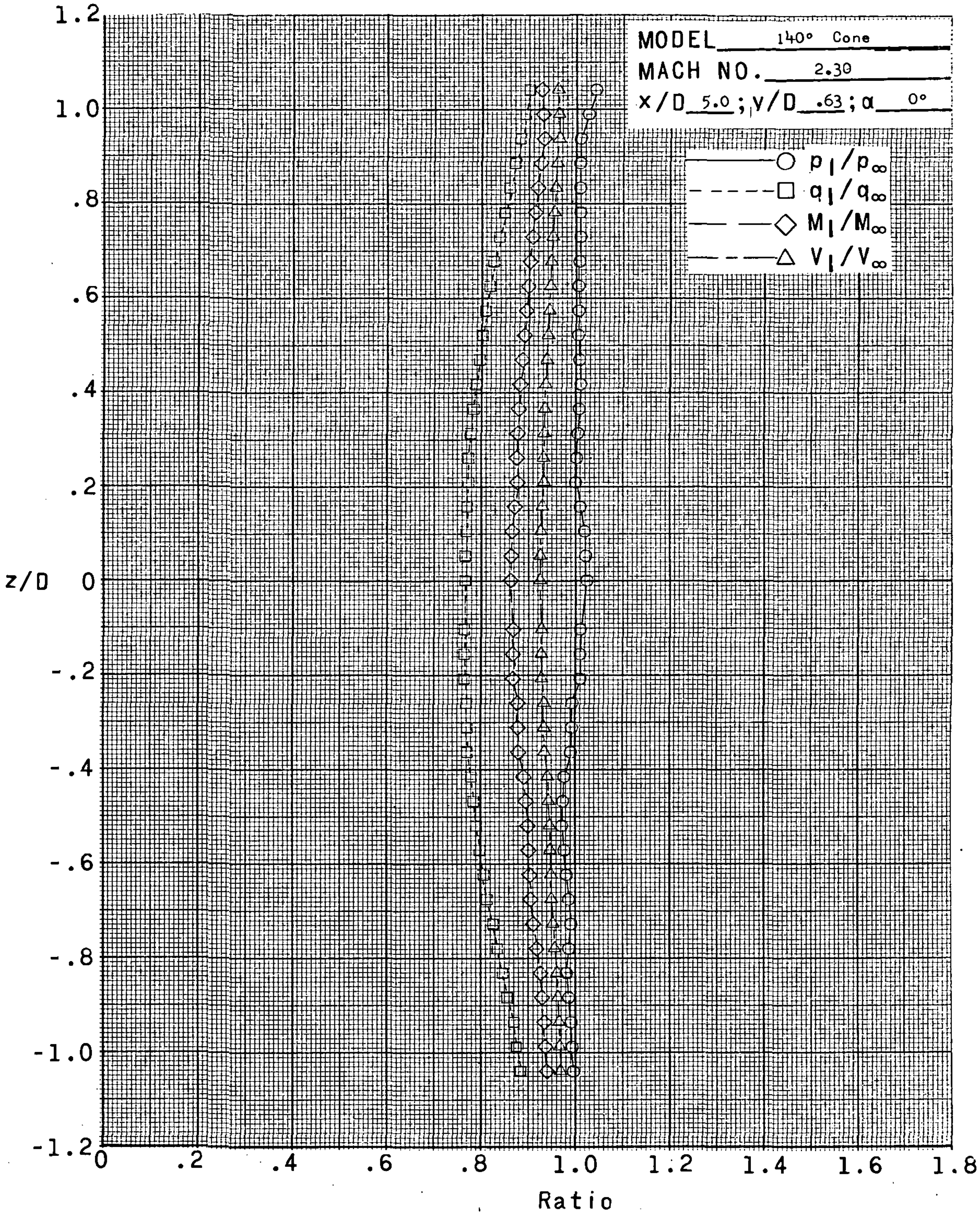
(s) $x/D = 5.0$; $y/D = 1.0$; $\alpha = 0^{\circ}$.

Figure 6.- Continued.



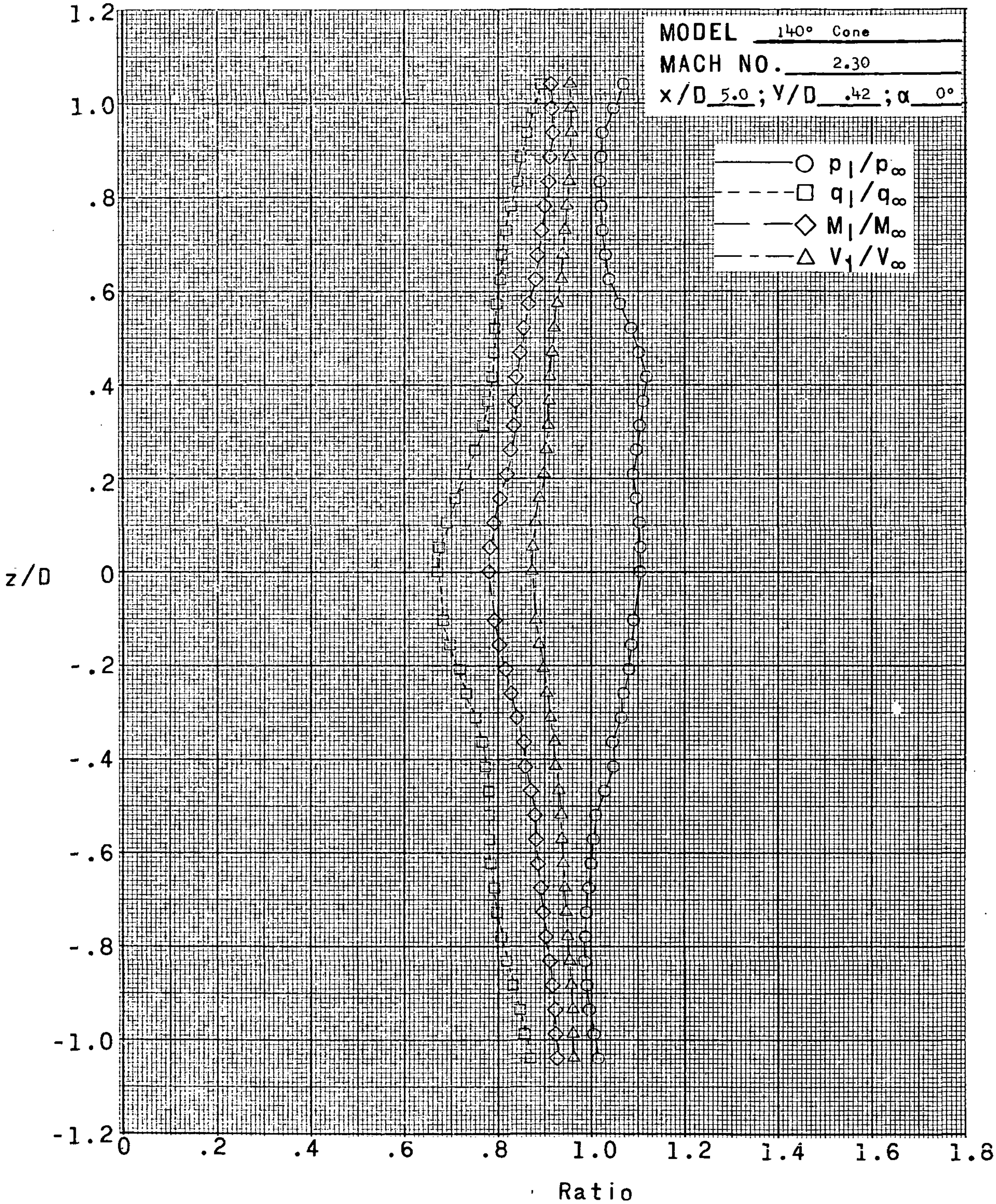
(t) $x/D = 5.0$; $y/D = 0.83$; $\alpha = 0^{\circ}$.

Figure 6.- Continued.



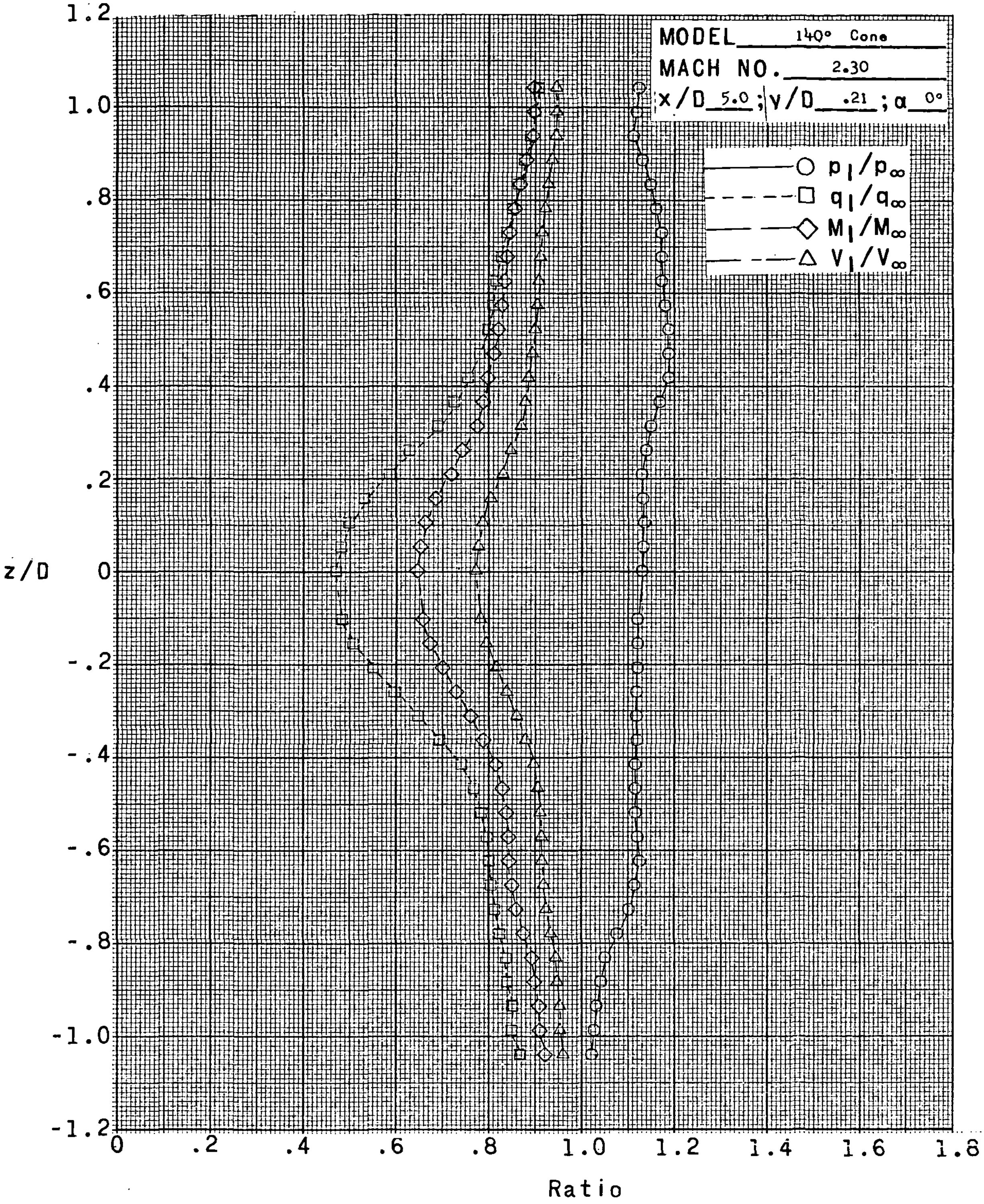
(u) x/D = 5.0; y/D = 0.63; α = 0°.

Figure 6.- Continued.



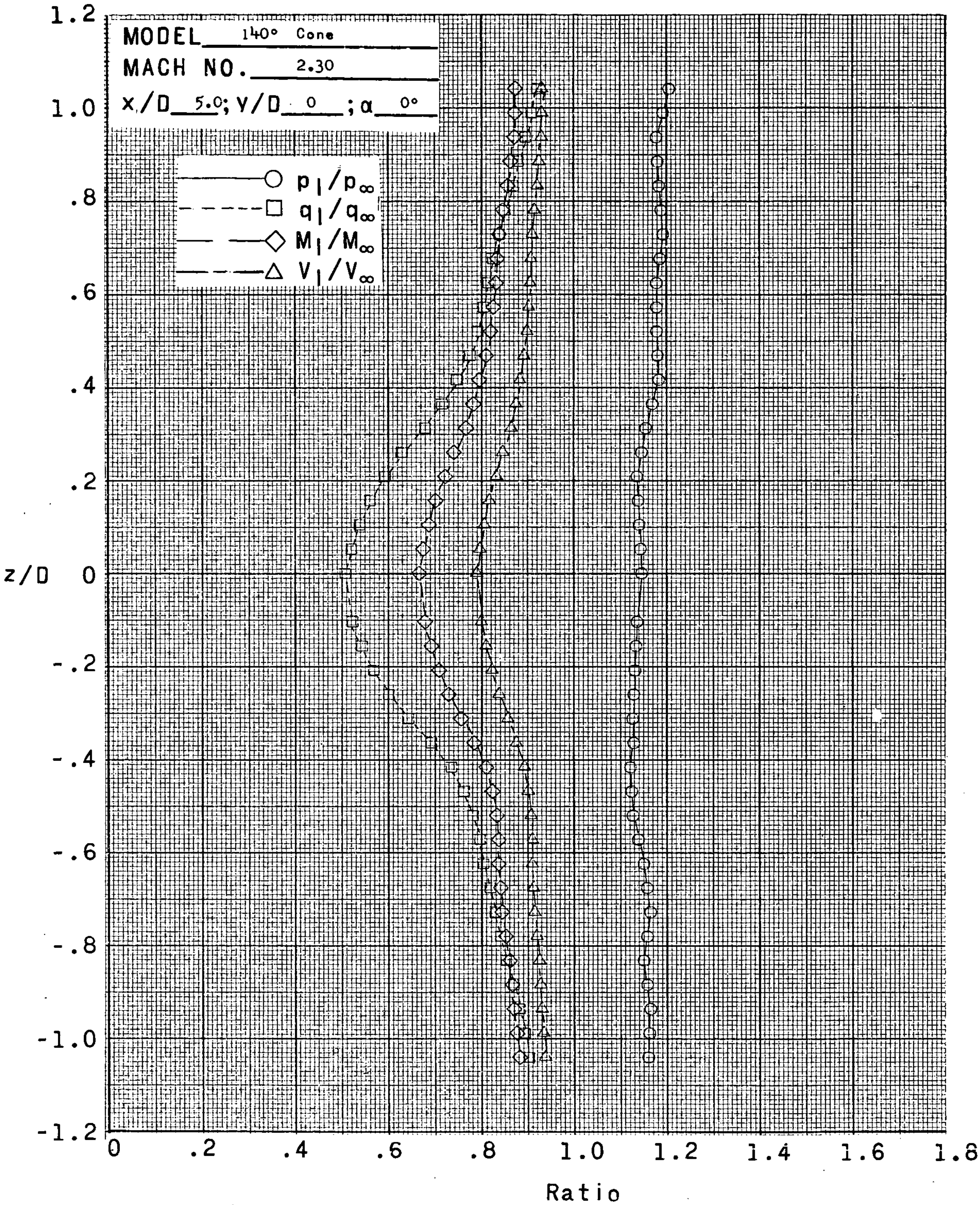
(v) x/D = 5.0; y/D = 0.42; α = 0°.

Figure 6.- Continued.



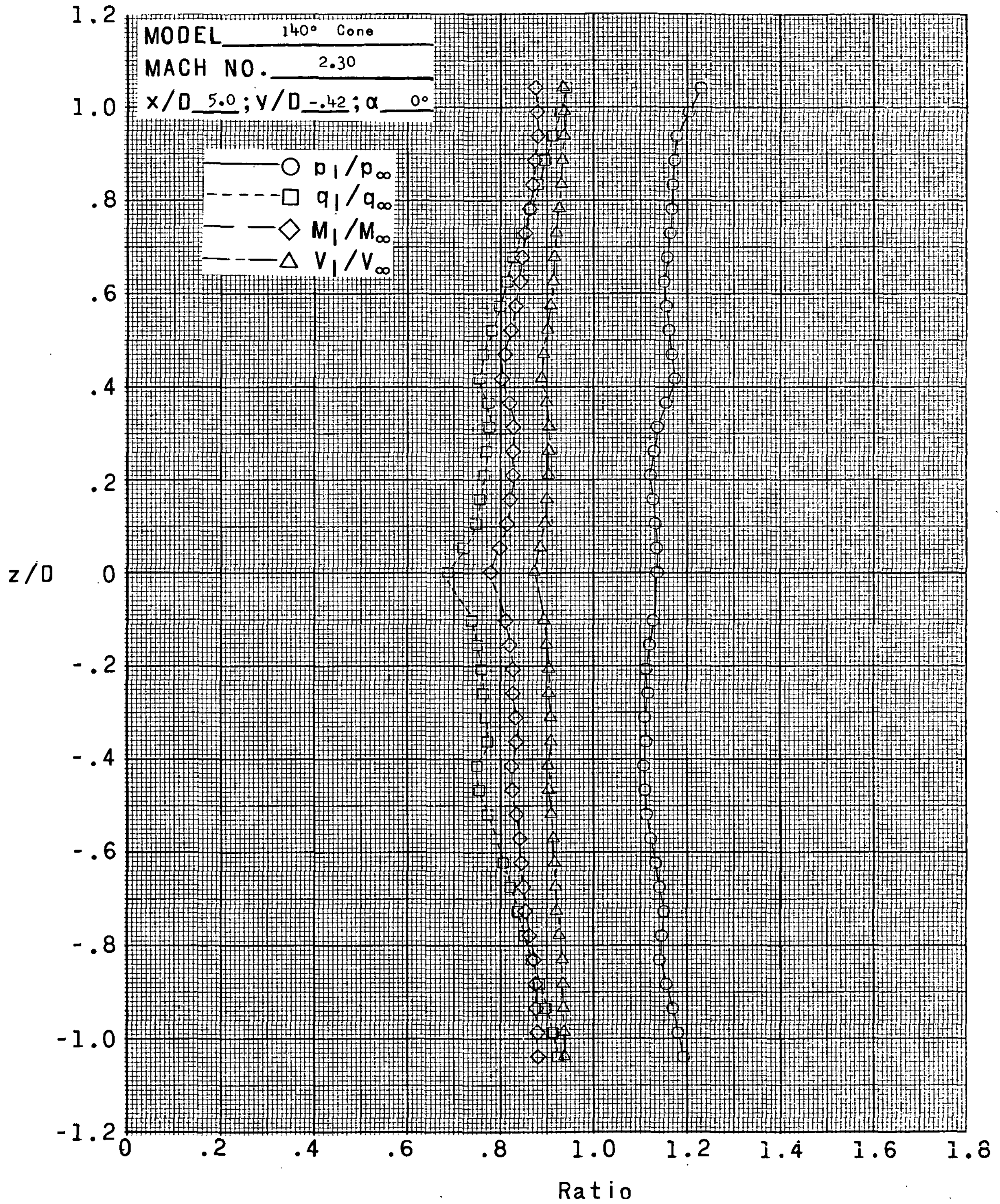
(w) $x/D = 5.0$; $y/D = 0.21$; $\alpha = 0^0$.

Figure 6.- Continued.



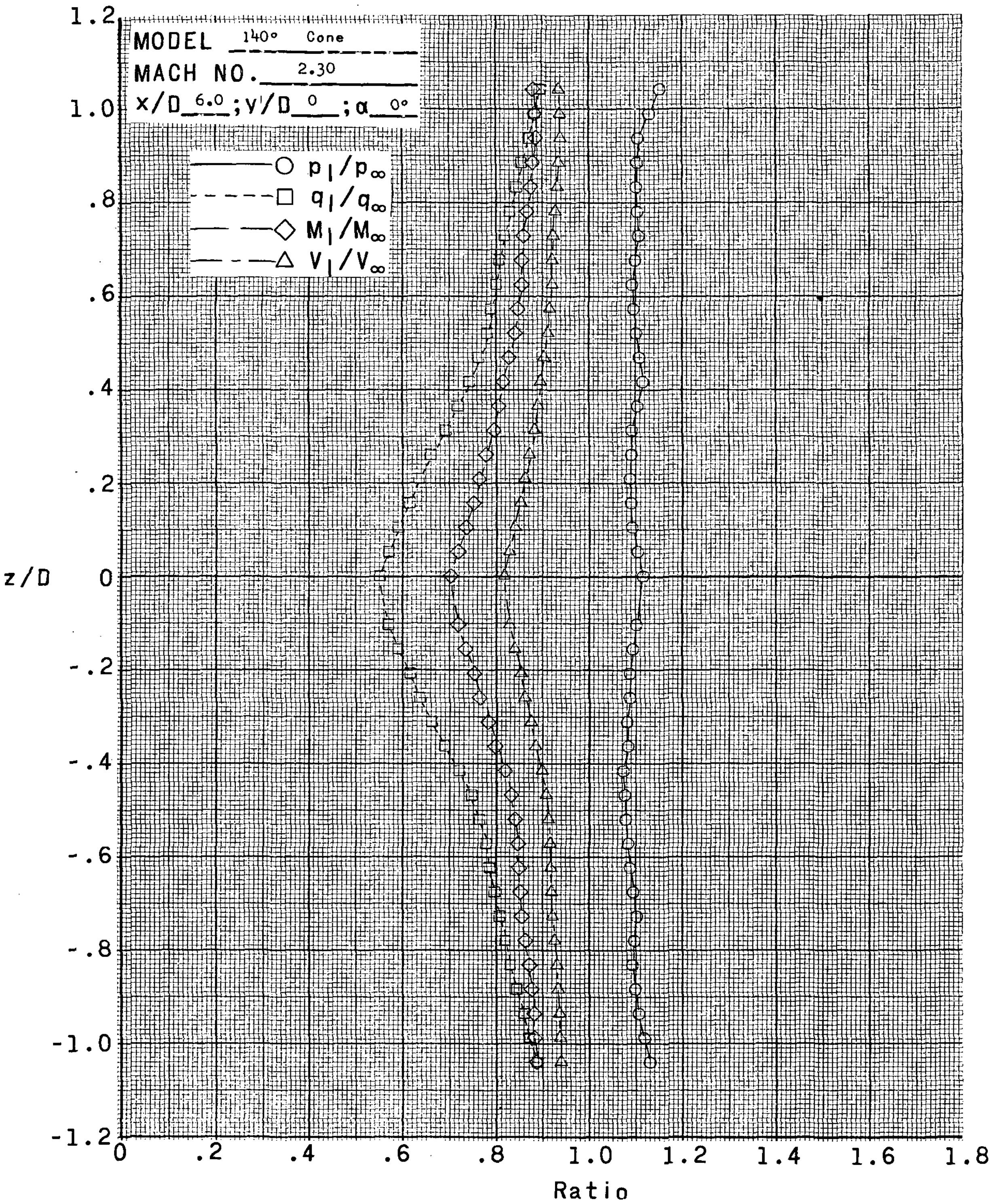
(x) $x/D = 5.0$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 6.- Continued.



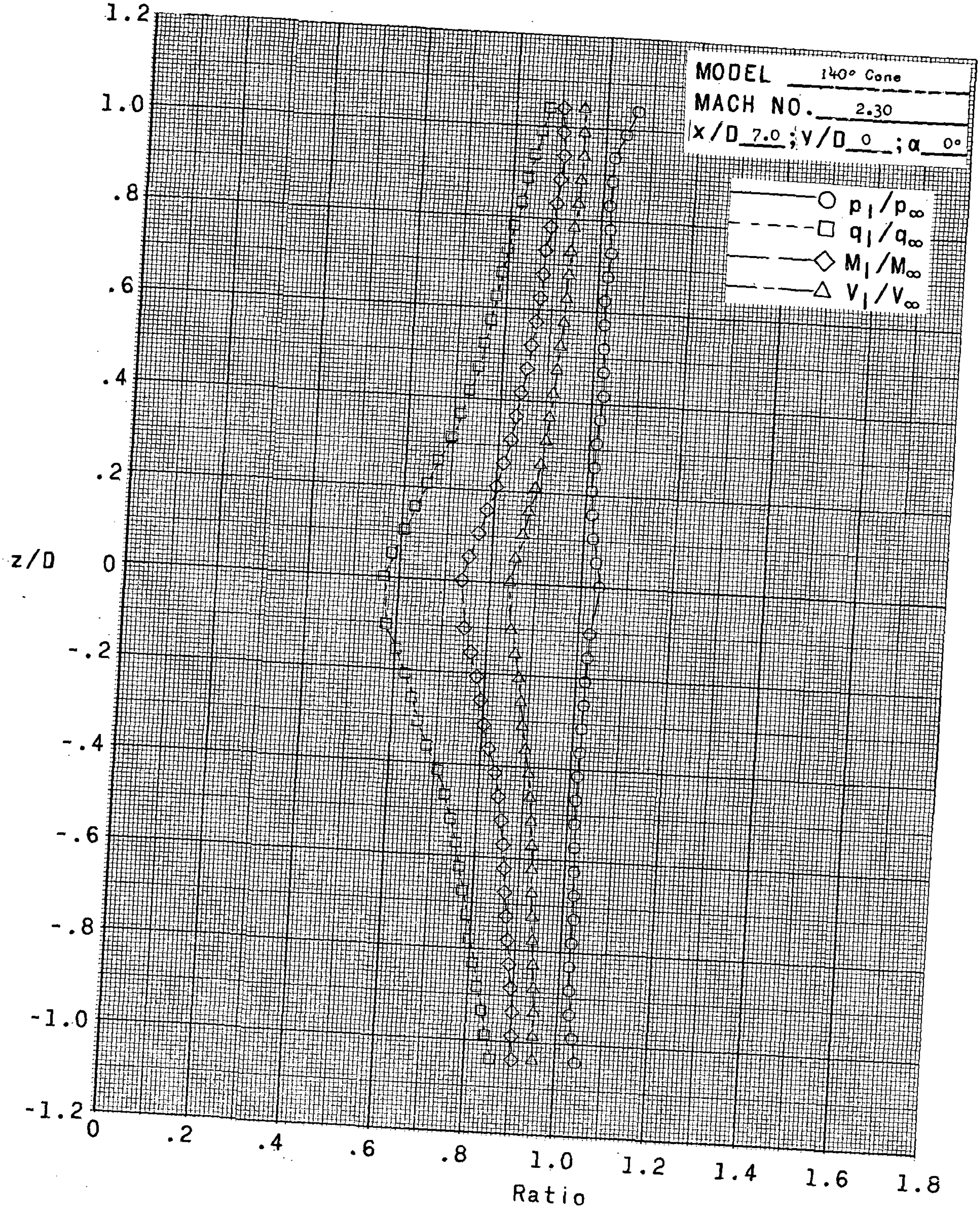
(y) $x/D = 5.0$; $y/D = -0.42$; $\alpha = 0^{0}$.

Figure 6.- Continued.



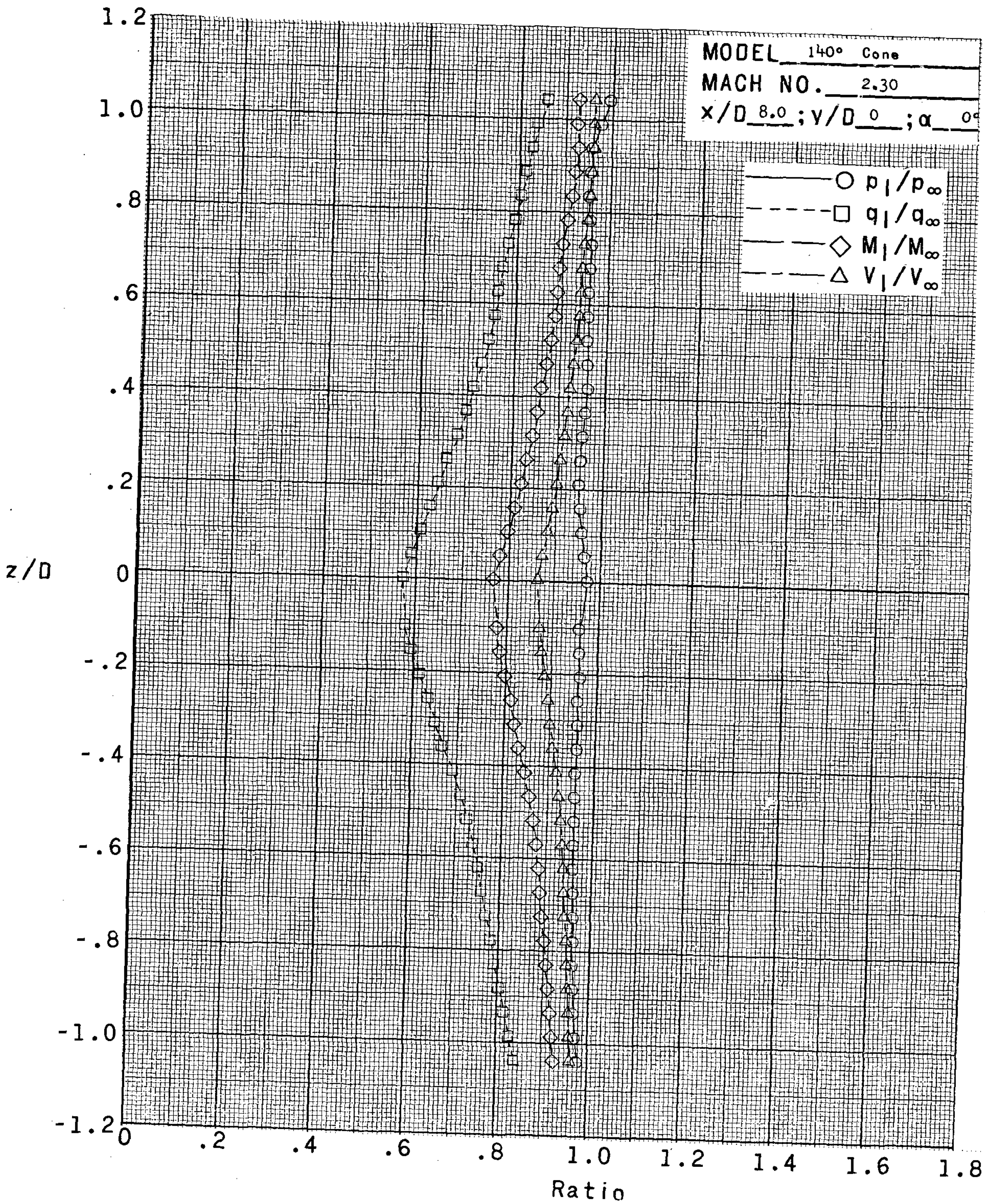
(z) $x/D = 6.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 6.- Continued.



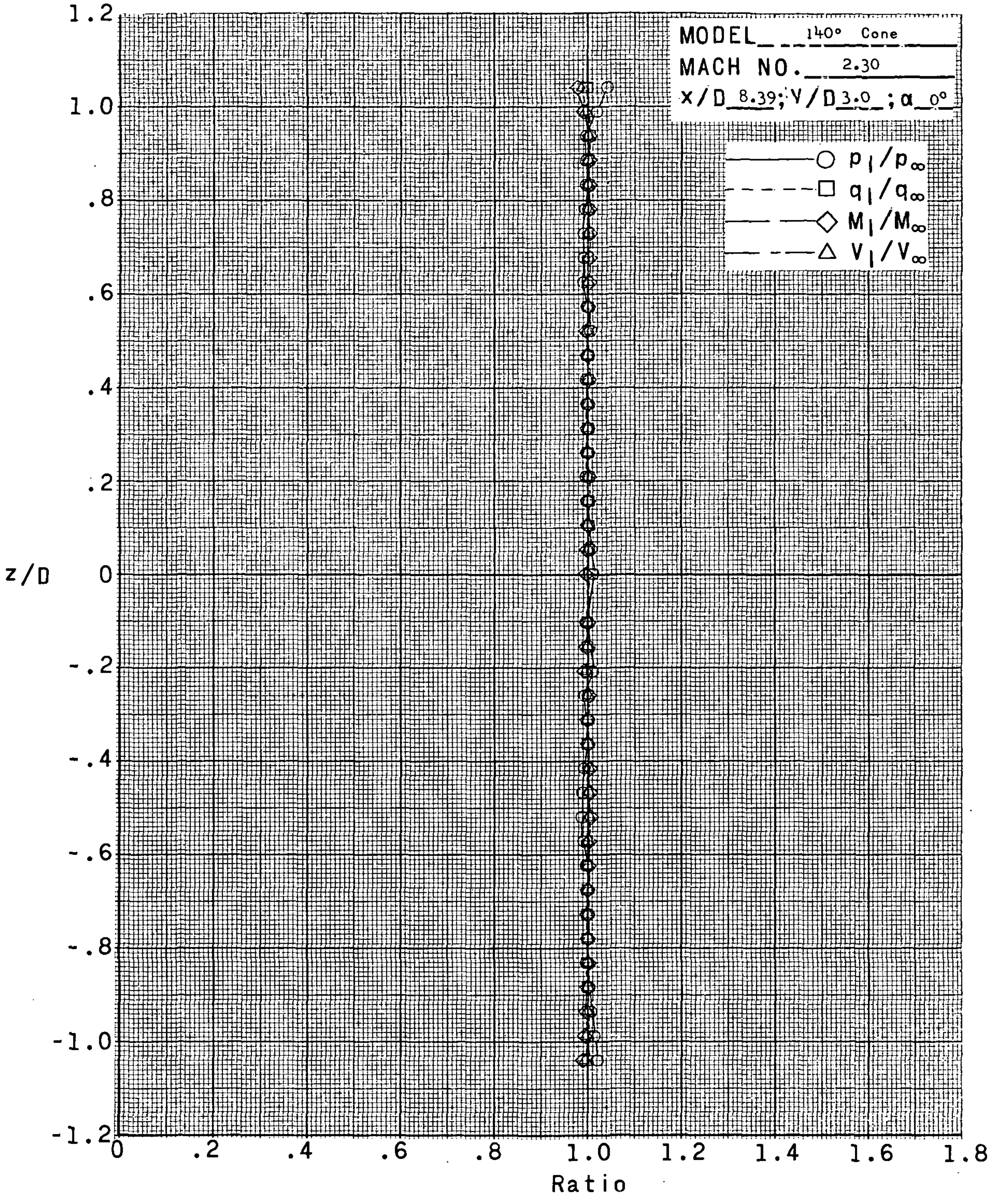
(aa) $x/D = 7.0$; $y/D = 0$; $\alpha = 0^\circ$.

Figure 6.- Continued.



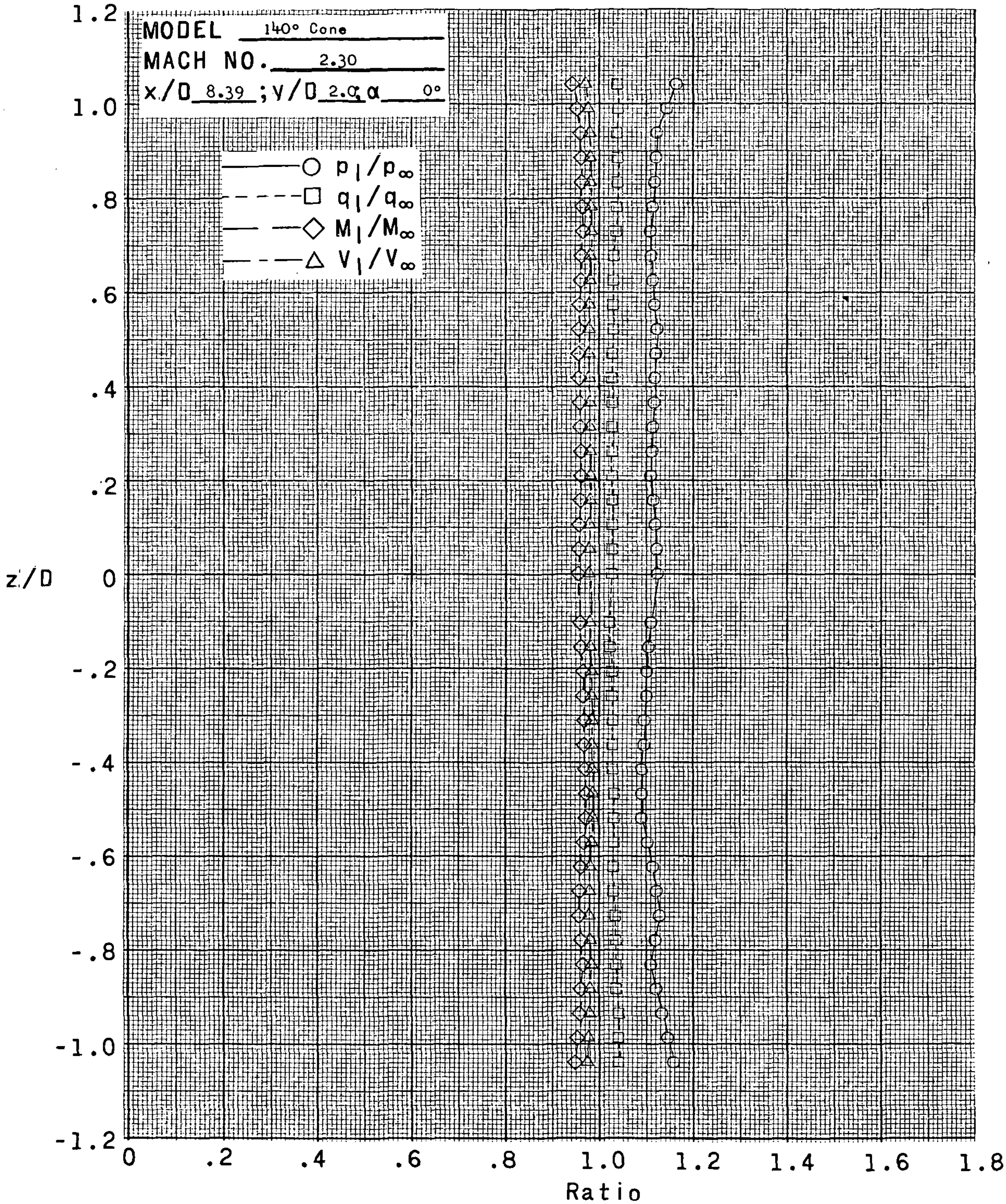
(bb) $x/D = 8.0$; $y/D = 0$; $\alpha = 0^\circ$.

Figure 6.- Continued.



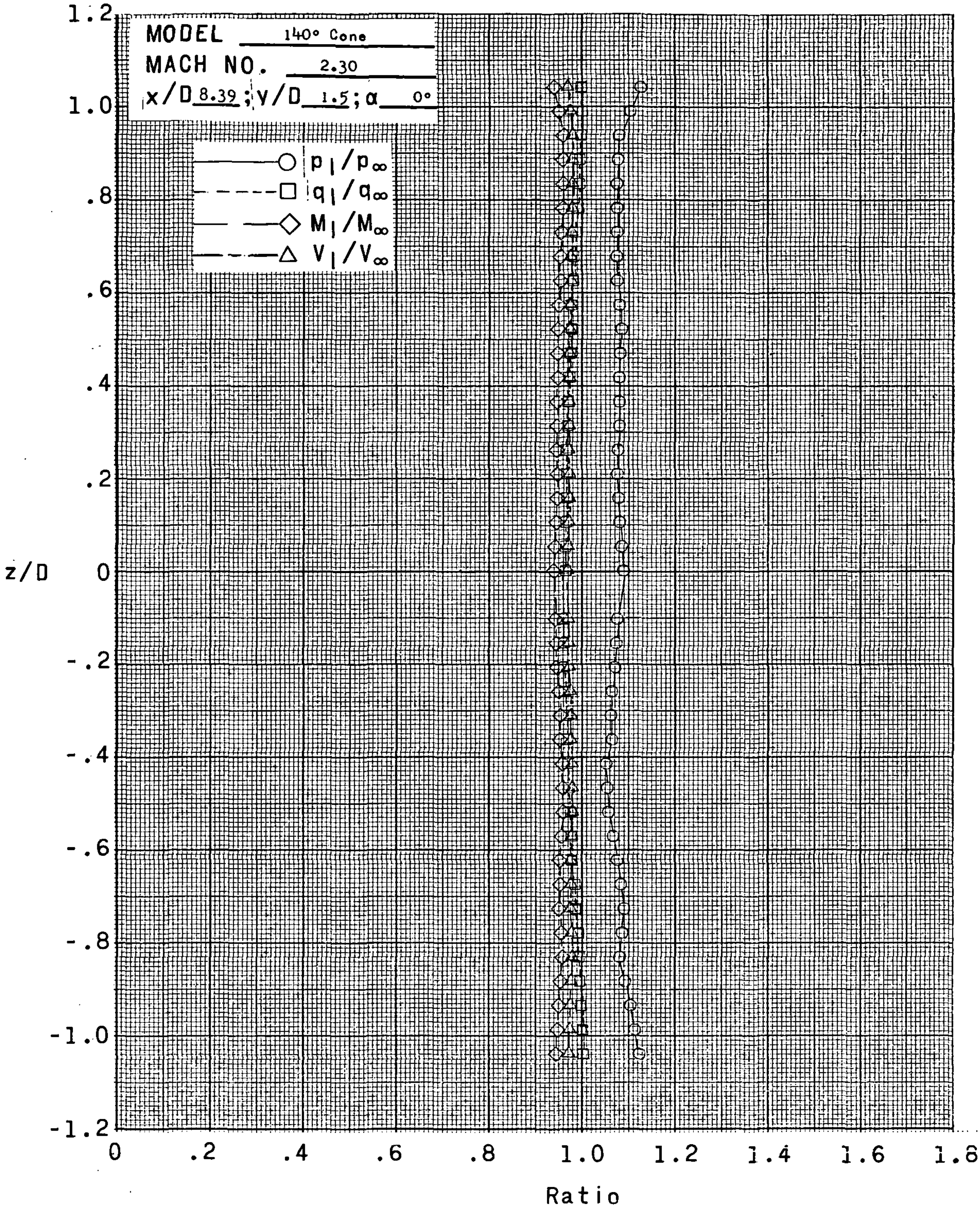
(cc) $x/D = 8.39$; $y/D = 3.0$; $\alpha = 0^0$.

Figure 6.- Continued.



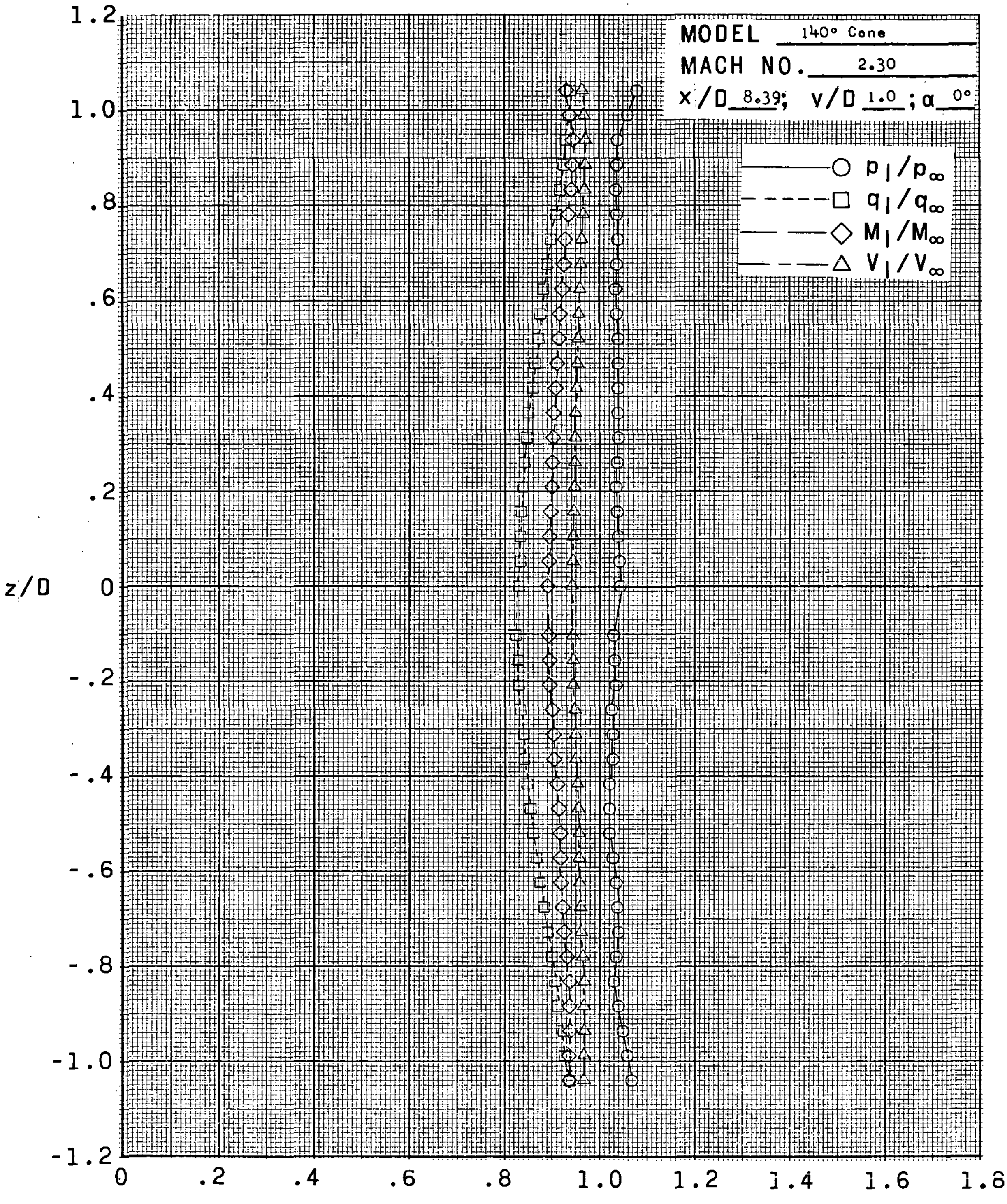
(dd) $x/D = 8.39$; $y/D = 2.0$; $\alpha = 0^0$.

Figure 6.- Continued.



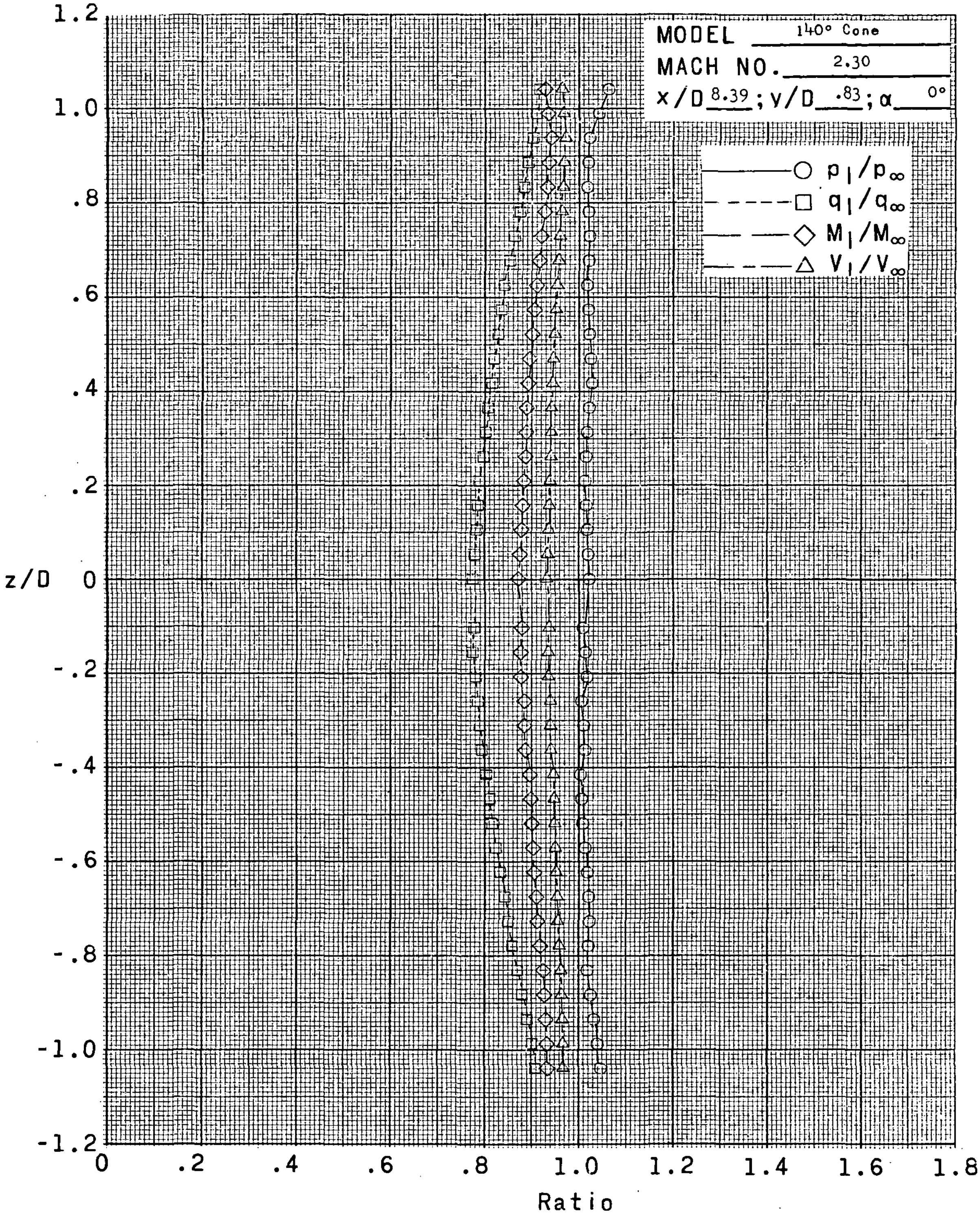
(ee) $x/D = 8.39$; $y/D = 1.5$; $\alpha = 0^0$.

Figure 6.- Continued.



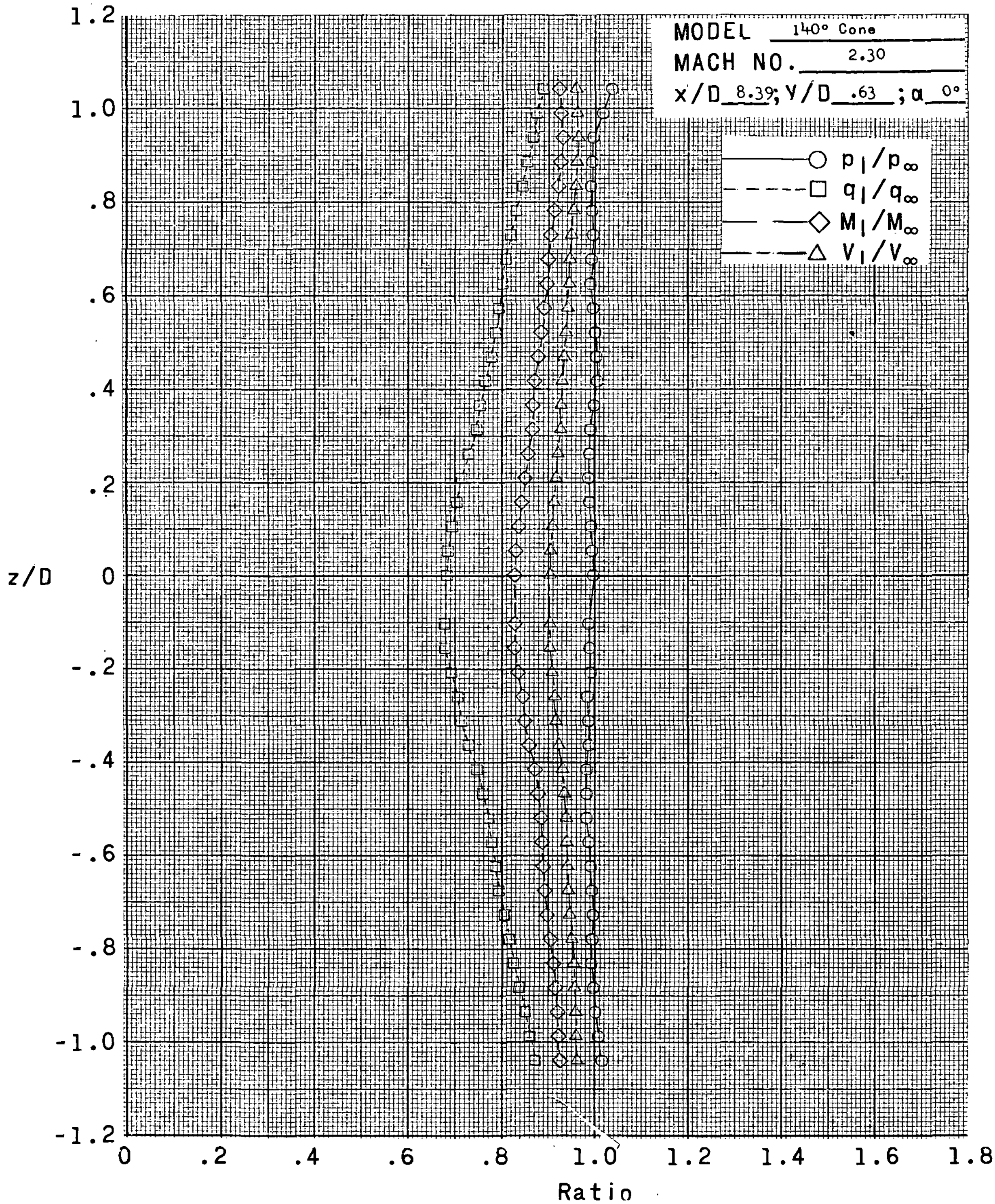
(ff) $x/D = 8.39$; $y/D = 1.0$; $\alpha = 0^o$.

Figure 6.- Continued.



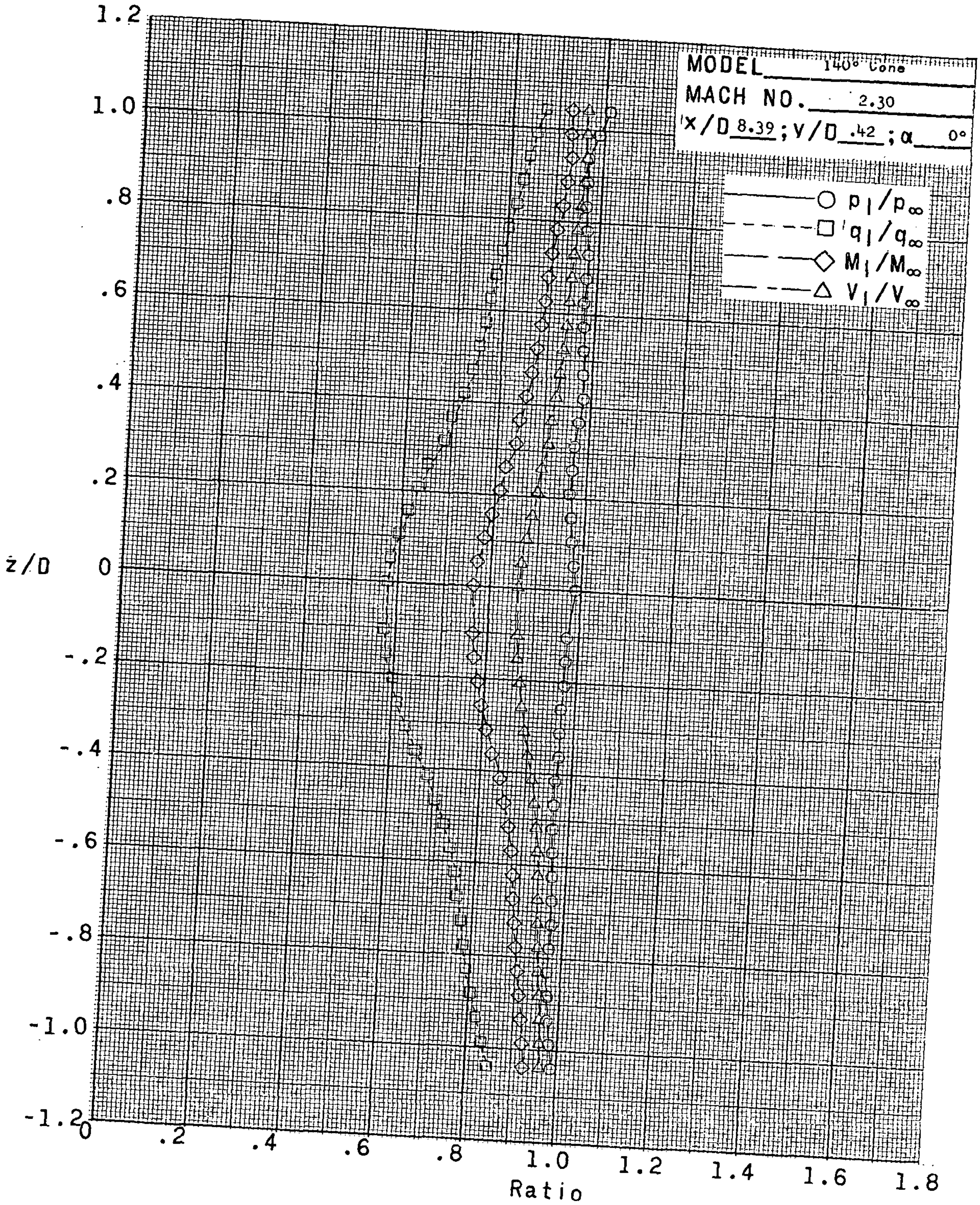
(gg) $x/D = 8.39$; $y/D = 0.83$; $\alpha = 0^0$.

Figure 6.- Continued.



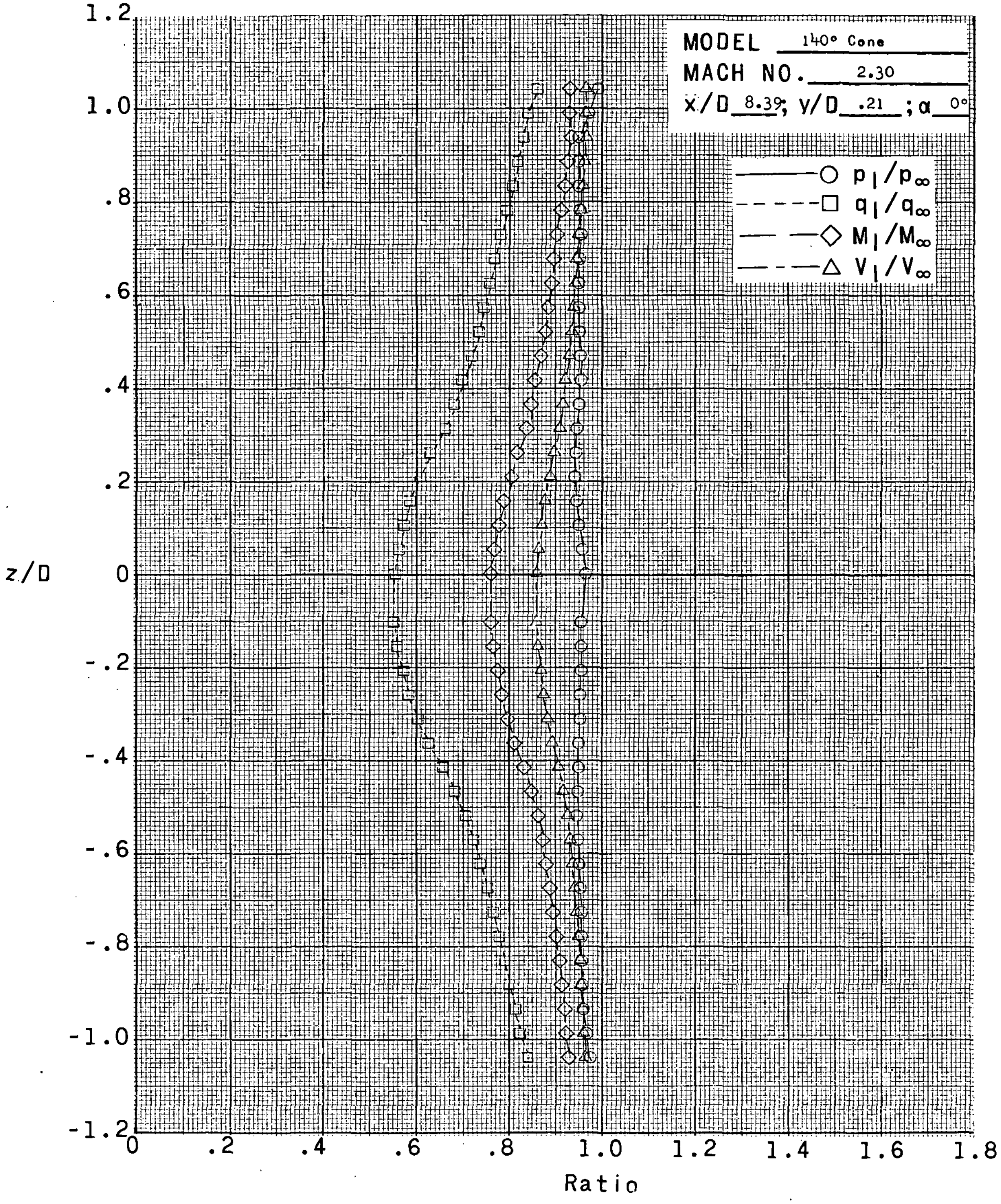
(hh) x/D = 8.39; y/D = 0.63; α = 0°.

Figure 6.- Continued.



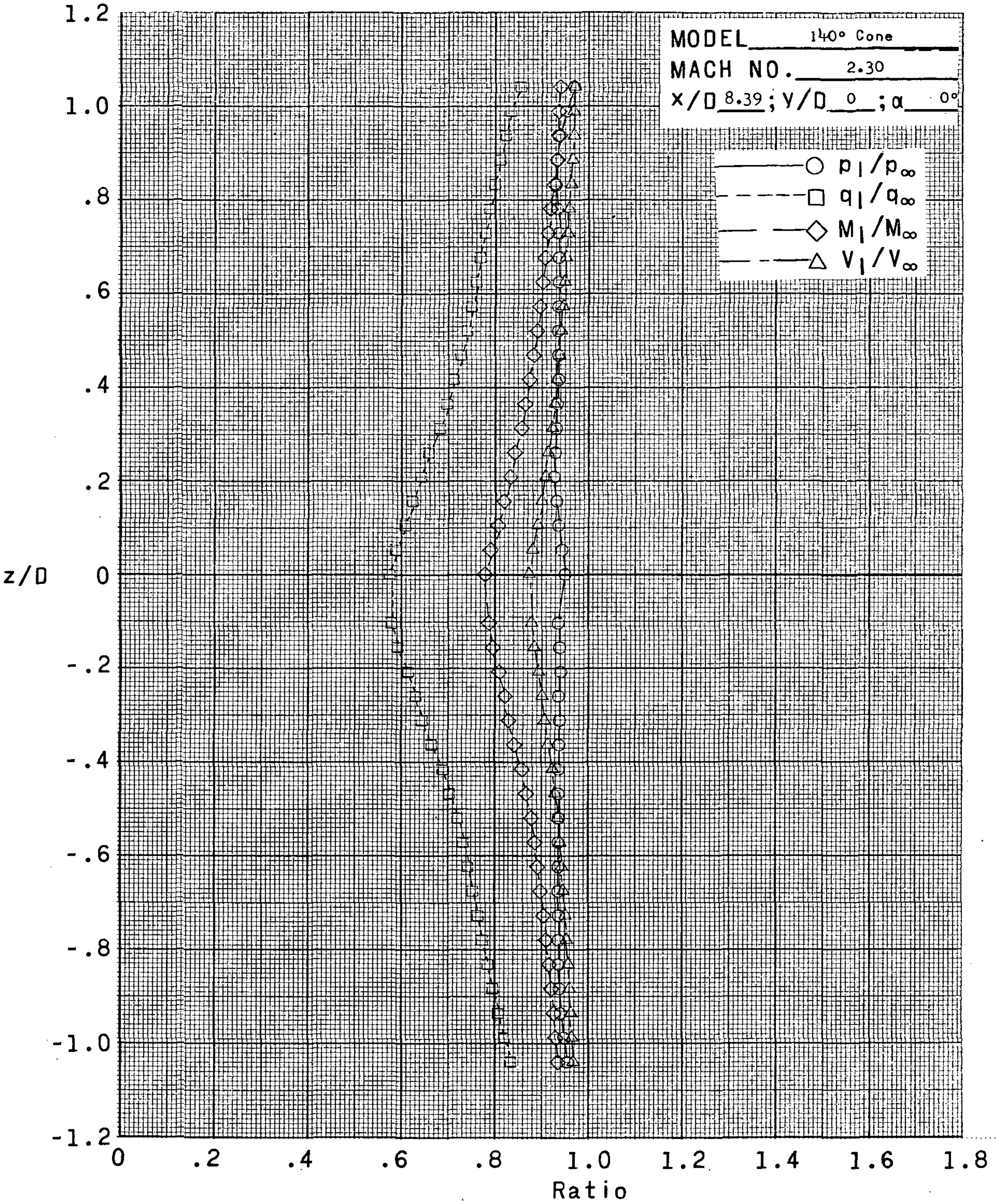
(ii) $x/D = 8.39$; $y/D = 0.42$; $\alpha = 0^0$.

Figure 6.- Continued.



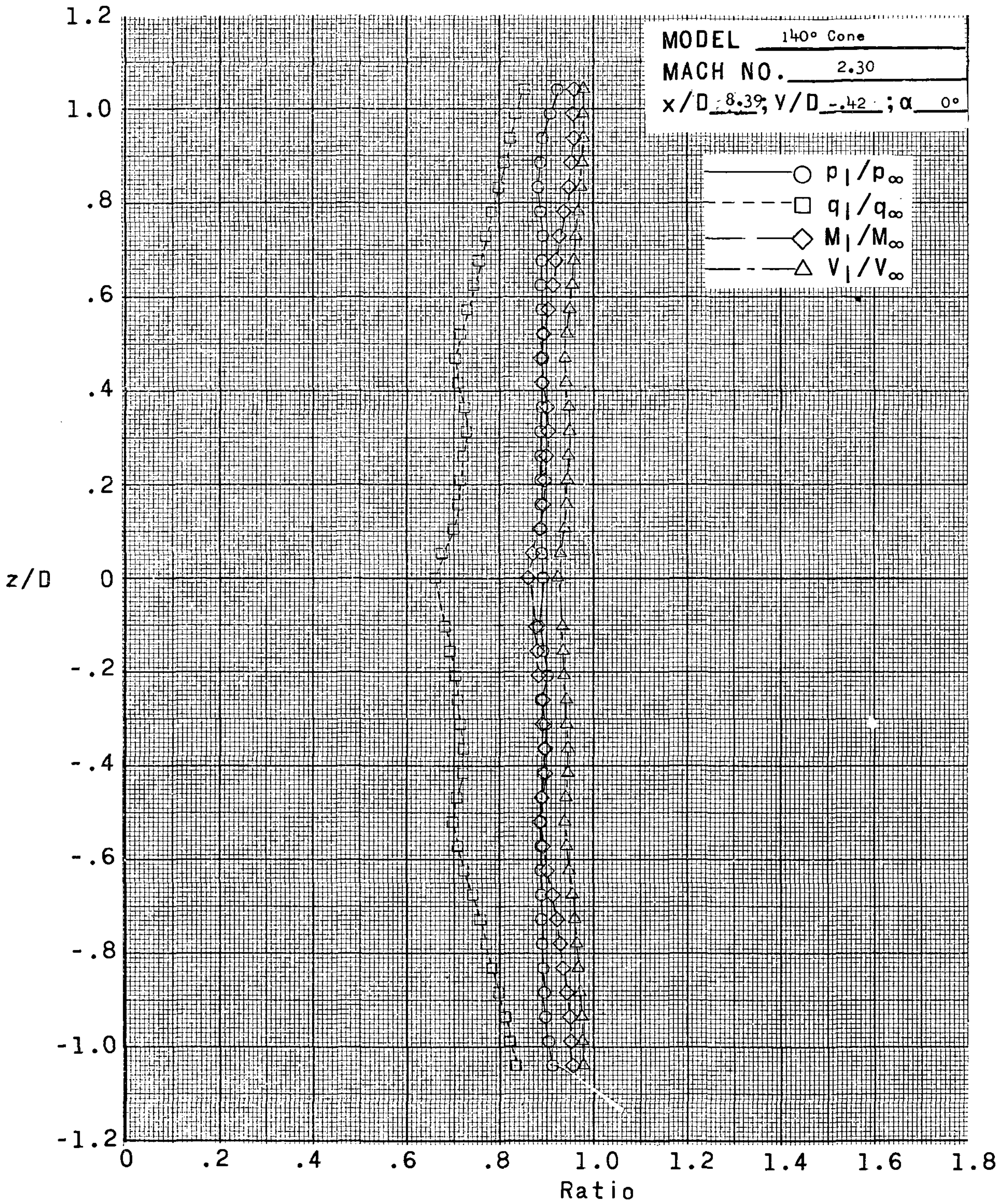
(jj) x/D = 8.39; y/D = 0.21; α = 0°.

Figure 6.- Continued.



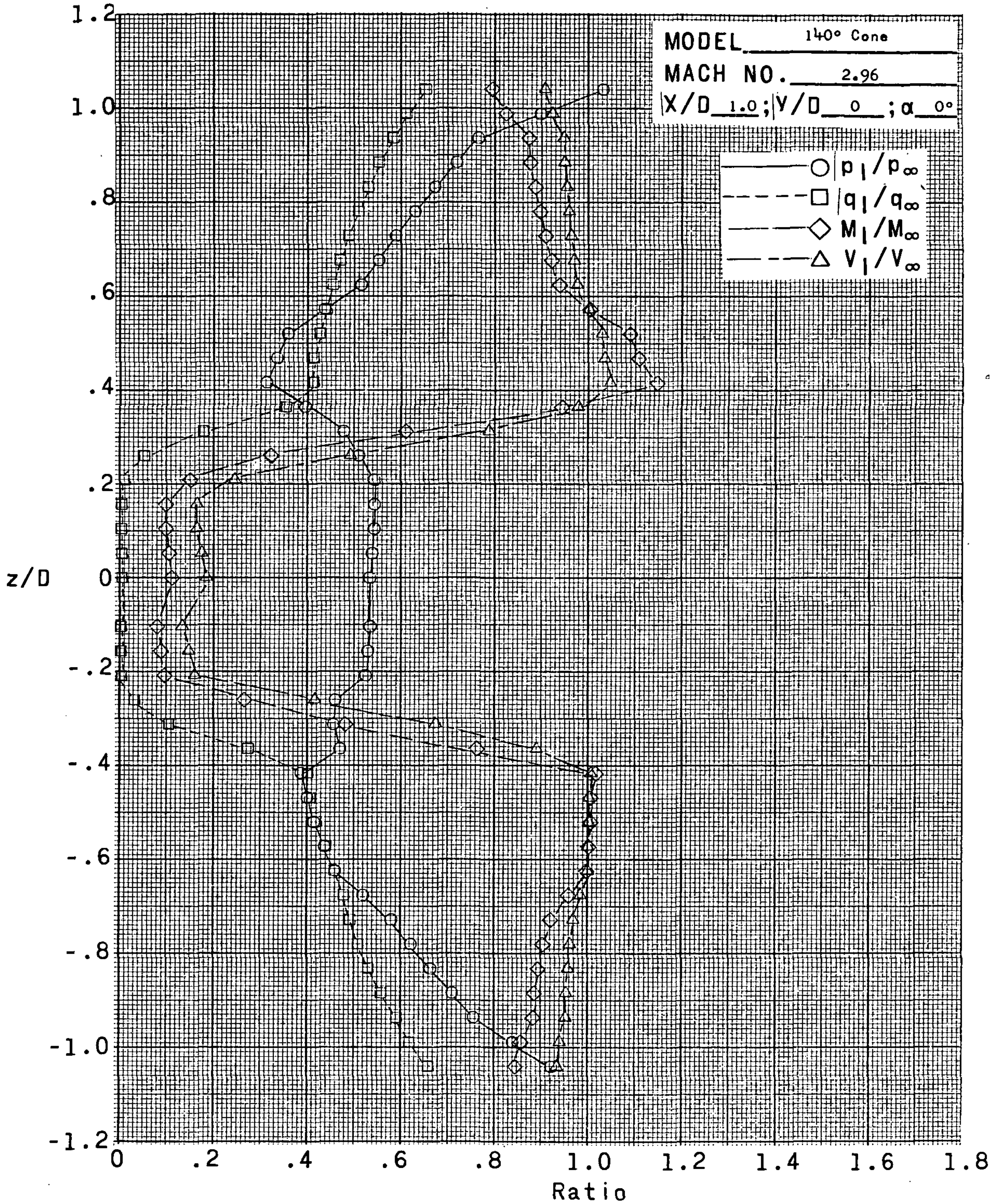
(kk) $x/D = 8.39$; $y/D = 0$; $\alpha = 0^0$.

Figure 6.- Continued.



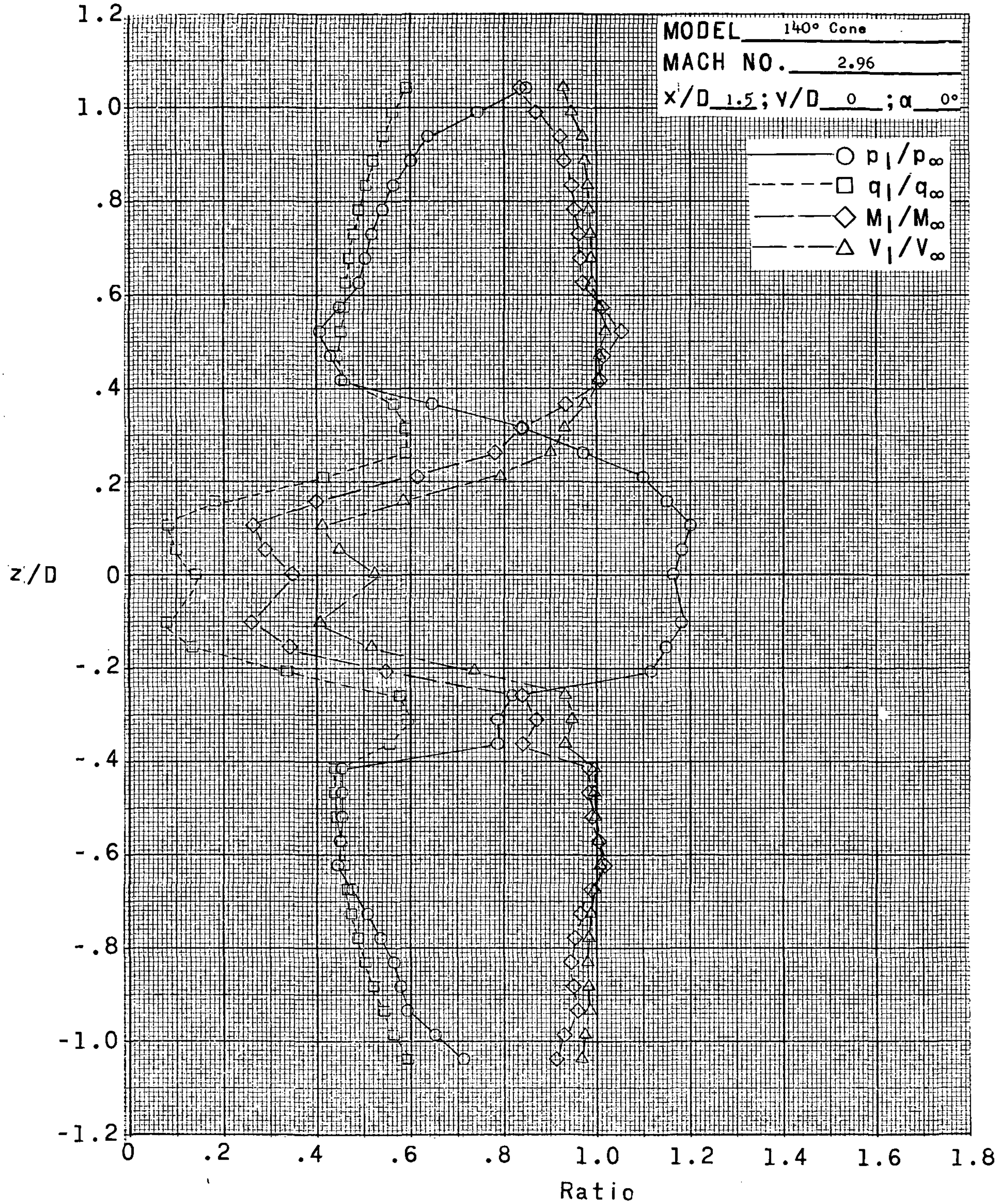
(l) x/D = 8.39; y/D = -0.42; $\alpha = 0^0$.

Figure 6.- Concluded.



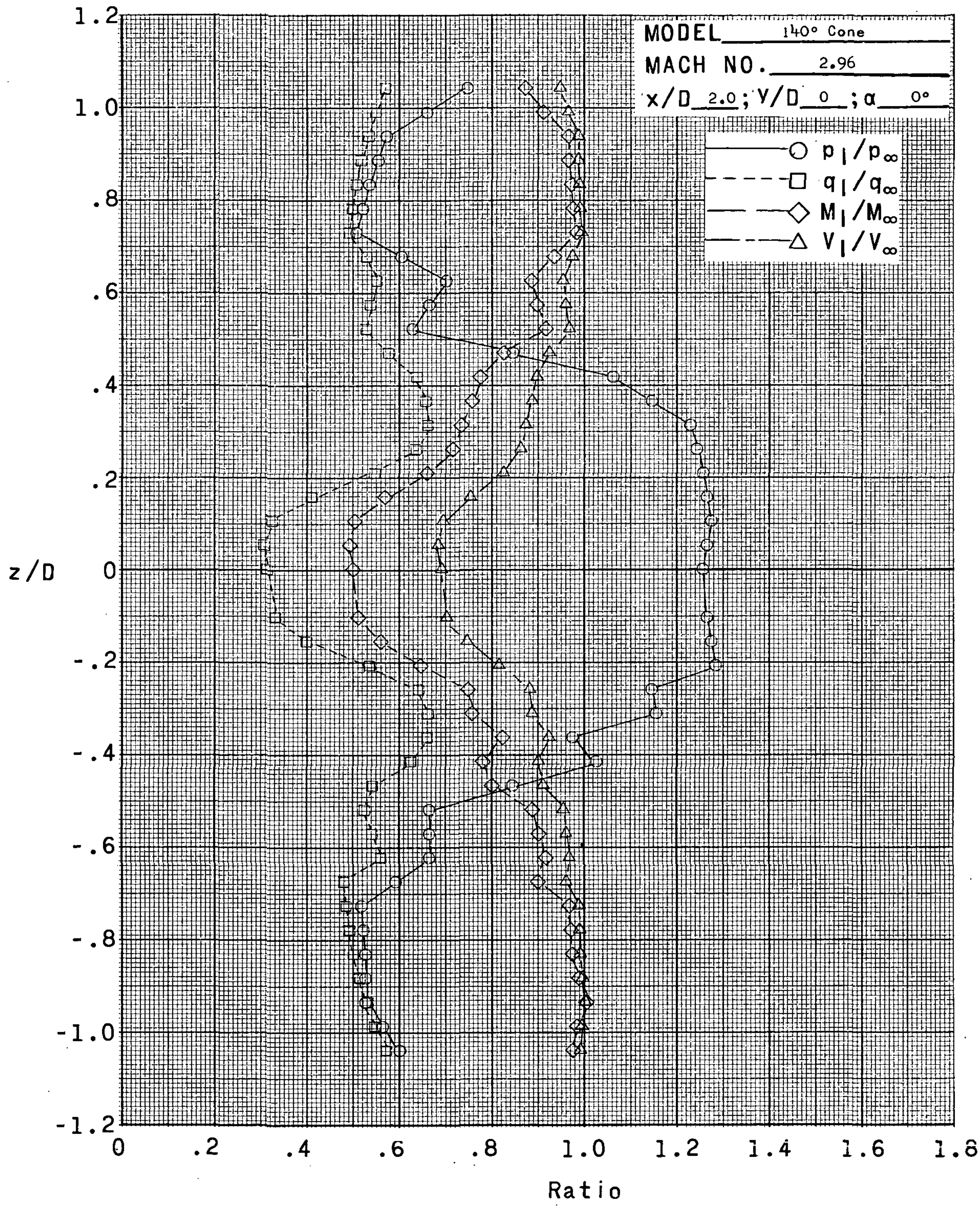
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 7.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D in wake of 140^0-included-angle cone at Mach number of 2.96 and Reynolds number of 5.42×10^6 per meter $(1.65 \times 10^6$ per foot).



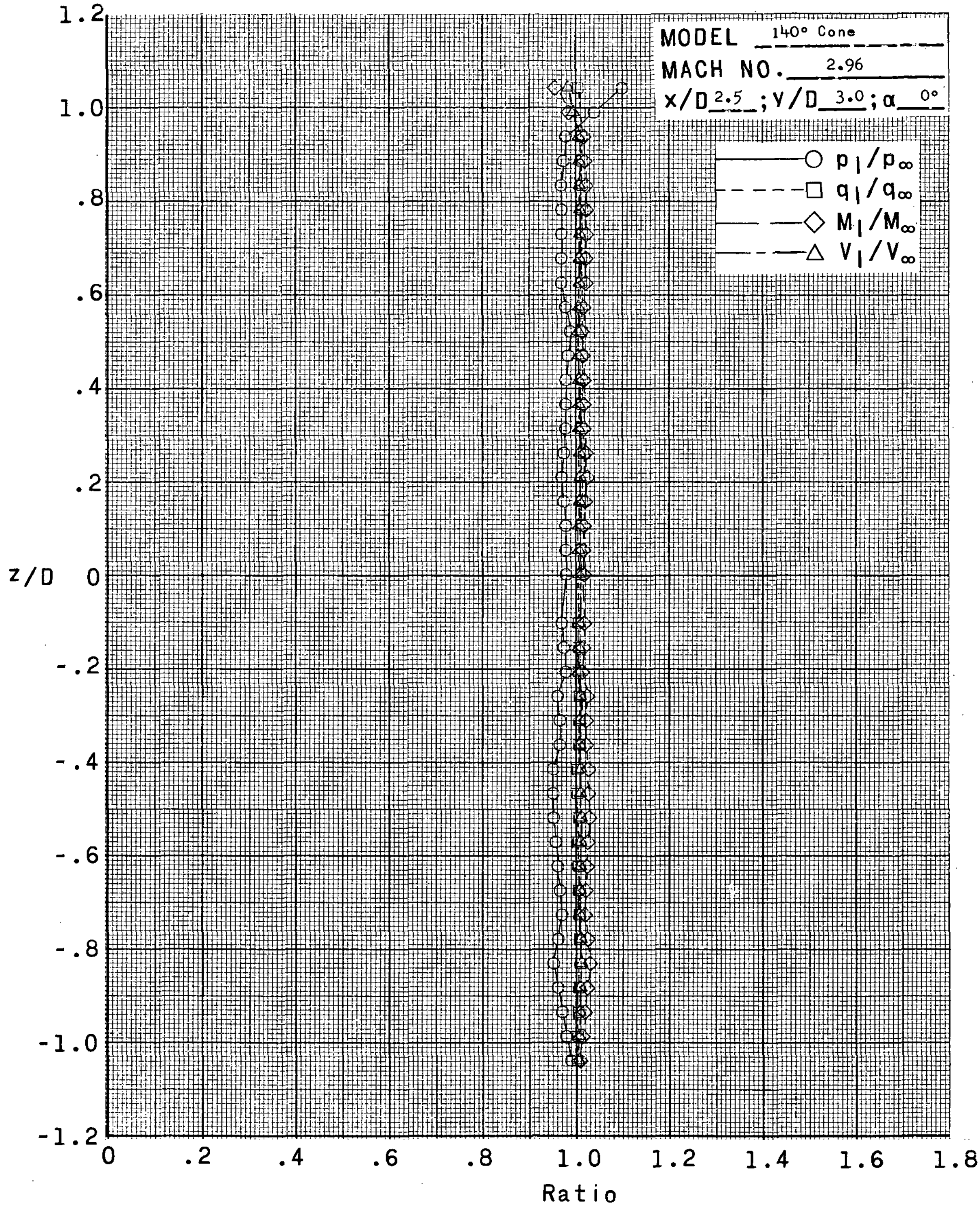
(b) x/D = 1.5; y/D = 0; α = 0°.

Figure 7.- Continued.



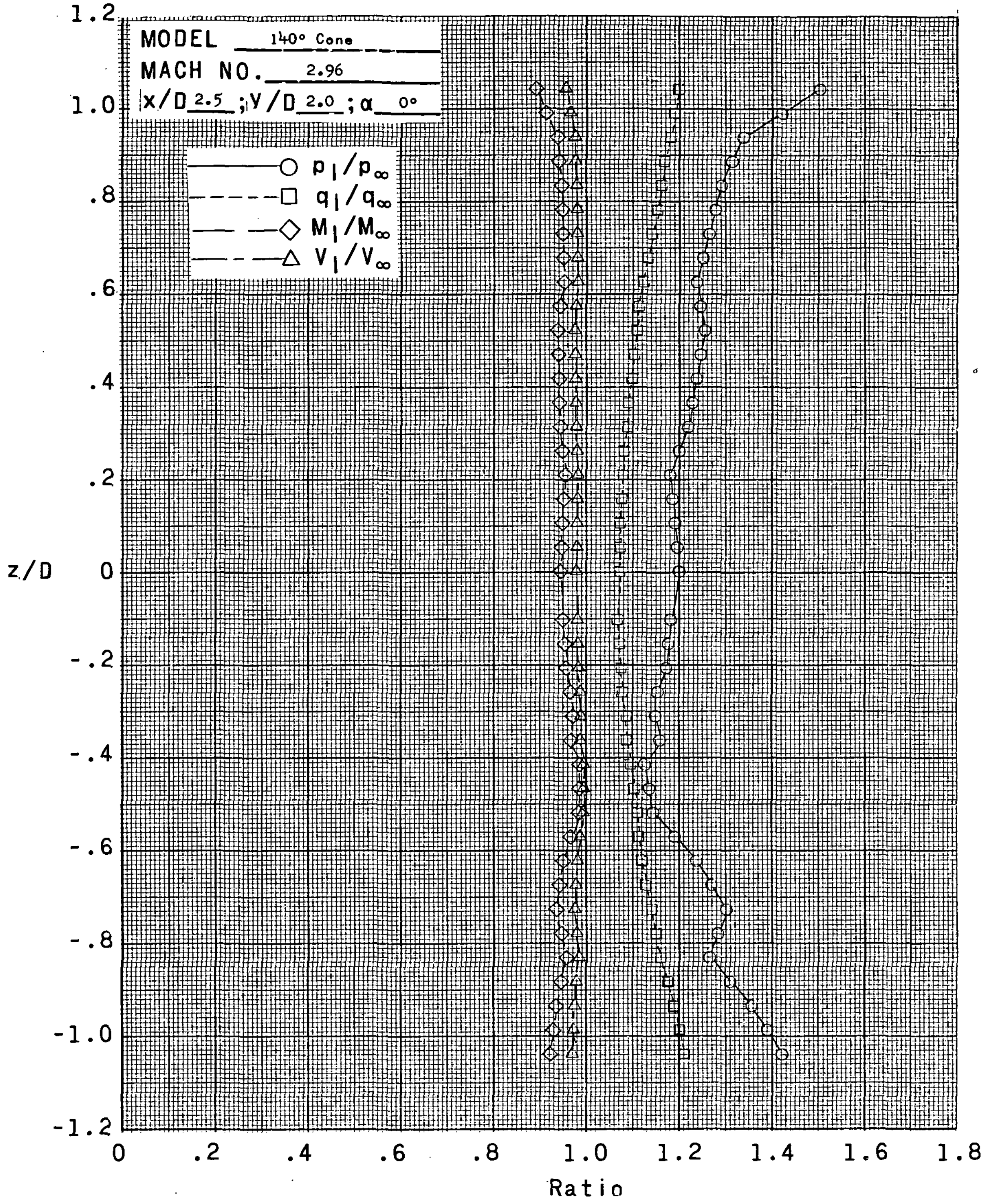
(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 7.- Continued.



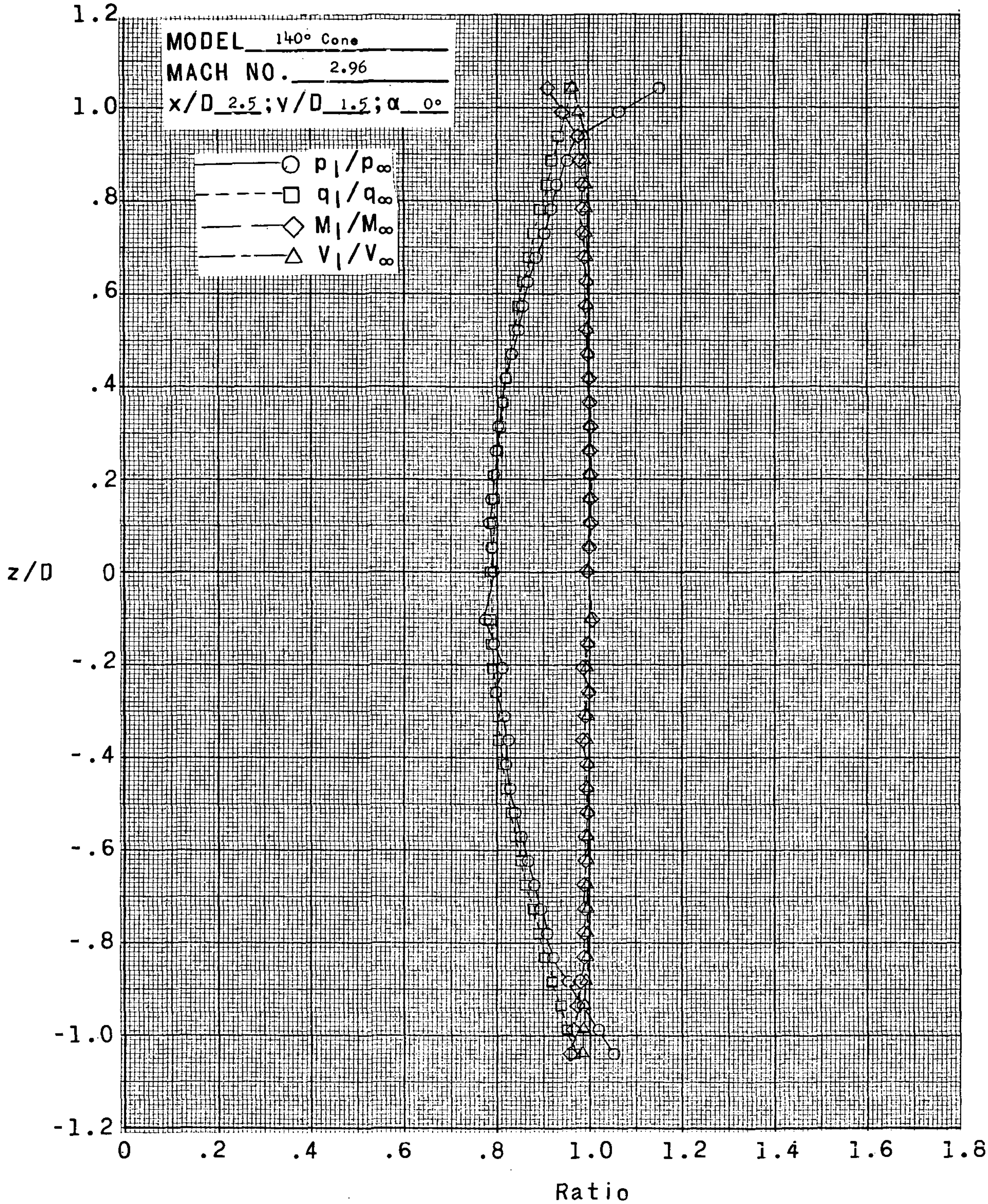
(d) $x/D = 2.5$; $y/D = 3.0$; $\alpha = 0^{\circ}$.

Figure 7.- Continued.



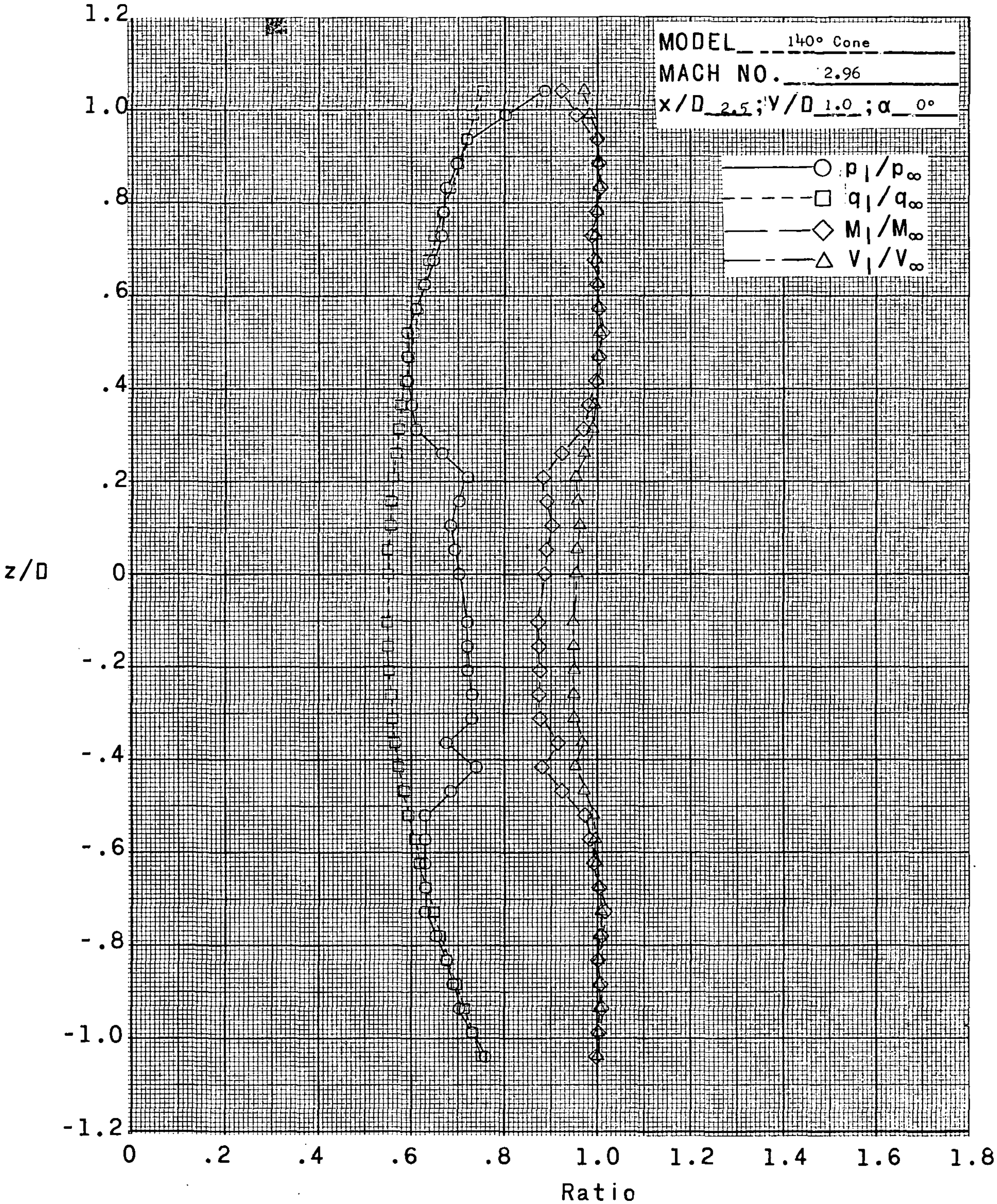
(e) x/D = 2.5; y/D = 2.0; α = 0°.

Figure 7.- Continued.



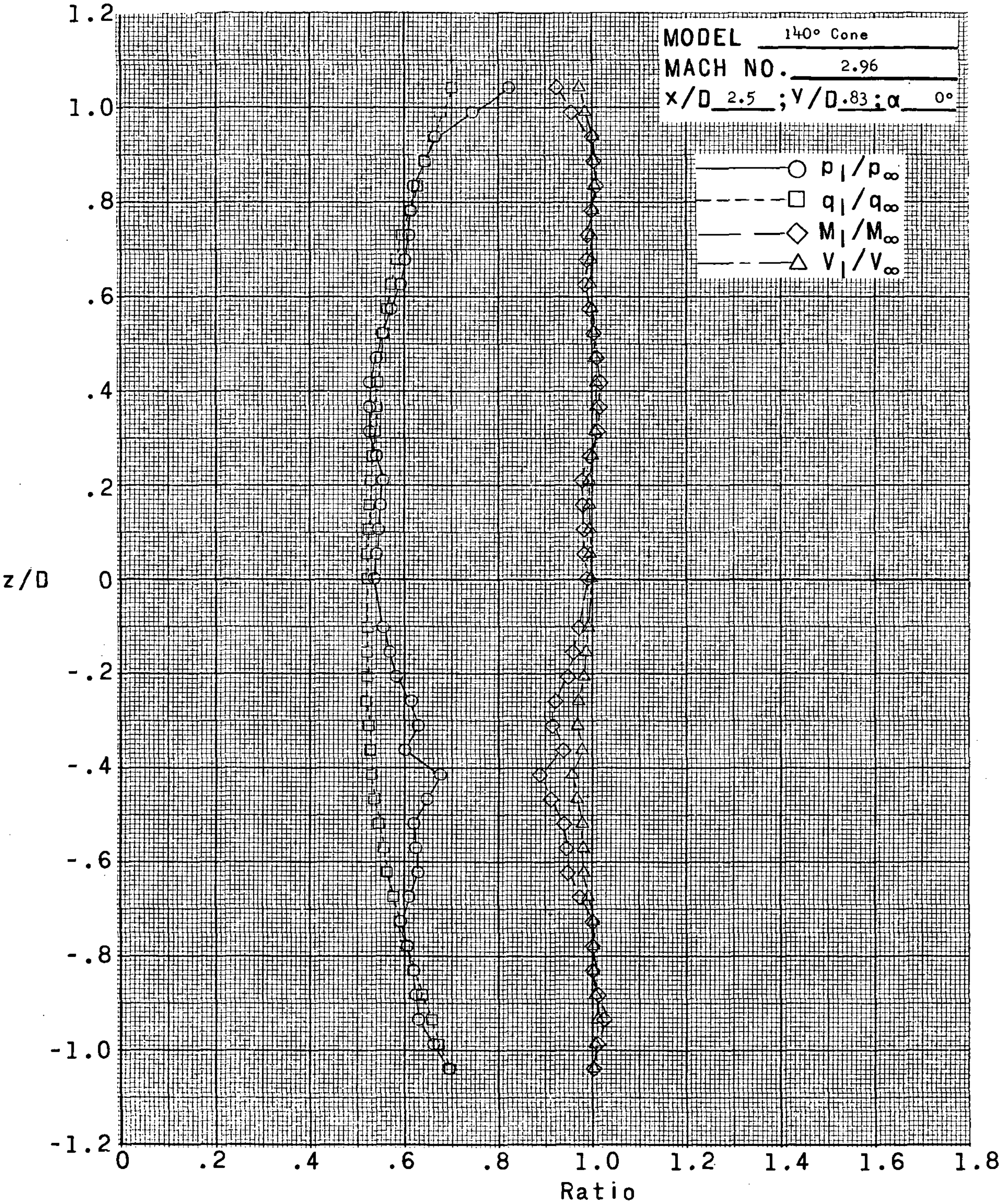
(f) $x/D = 2.5$; $y/D = 1.5$; $\alpha = 0^0$.

Figure 7.- Continued.



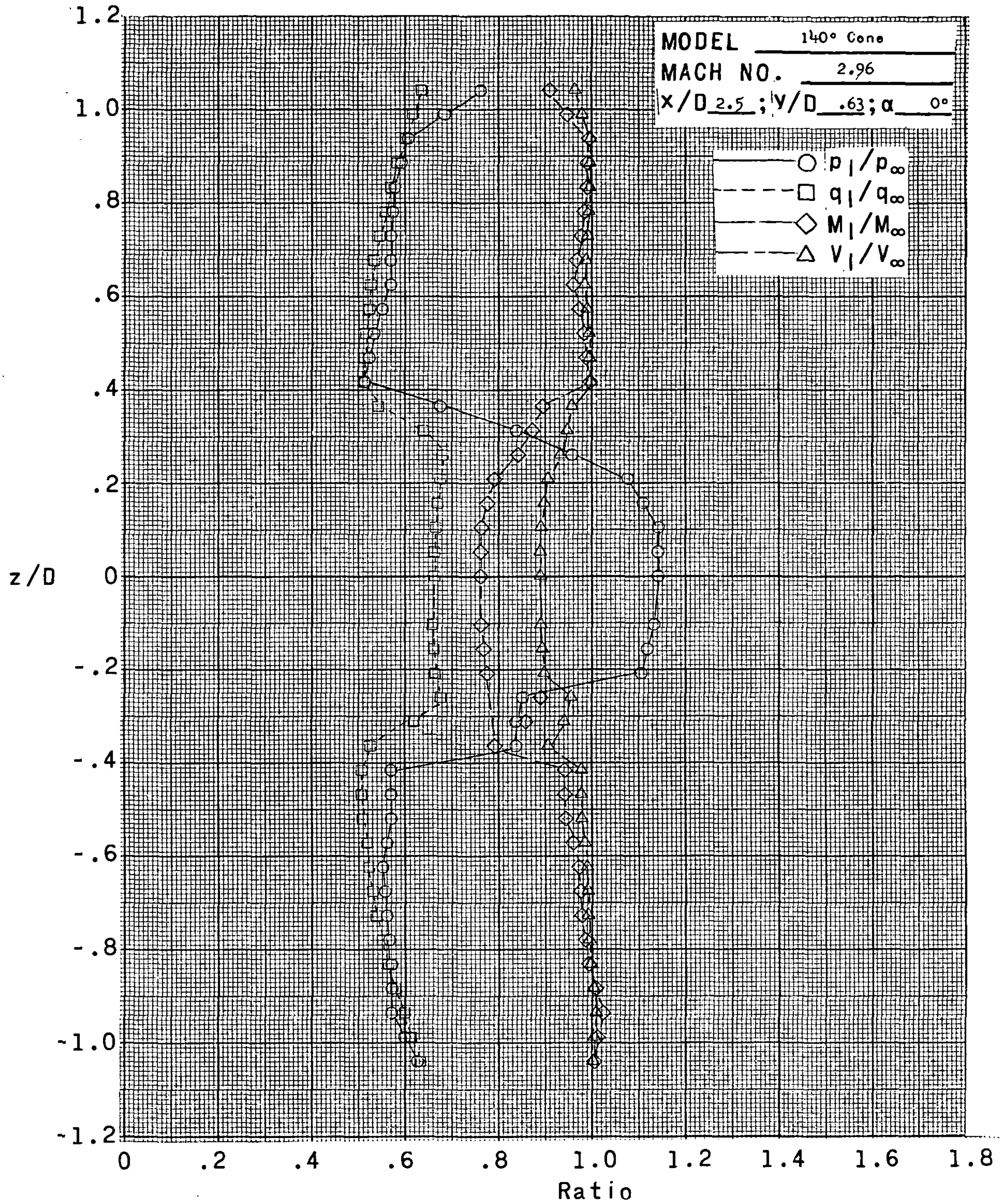
(g) $x/D = 2.5$; $y/D = 1.0$; $\alpha = 0^0$.

Figure 7.- Continued.



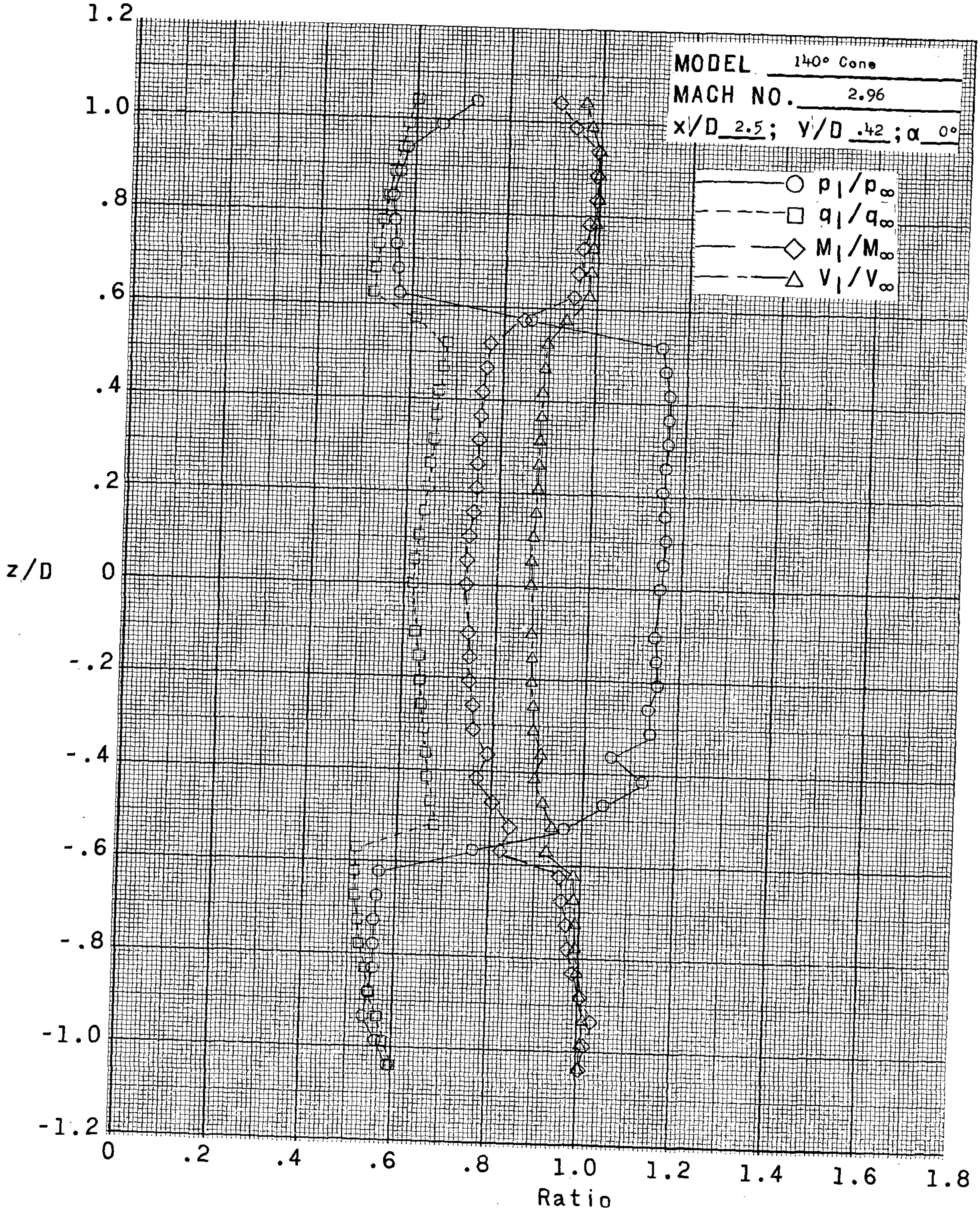
(h) $x/D = 2.5$; $y/D = 0.83$; $\alpha = 0^0$.

Figure 7.- Continued.



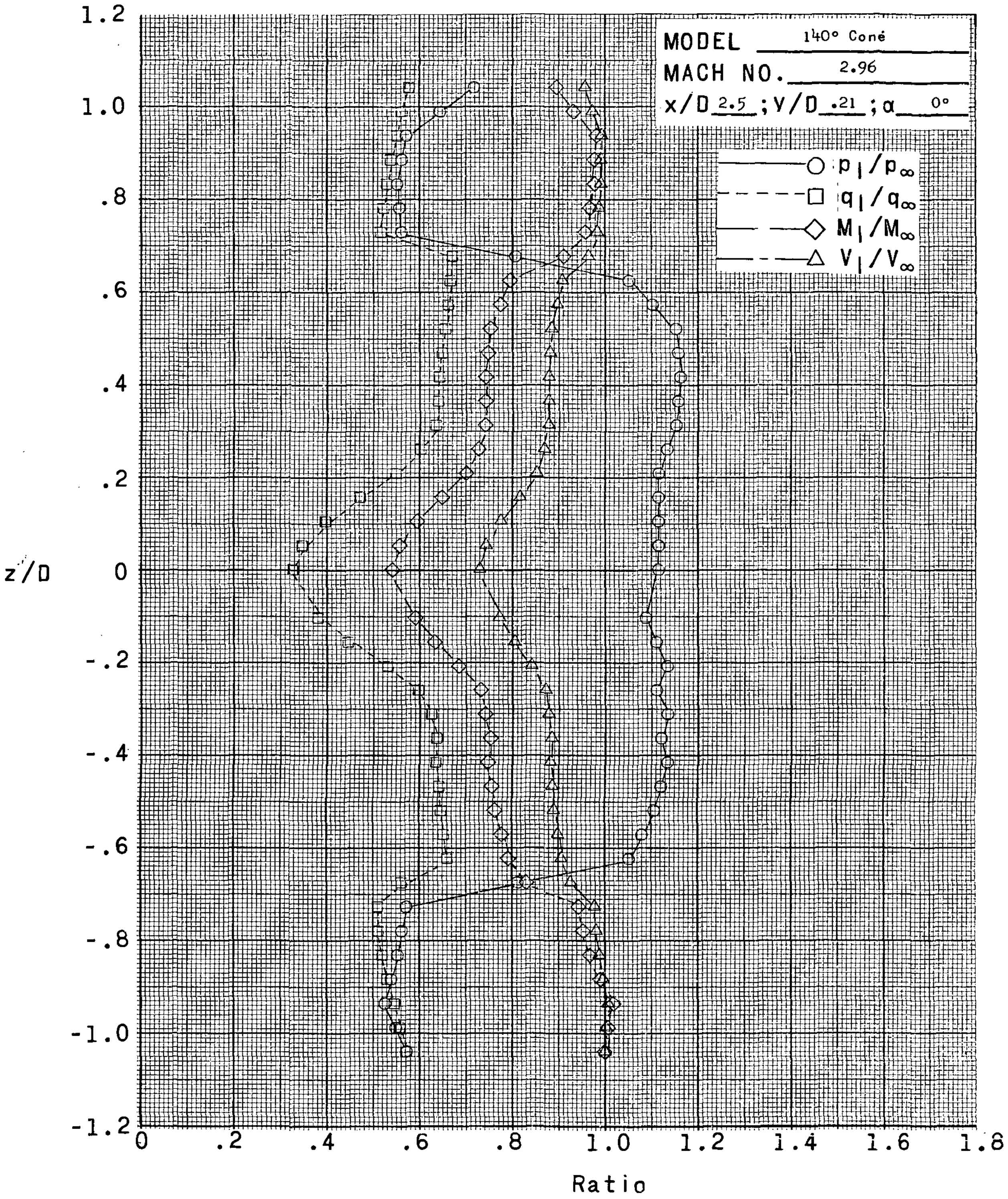
(i) $x/D = 2.5$; $y/D = 0.63$; $\alpha = 0^0$.

Figure 7.- Continued.



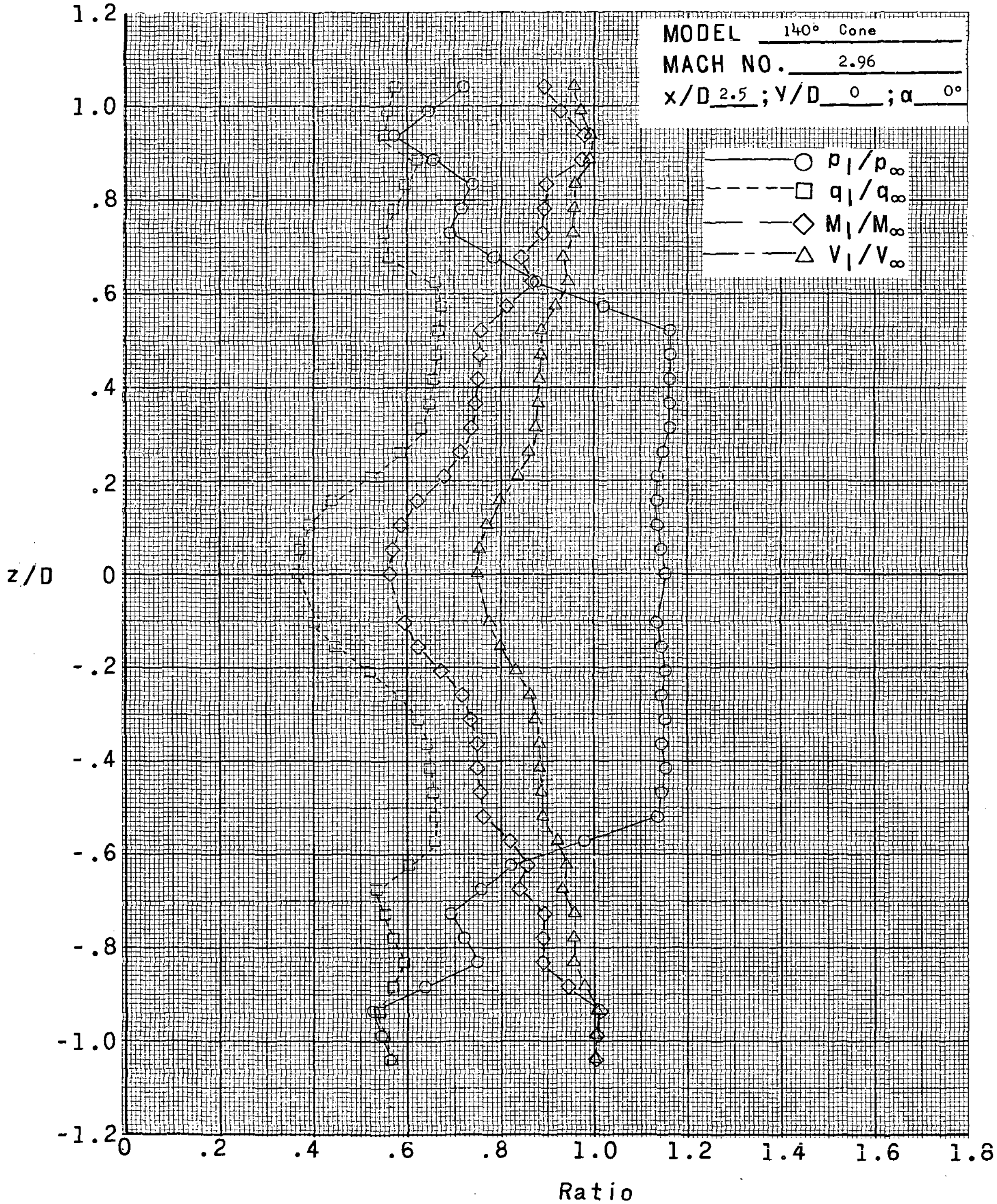
(j) $x/D = 2.5$; $y/D = 0.42$; $\alpha = 0^{0}$.

Figure 7.- Continued.



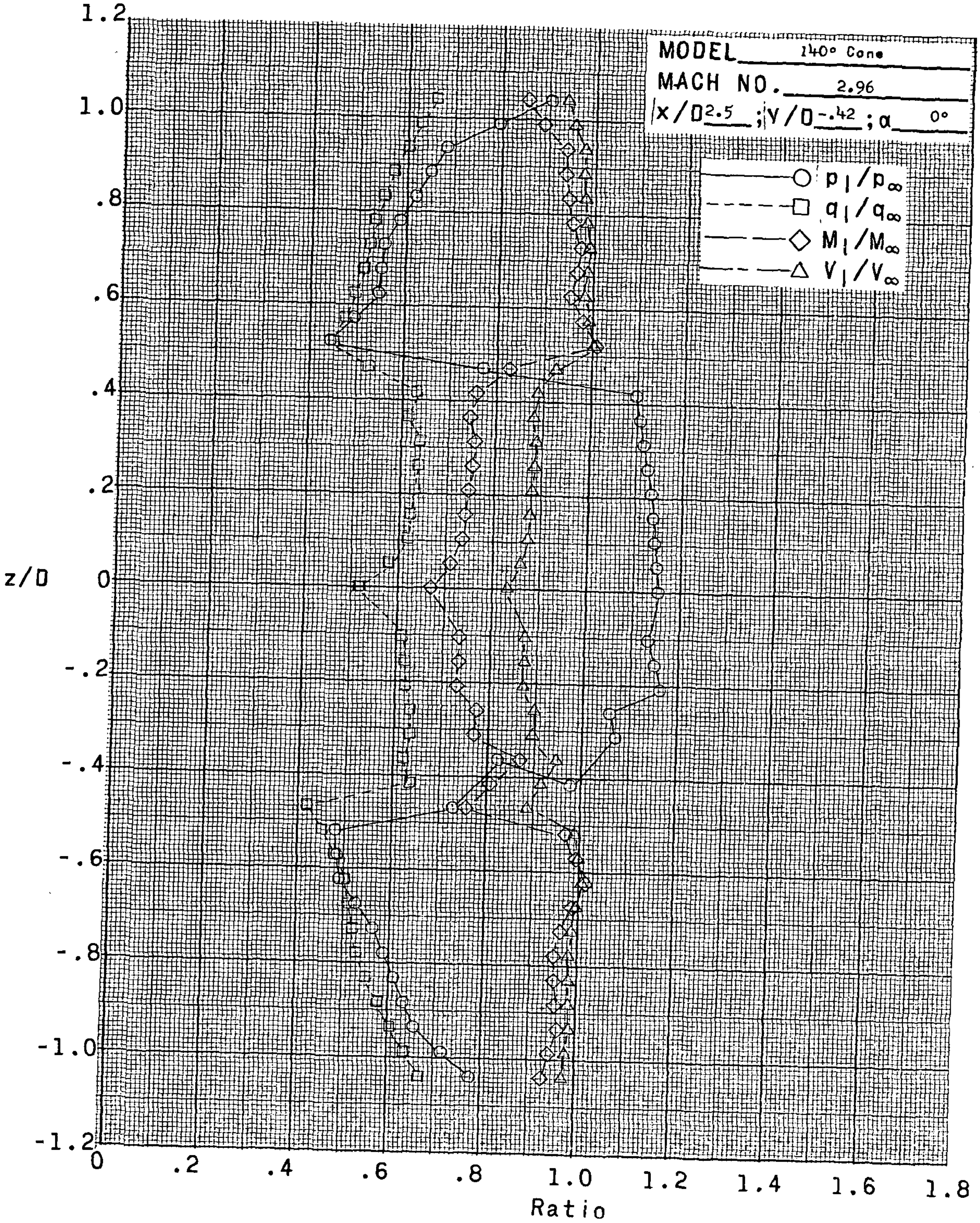
(k) $x/D = 2.5$; $y/D = 0.21$; $\alpha = 0^0$.

Figure 7.- Continued.



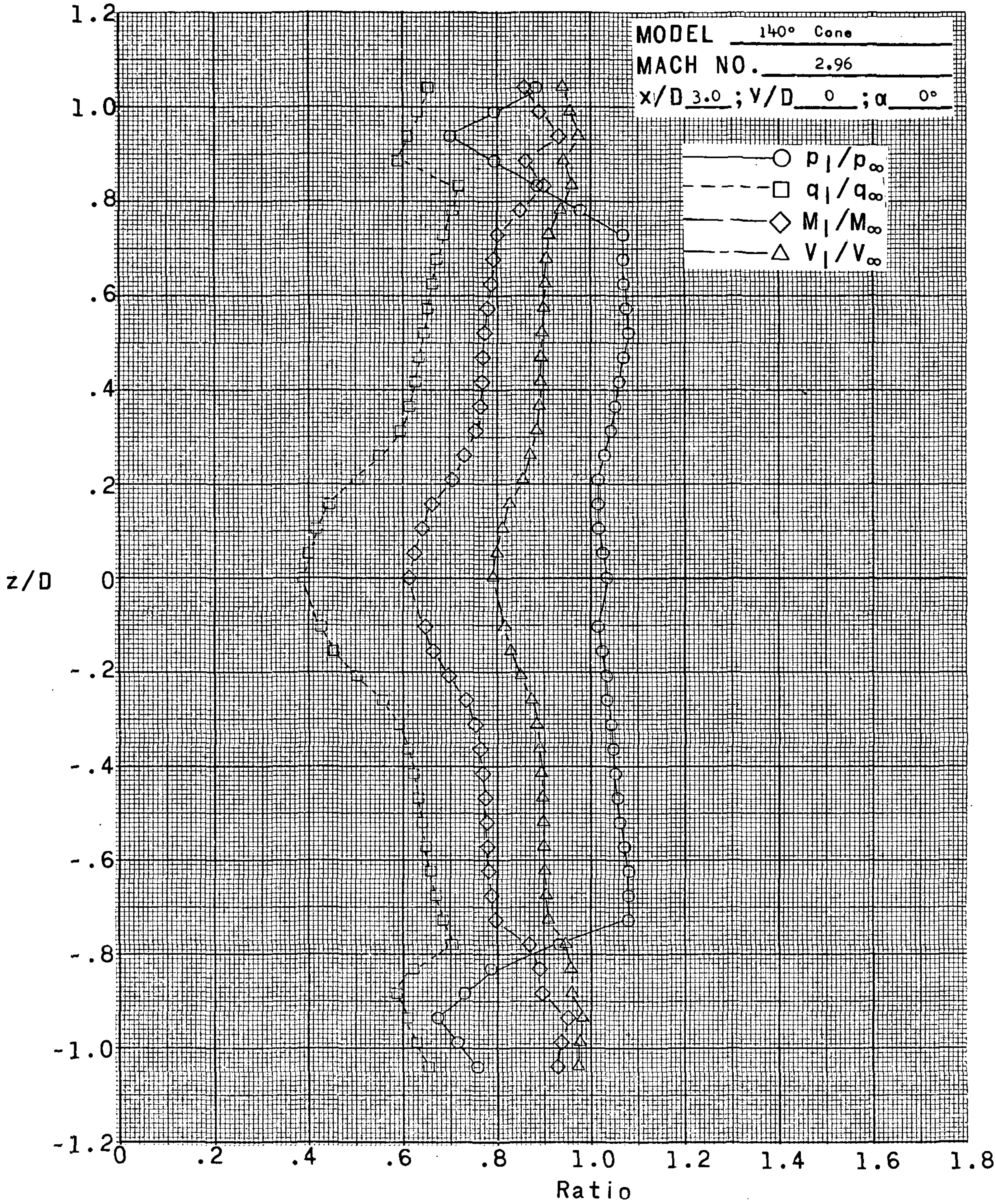
(l) $x/D = 2.5$; $y/D = 0$; $\alpha = 0^0$.

Figure 7.- Continued.



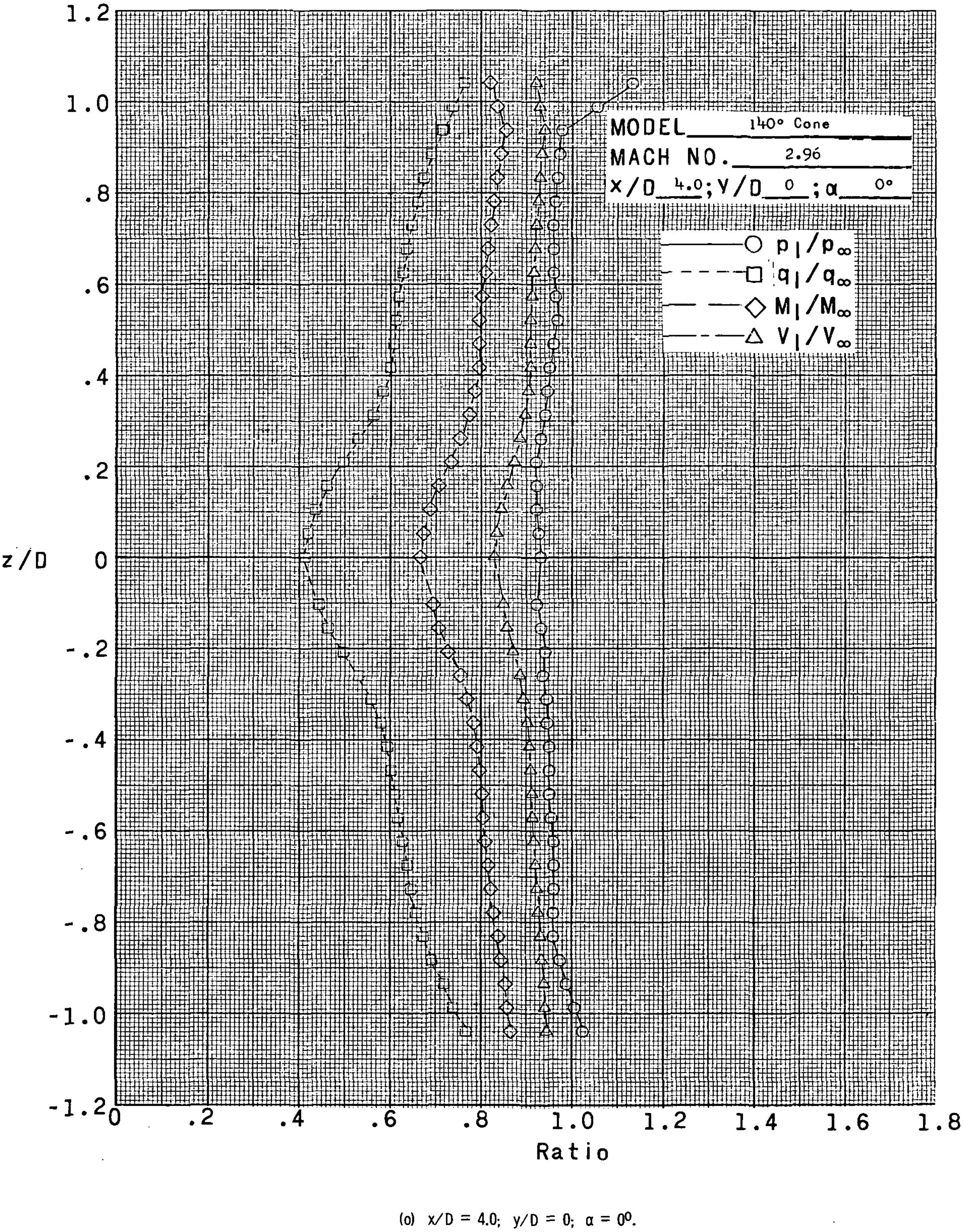
(m) x/D = 2.5; y/D = -0.42; α = 0°.

Figure 7.- Continued.



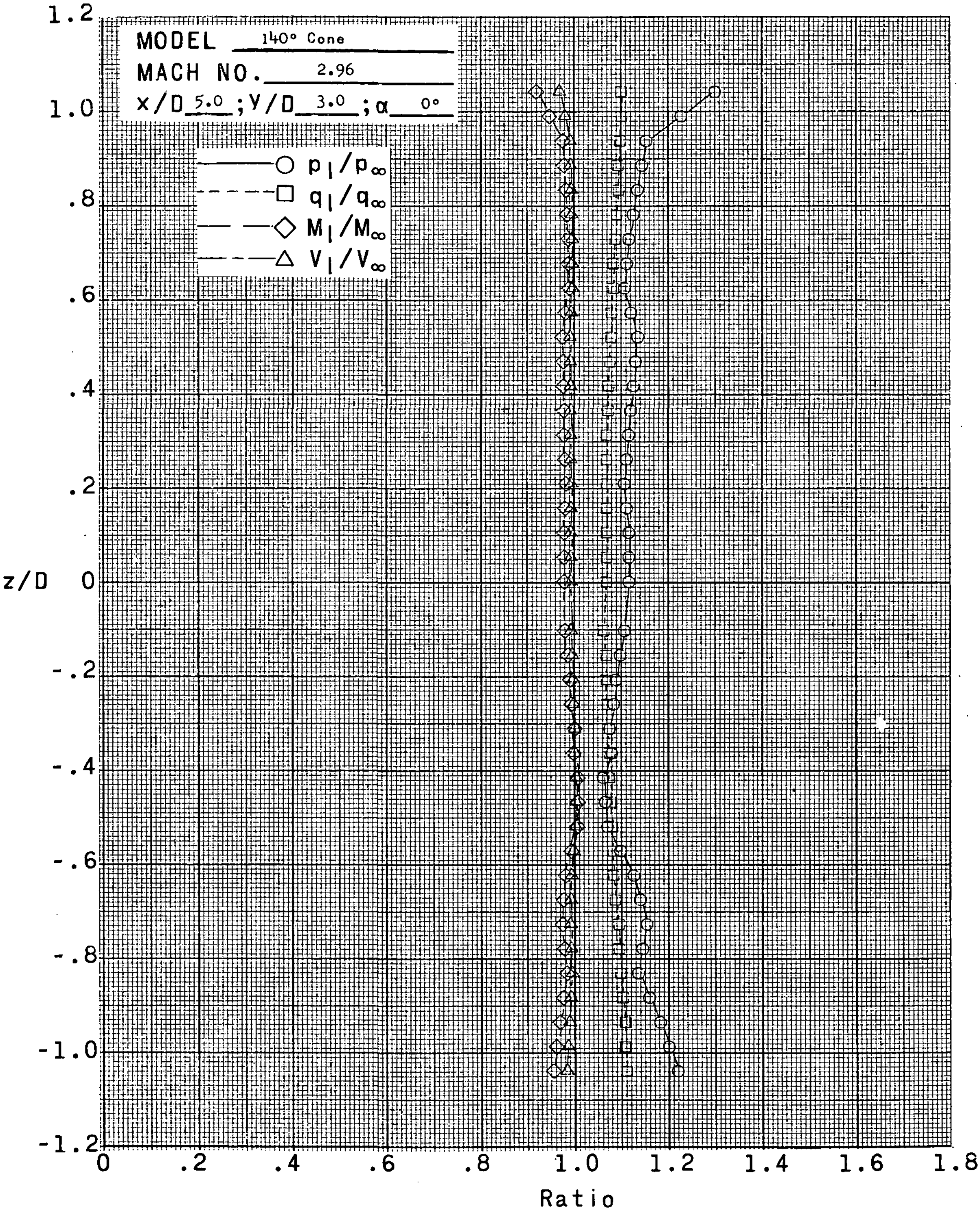
(n) x/D = 3.0; y/D = 0; α = 0°.

Figure 7.- Continued.



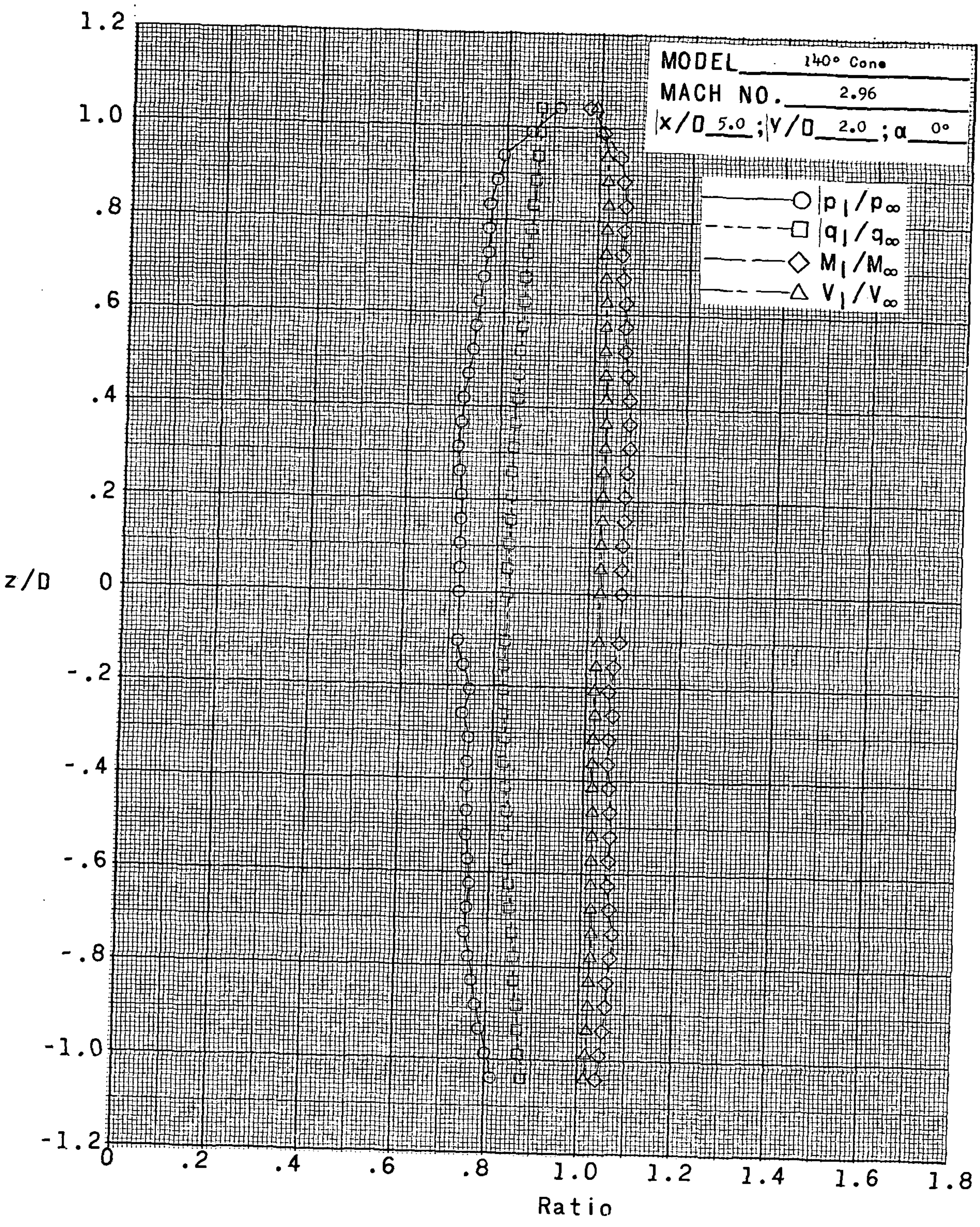
(o) $x/D = 4.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 7.- Continued.



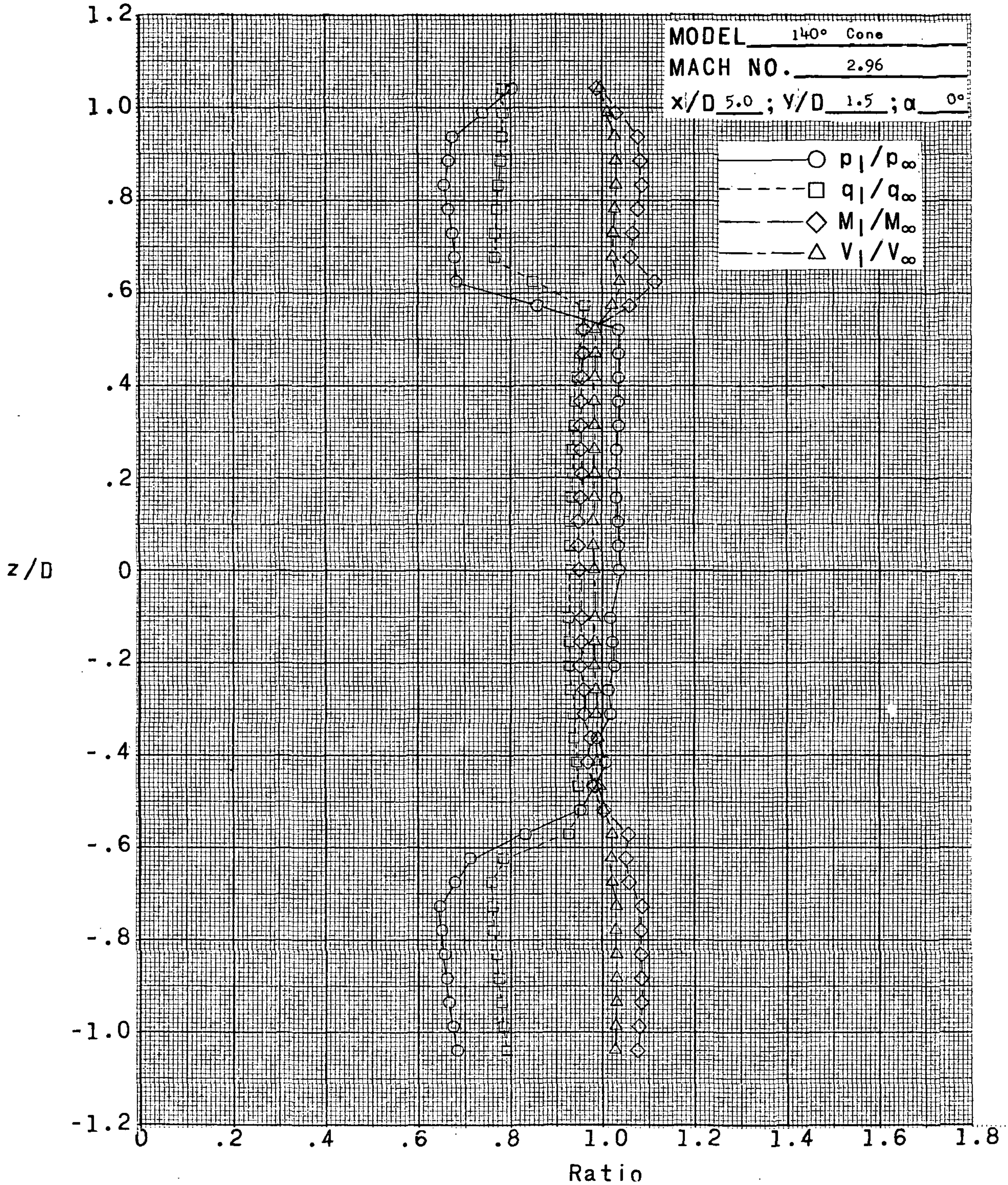
(p) $x/D = 5.0$; $y/D = 3.0$; $\alpha = 0^{\circ}$.

Figure 7.- Continued.



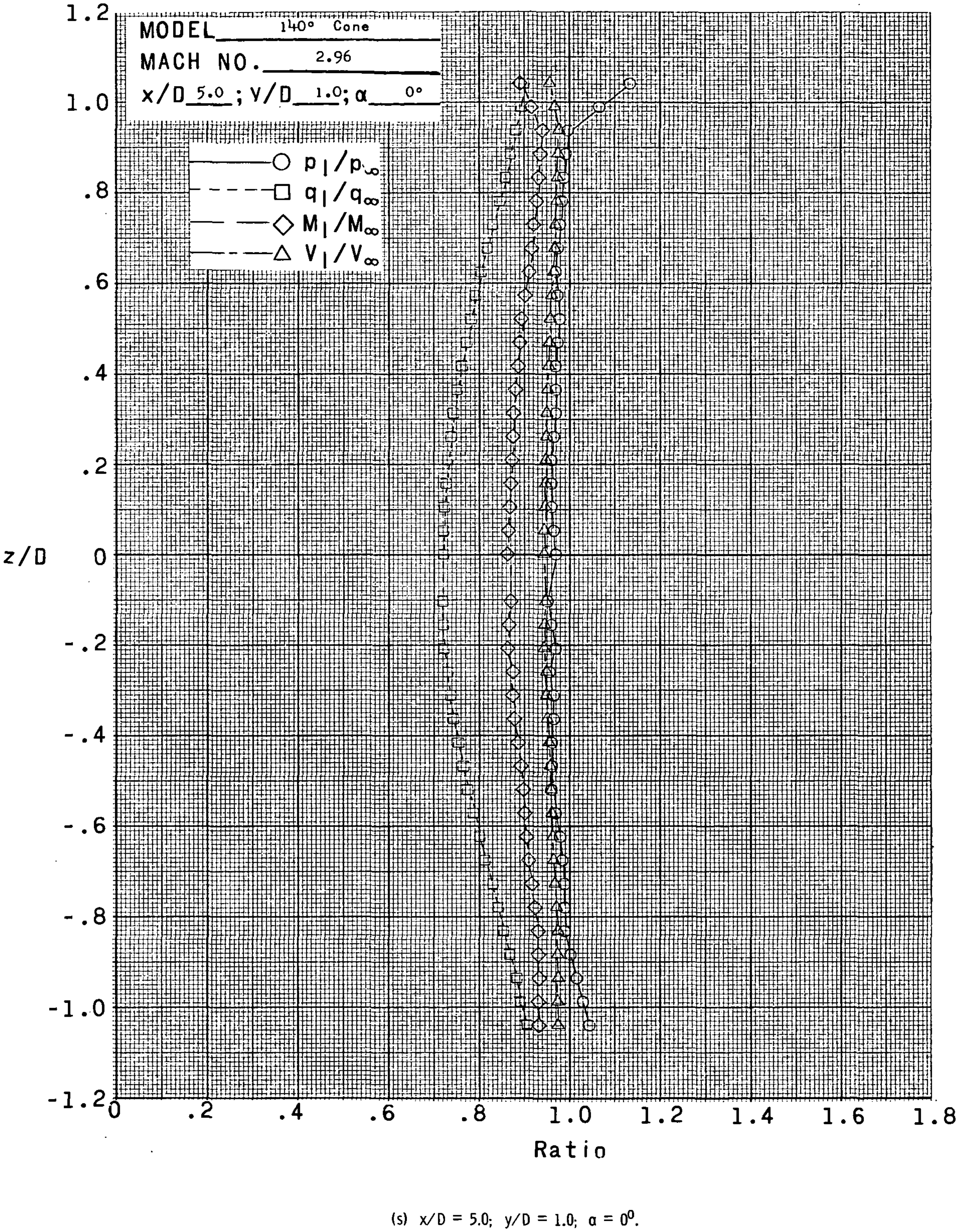
(q) $x/D = 5.0$; $y/D = 2.0$; $\alpha = 0^o$.

Figure 7.- Continued.



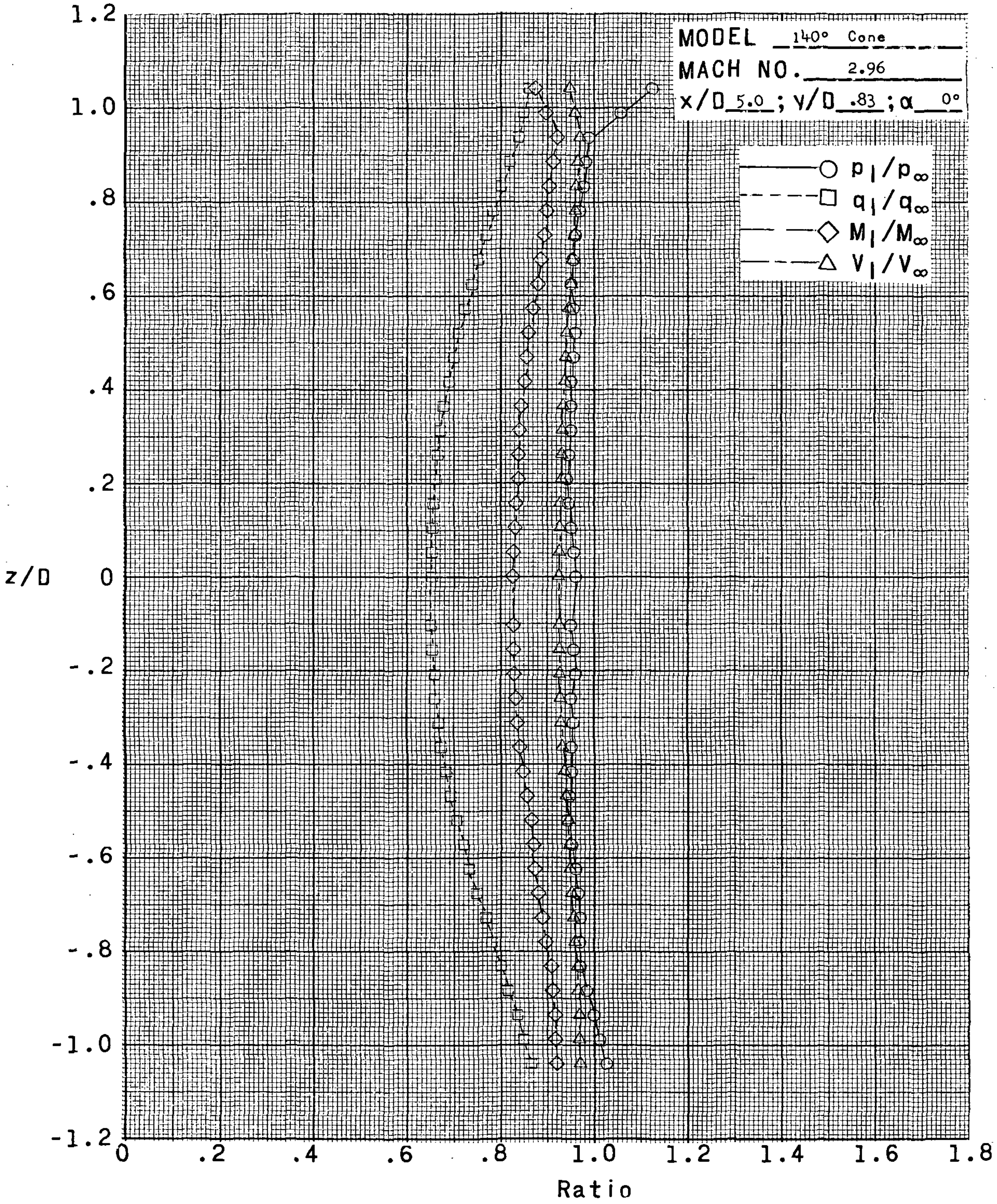
(r) $x/D = 5.0$; $y/D = 1.5$; $\alpha = 0^{o}$.

Figure 7.- Continued.



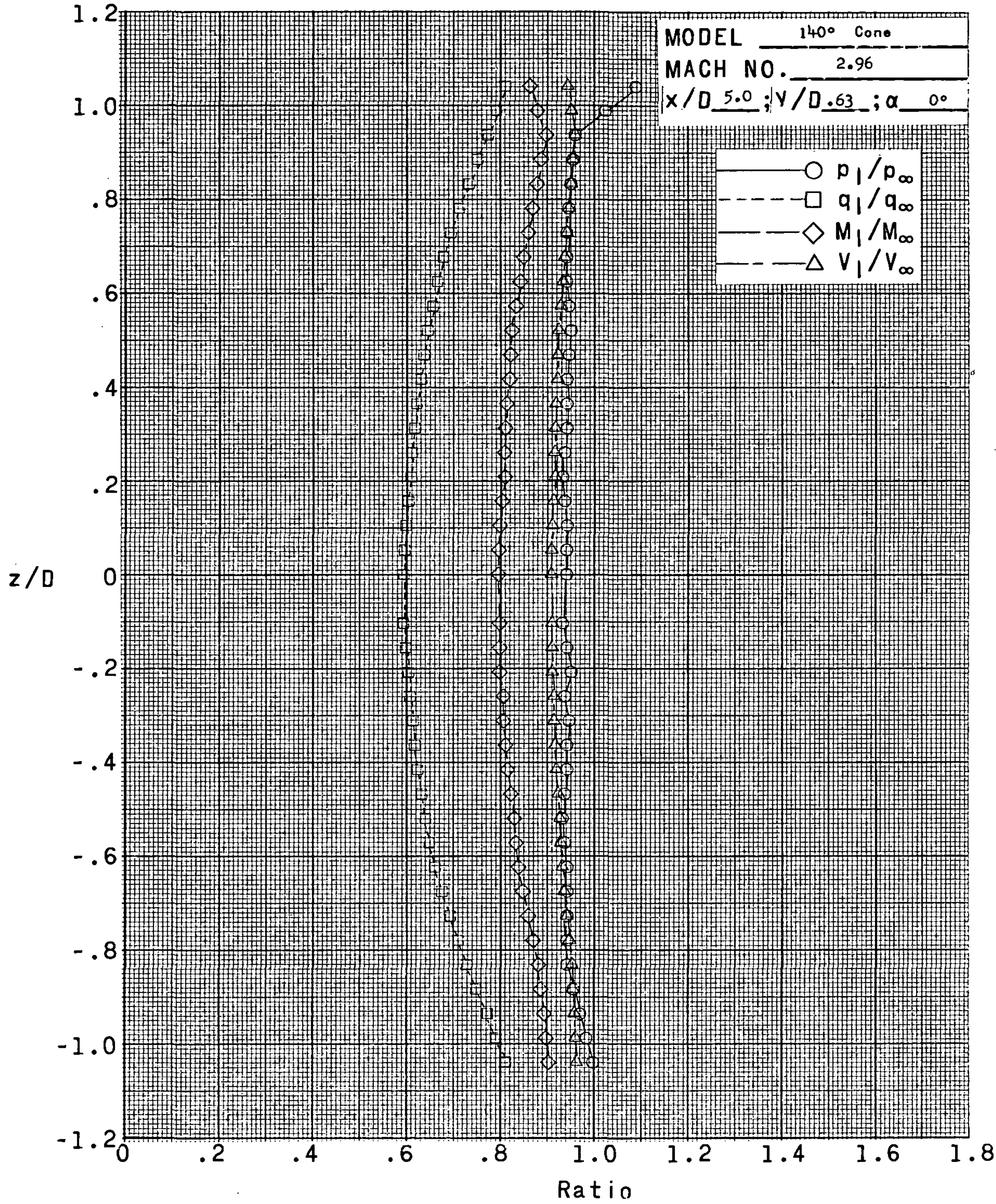
(s) $x/D = 5.0$; $y/D = 1.0$; $\alpha = 0^0$.

Figure 7.- Continued.



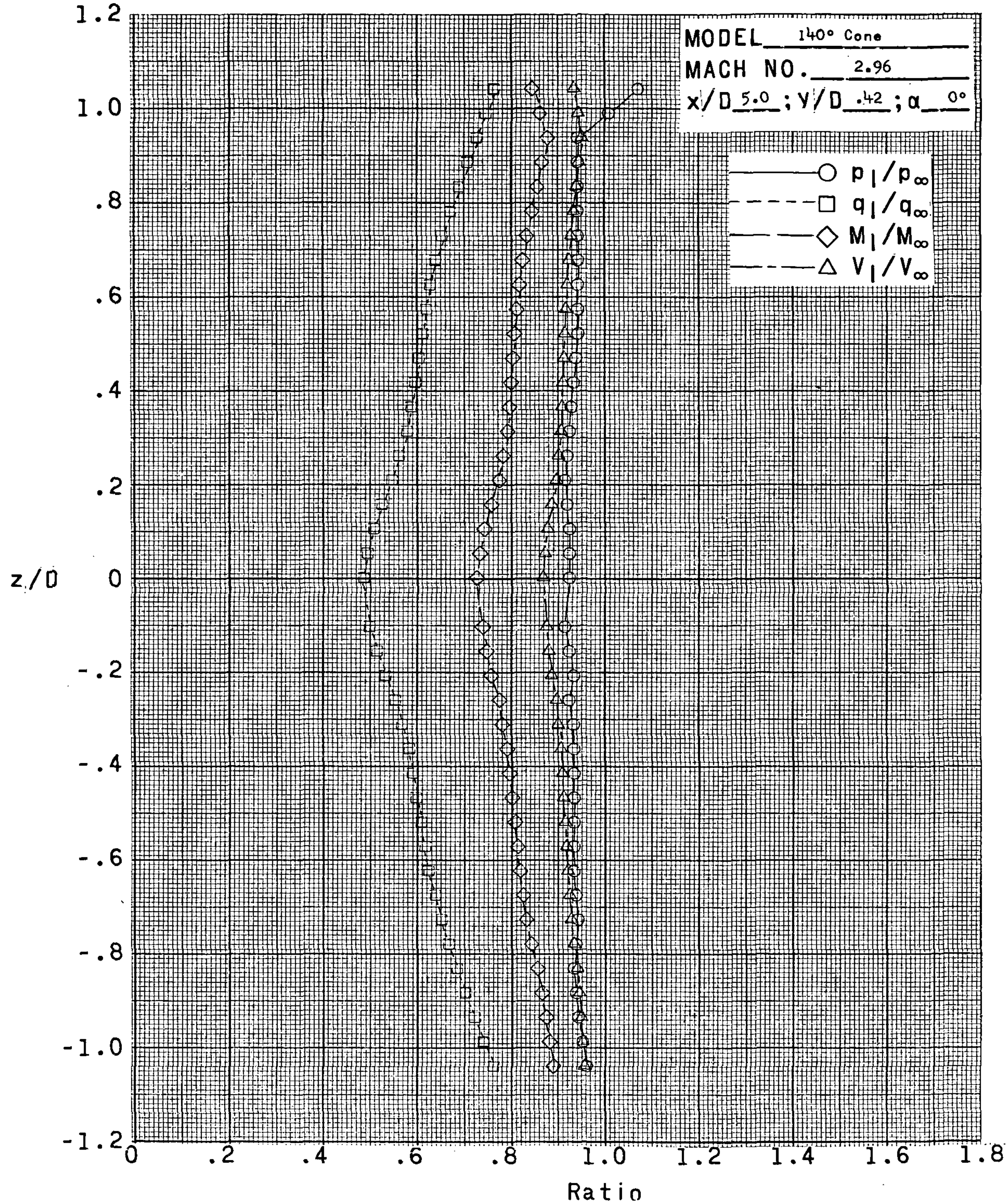
(t) x/D = 5.0; y/D = 0.83; α = 0°.

Figure 7.- Continued.



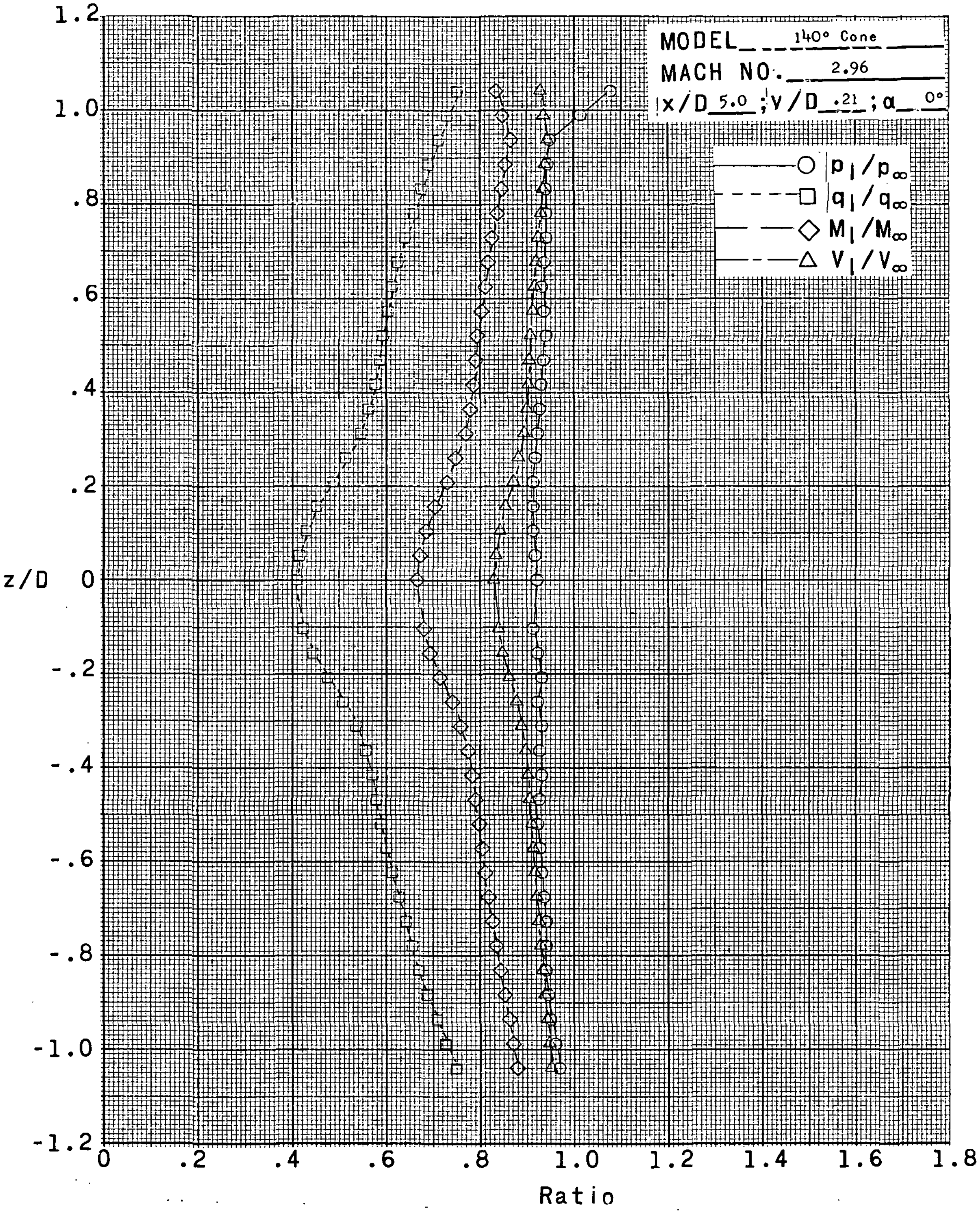
(u) x/D = 5.0; y/D = 0.63; α = 0°.

Figure 7.- Continued.



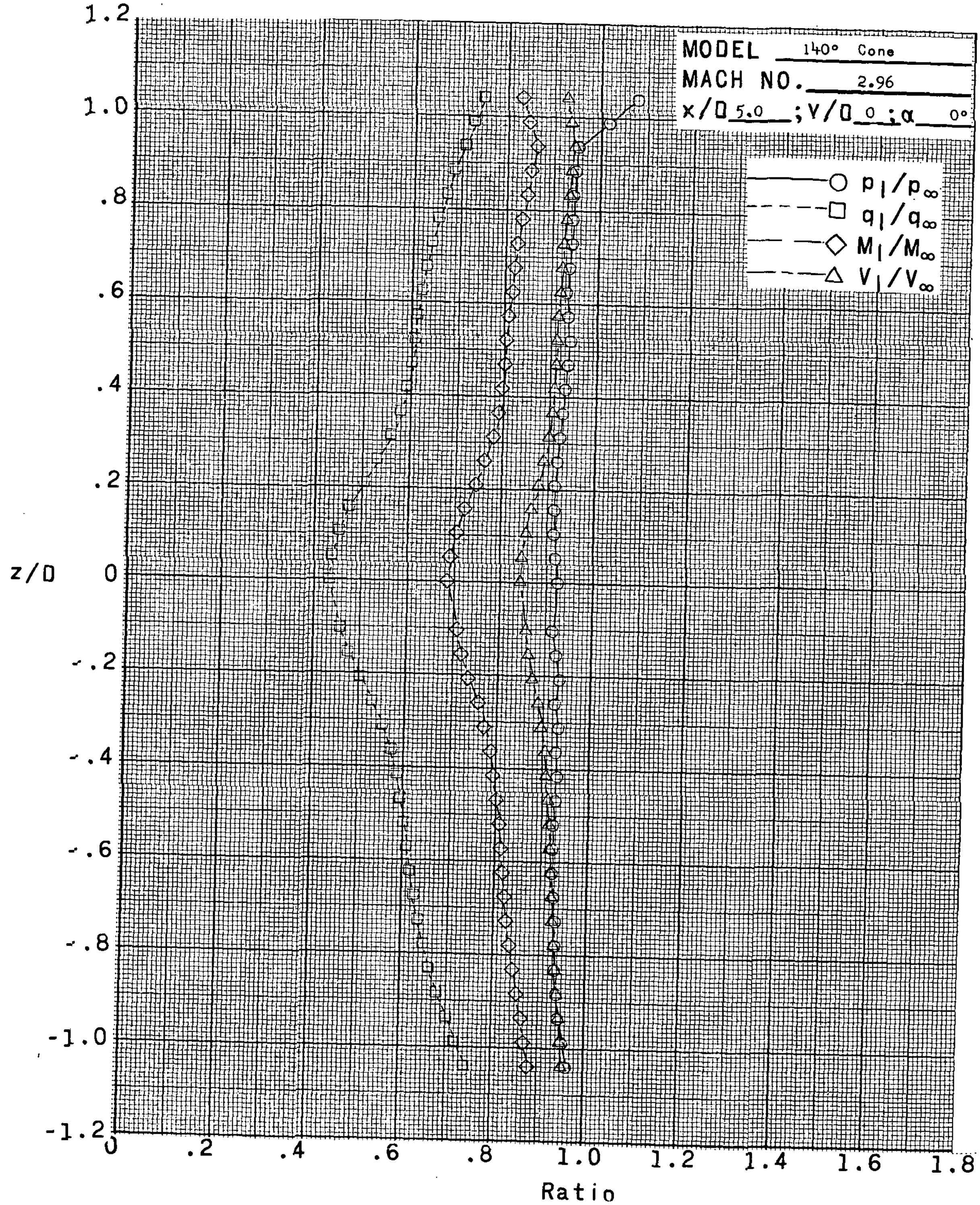
(v) $x/D = 5.0$; $y/D = 0.42$; $\alpha = 0^0$.

Figure 7.- Continued.



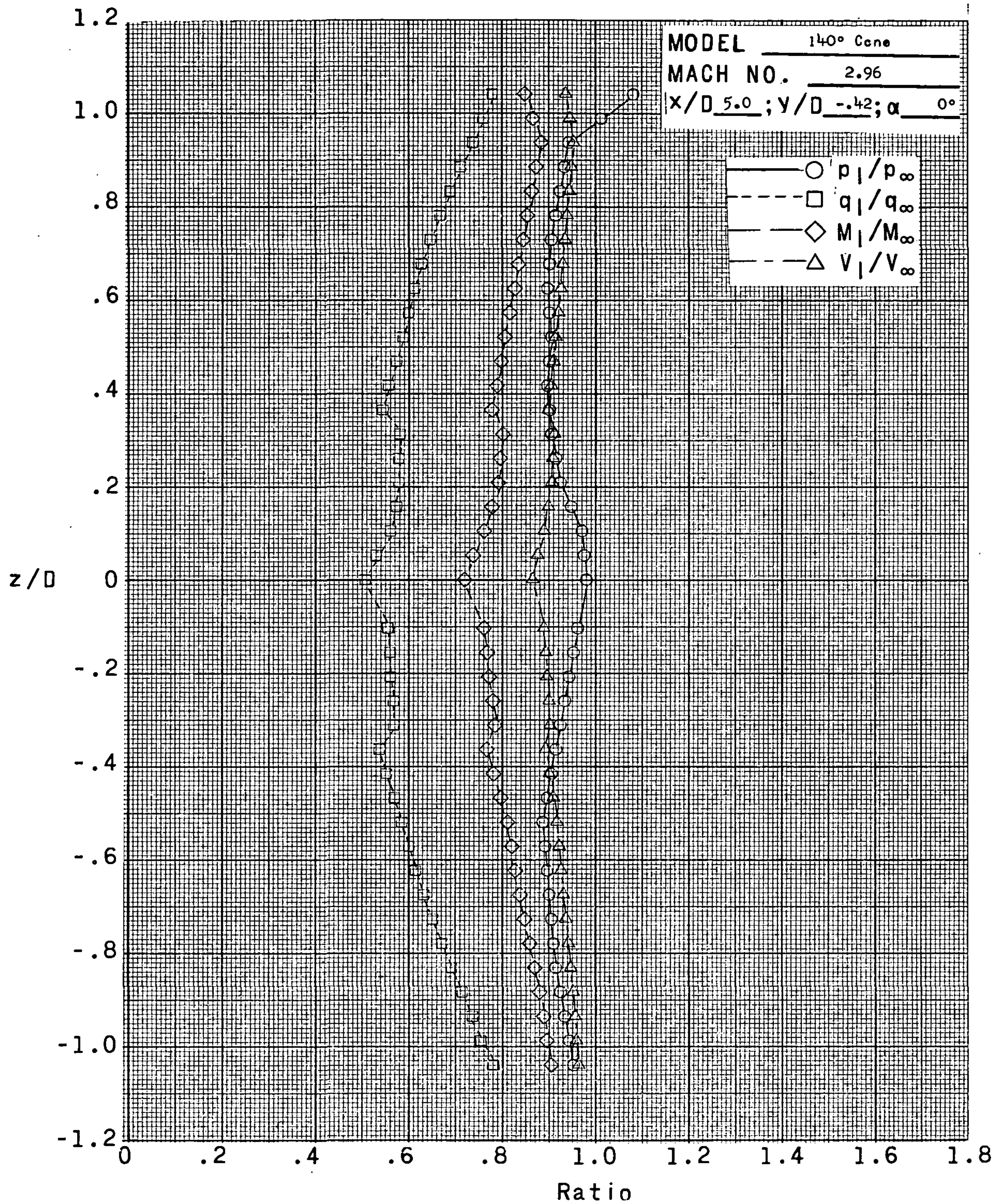
(w) x/D = 5.0; y/D = 0.21; α = 0°.

Figure 7.- Continued.



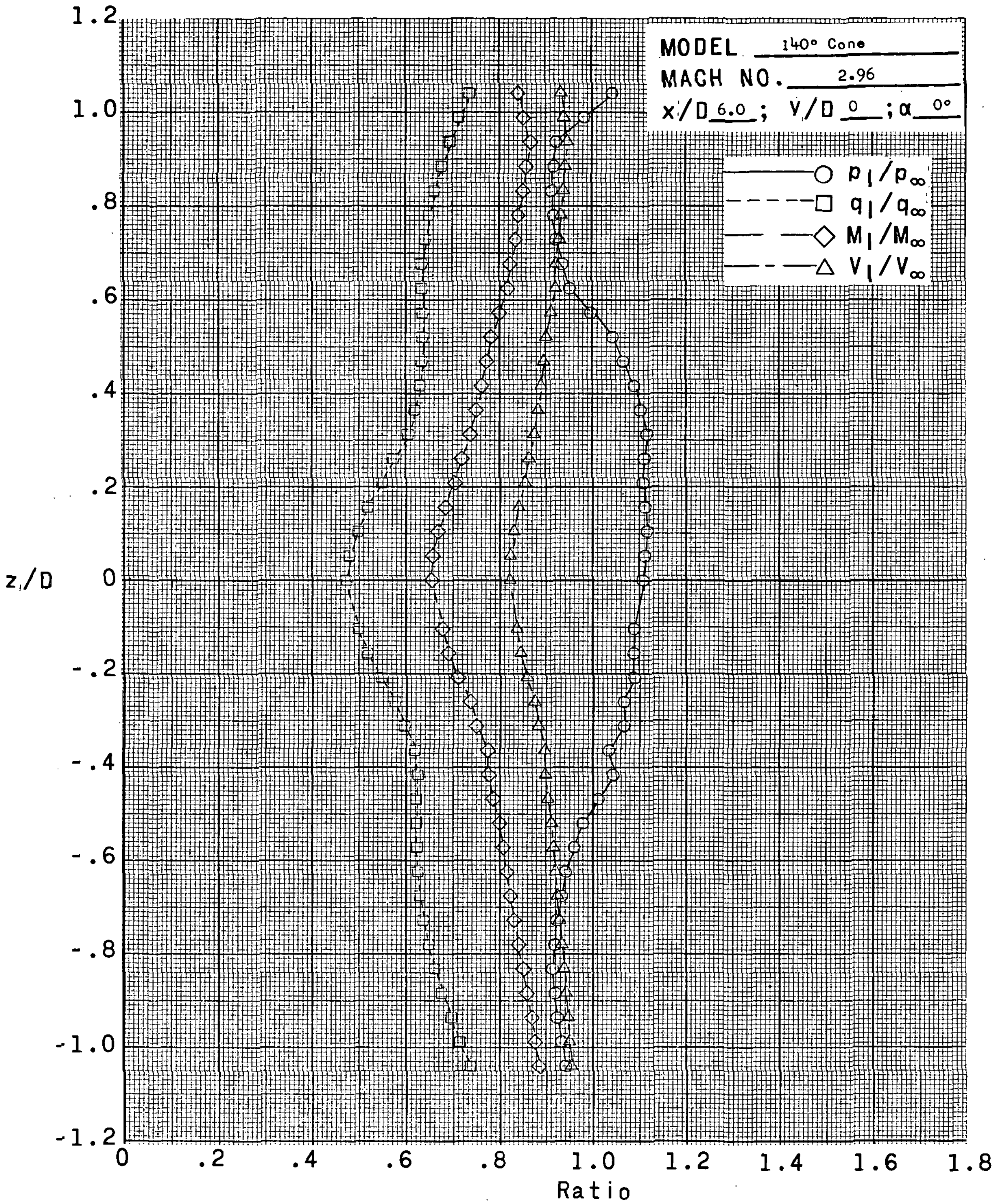
(x) x/D = 5.0; y/D = 0; α = 0°.

Figure 7.- Continued.



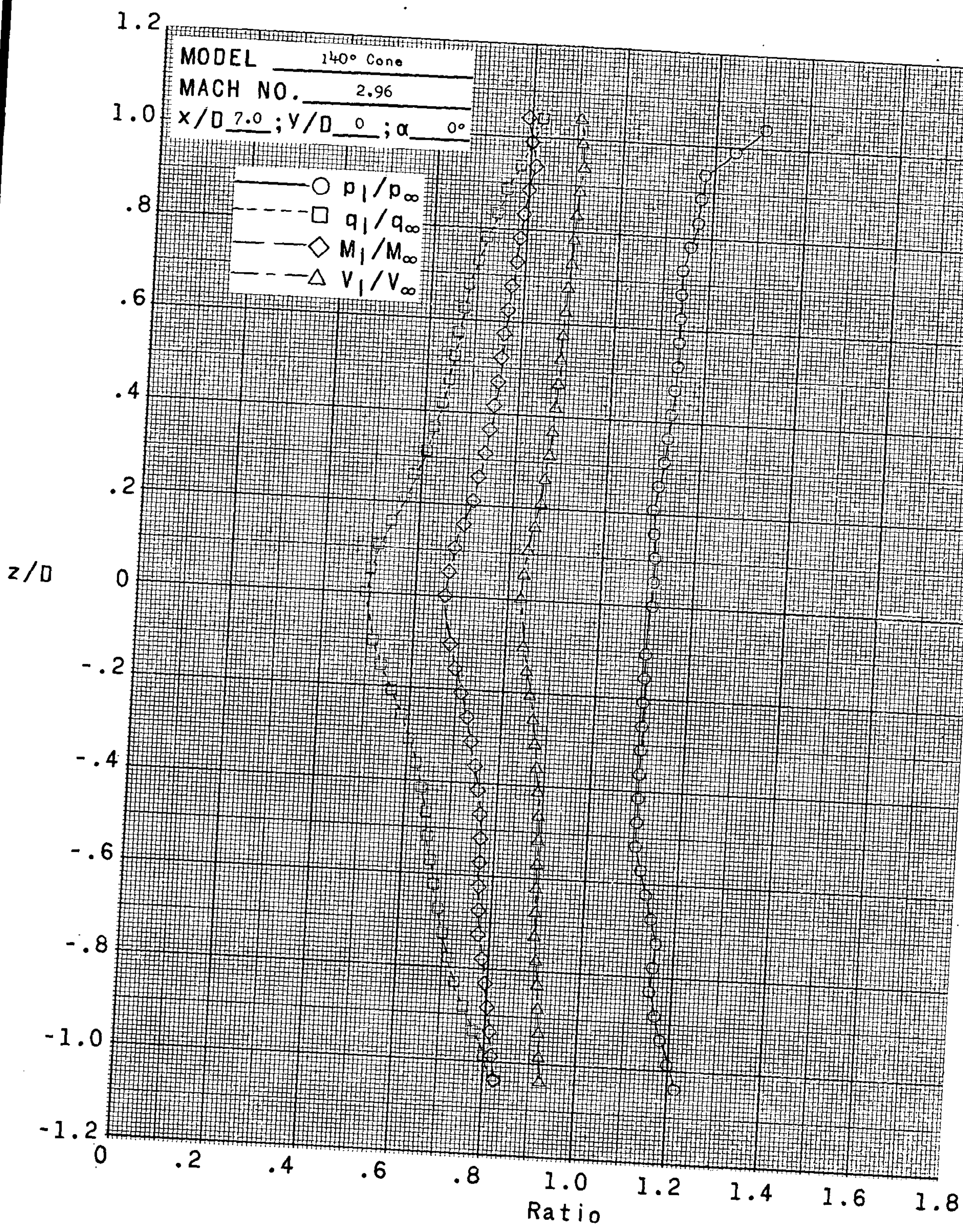
(y) x/D = 5.0; y/D = -0.42; α = 0°.

Figure 7.- Continued.



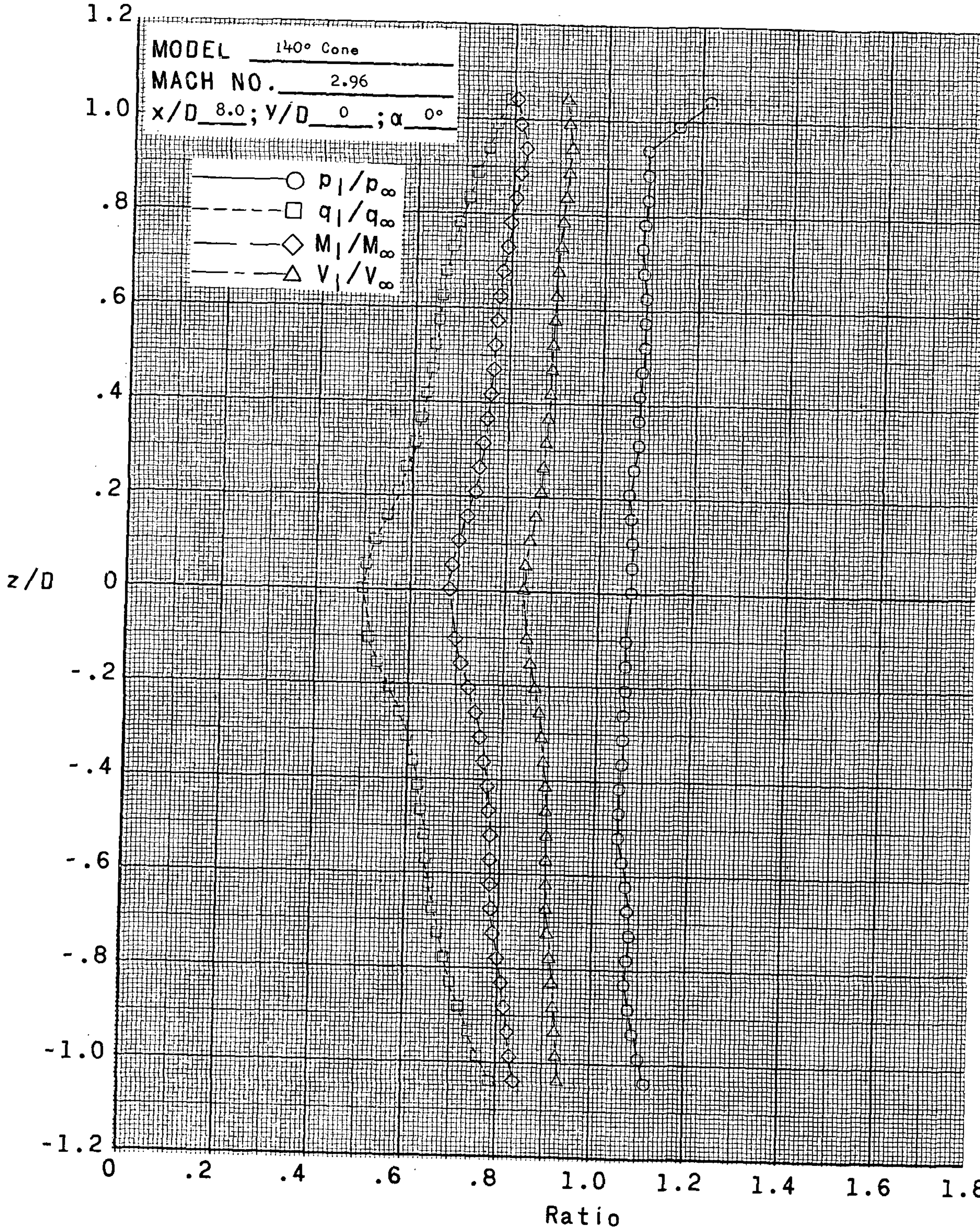
(z) $x/D = 6.0$; $y/D = 0$; $\alpha = 0^{0}$.

Figure 7.- Continued.



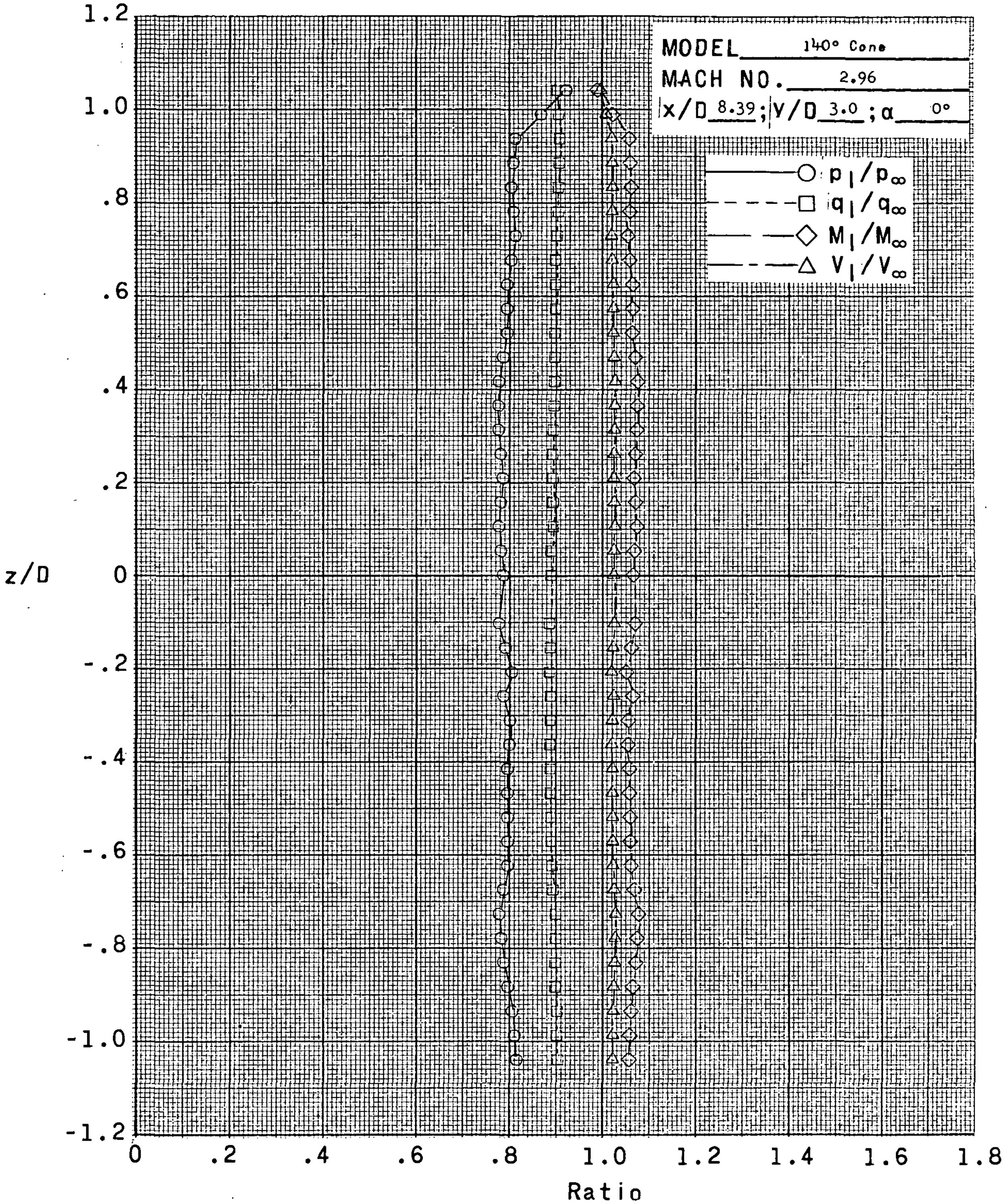
(aa) $x/D = 7.0$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 7.- Continued.



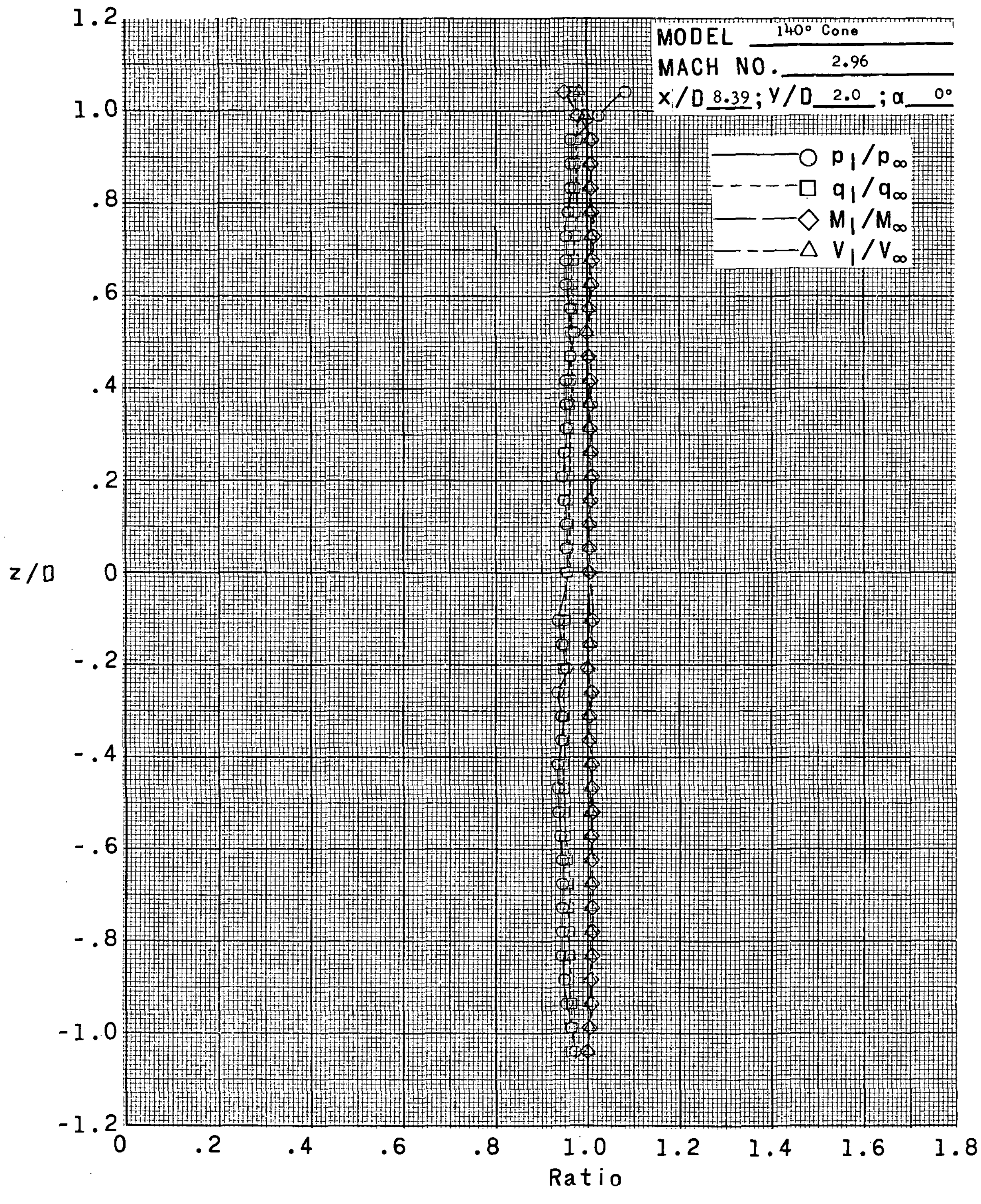
(bb) $x/D = 8.0$; $y/D = 0$; $\alpha = 0°$.

Figure 7.- Continued.



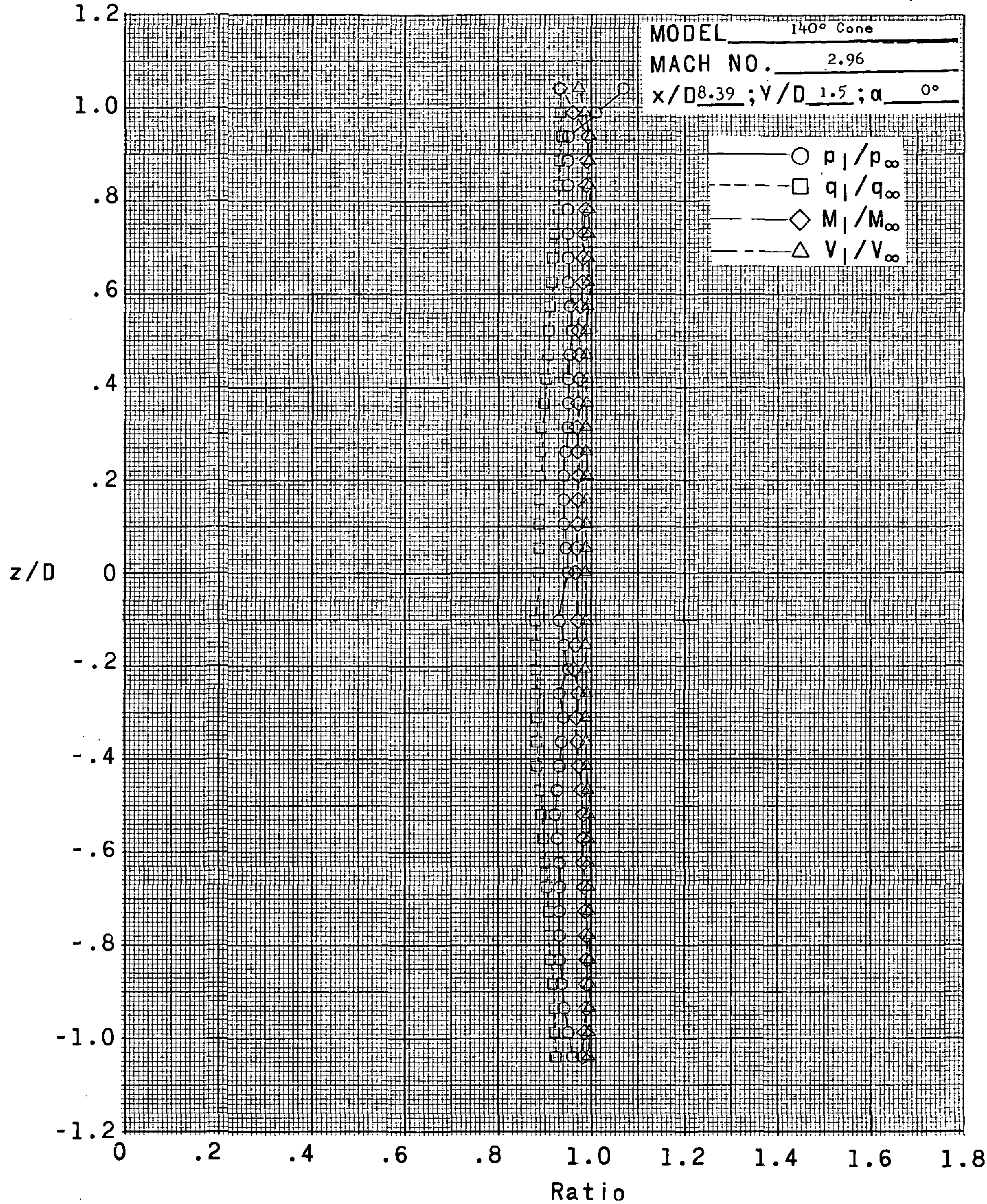
(cc) $x/D = 8.39$; $y/D = 3.0$; $\alpha = 0^{\circ}$.

Figure 7.- Continued.



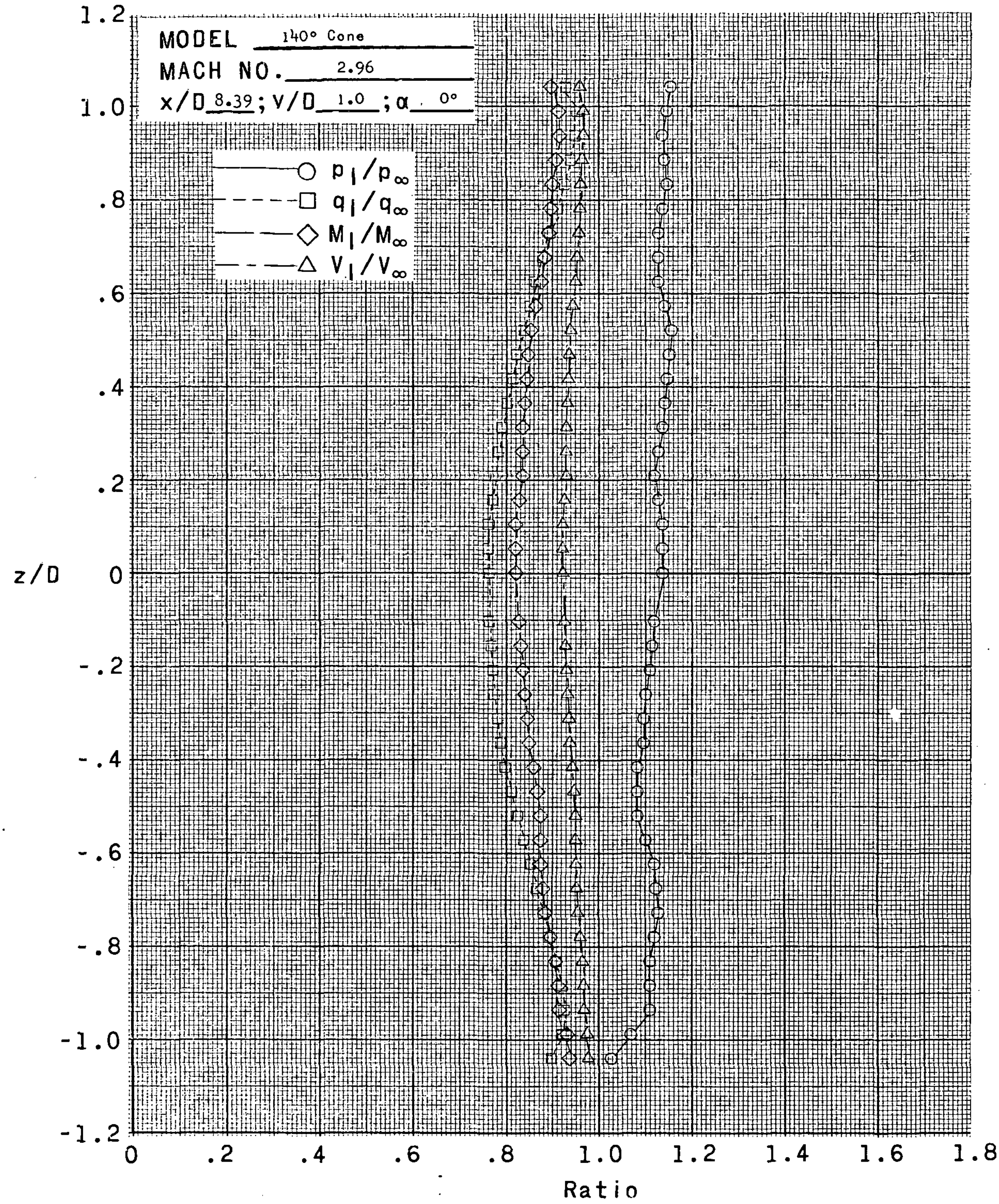
(dd) x/D = 8.39; y/D = 2.0; α = 0°.

Figure 7.- Continued.



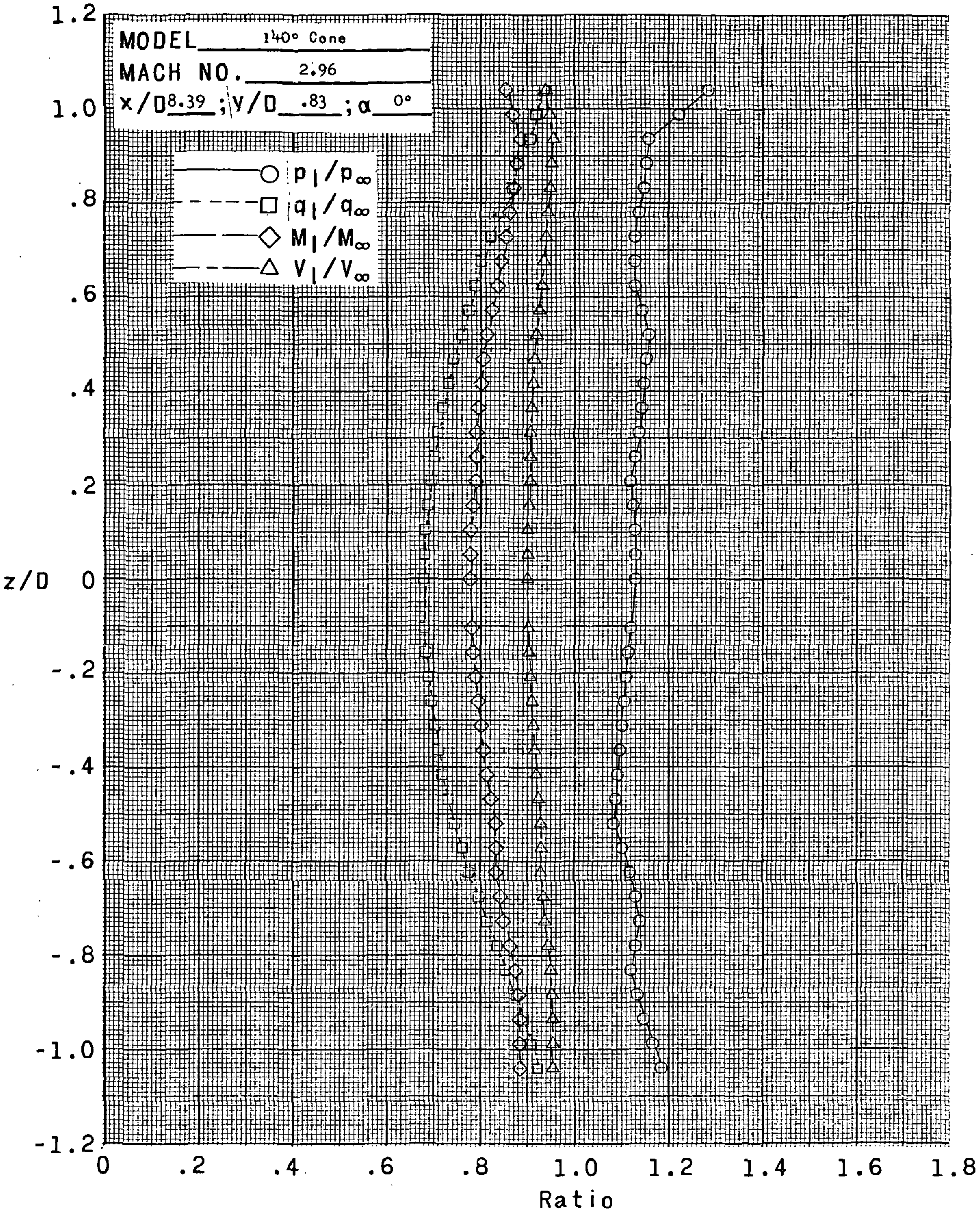
(ee) x/D = 8.39; y/D = 1.5; α = 0°.

Figure 7.- Continued.



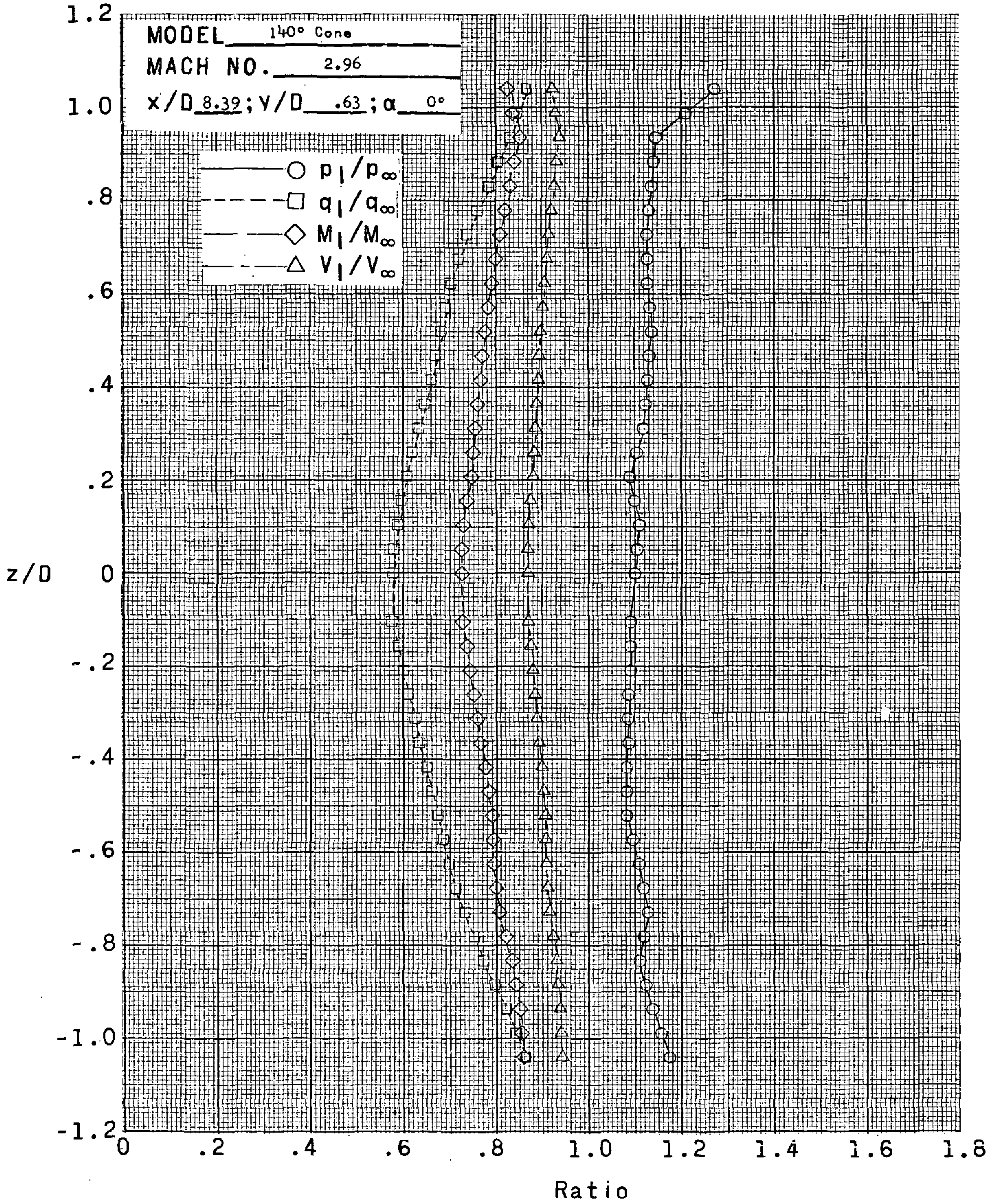
(ff) $x/D = 8.39$; $y/D = 1.0$; $\alpha = 0^0$.

Figure 7.- Continued.



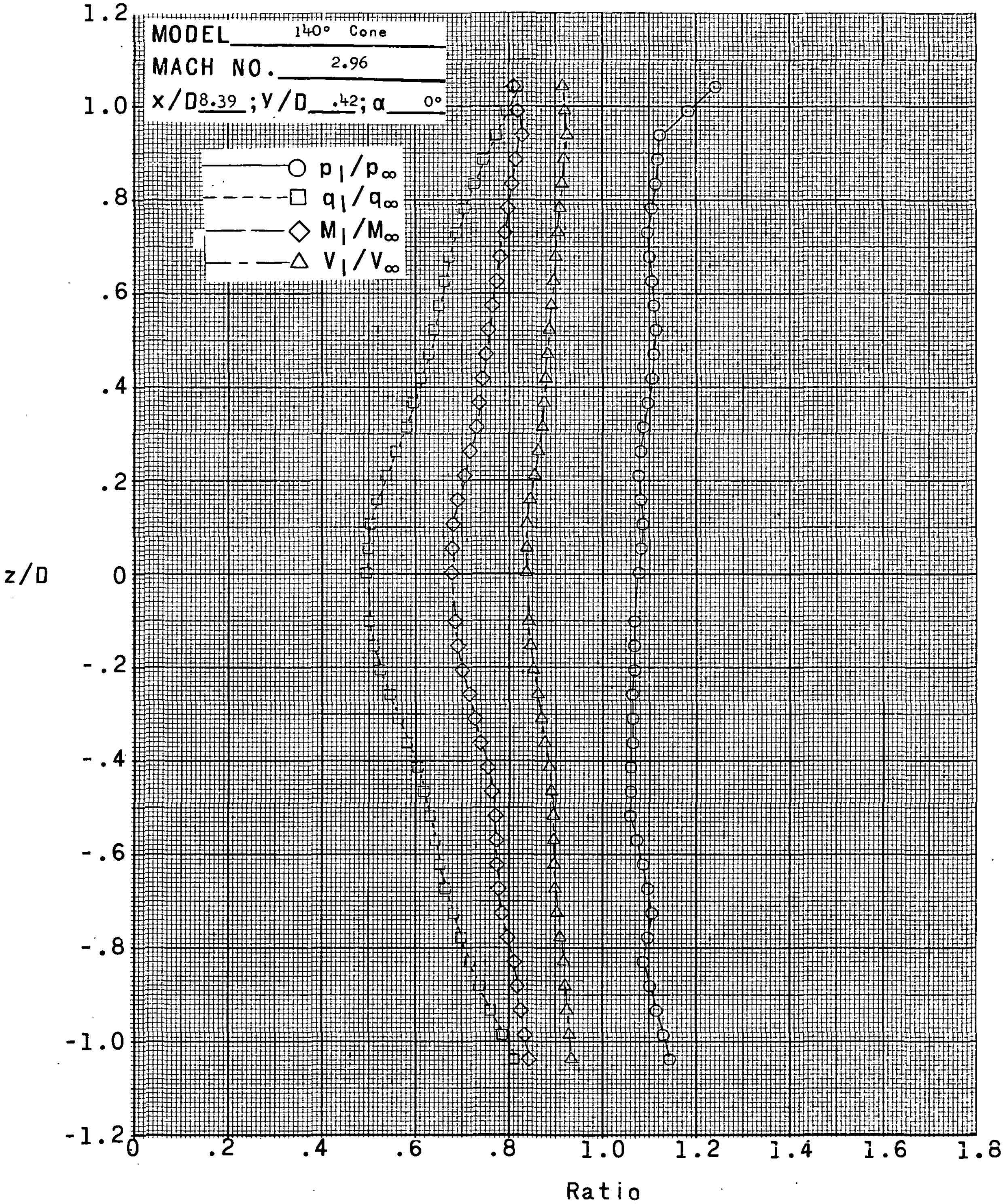
(gg) x/D = 8.39; y/D = 0.83; α = 0°.

Figure 7.- Continued.



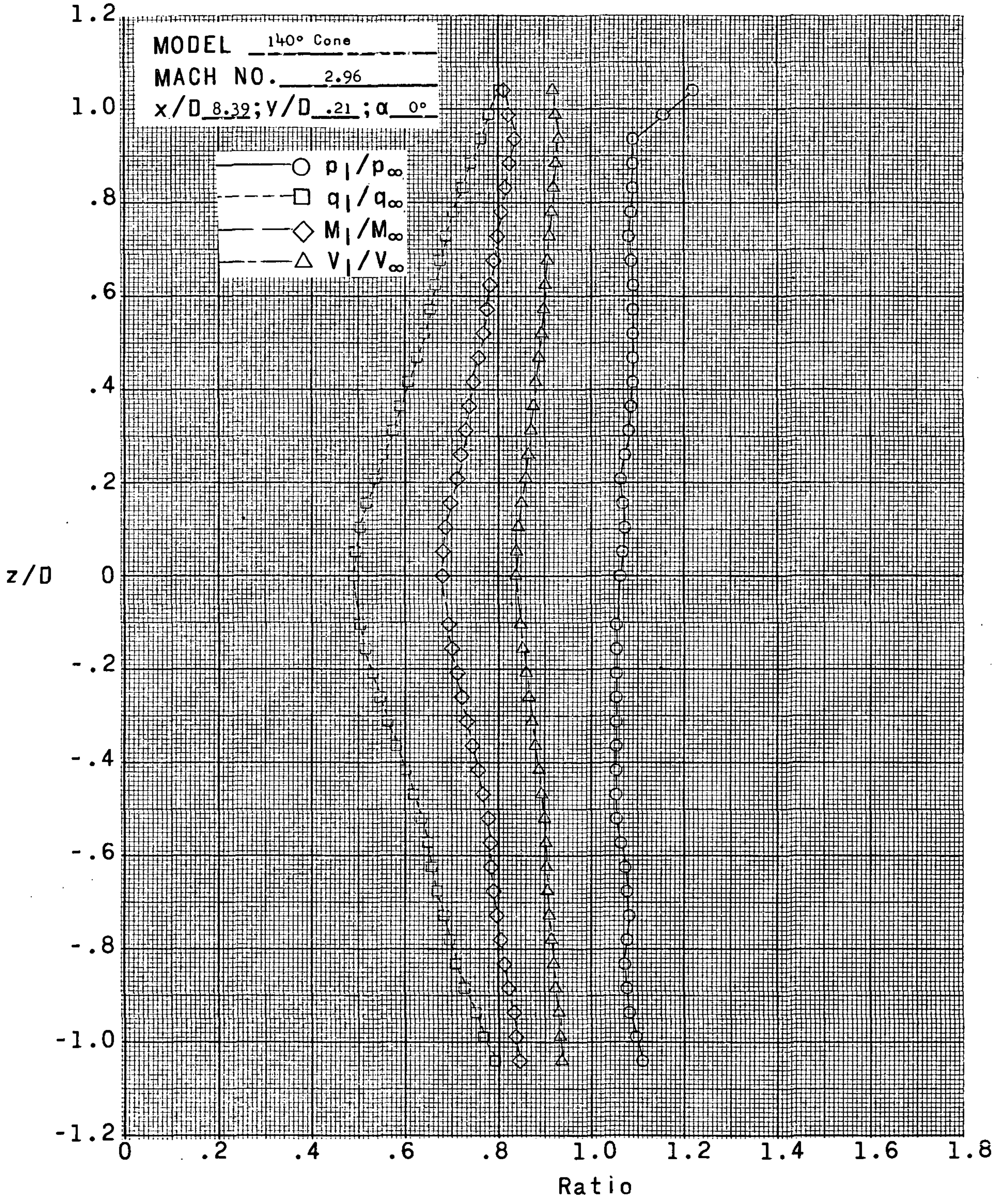
(hh) x/D = 8.39; y/D = 0.63; α = 0°.

Figure 7.- Continued.



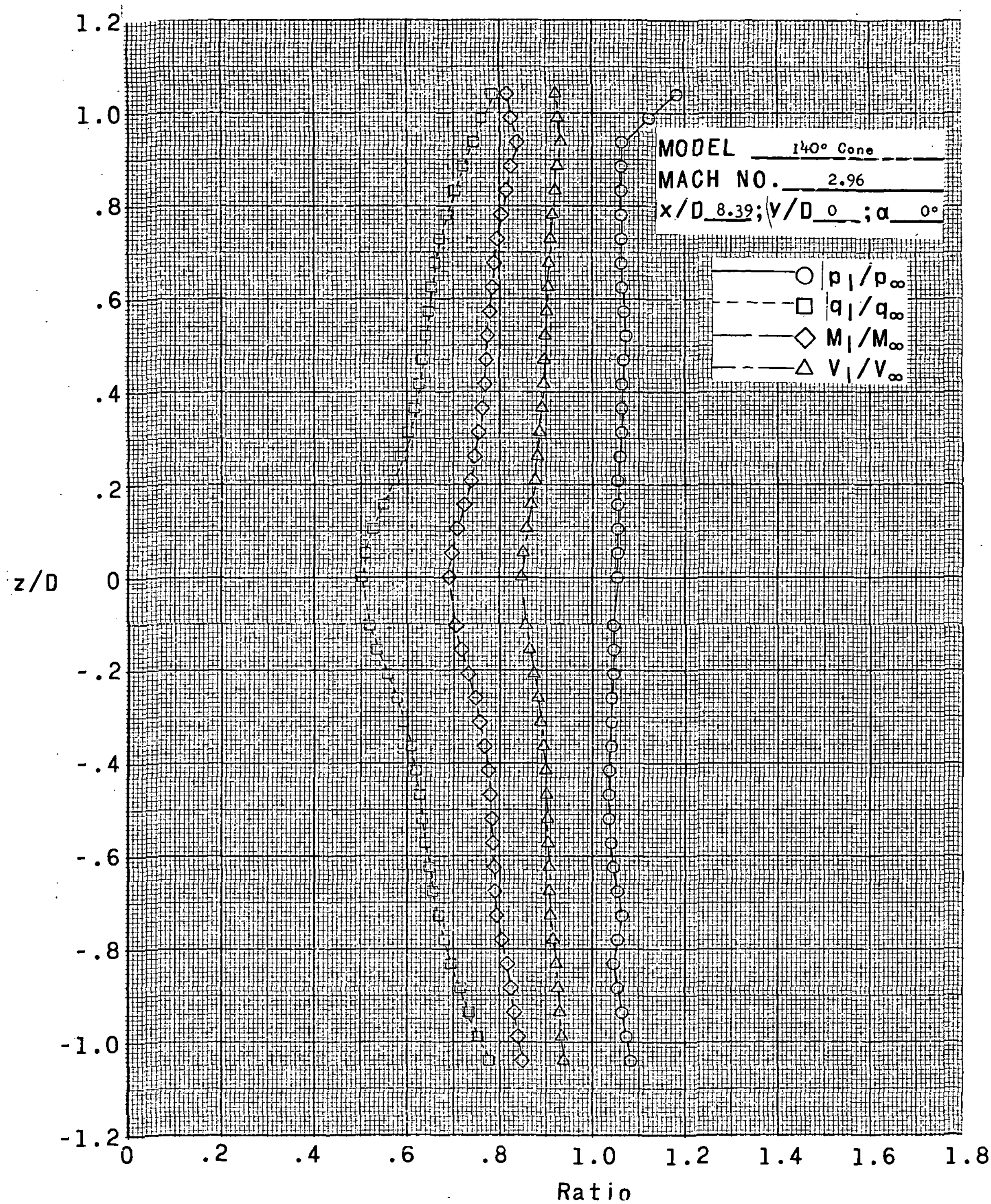
(ii) $x/D = 8.39$; $y/D = 0.42$; $\alpha = 0^{0}$.

Figure 7.- Continued.



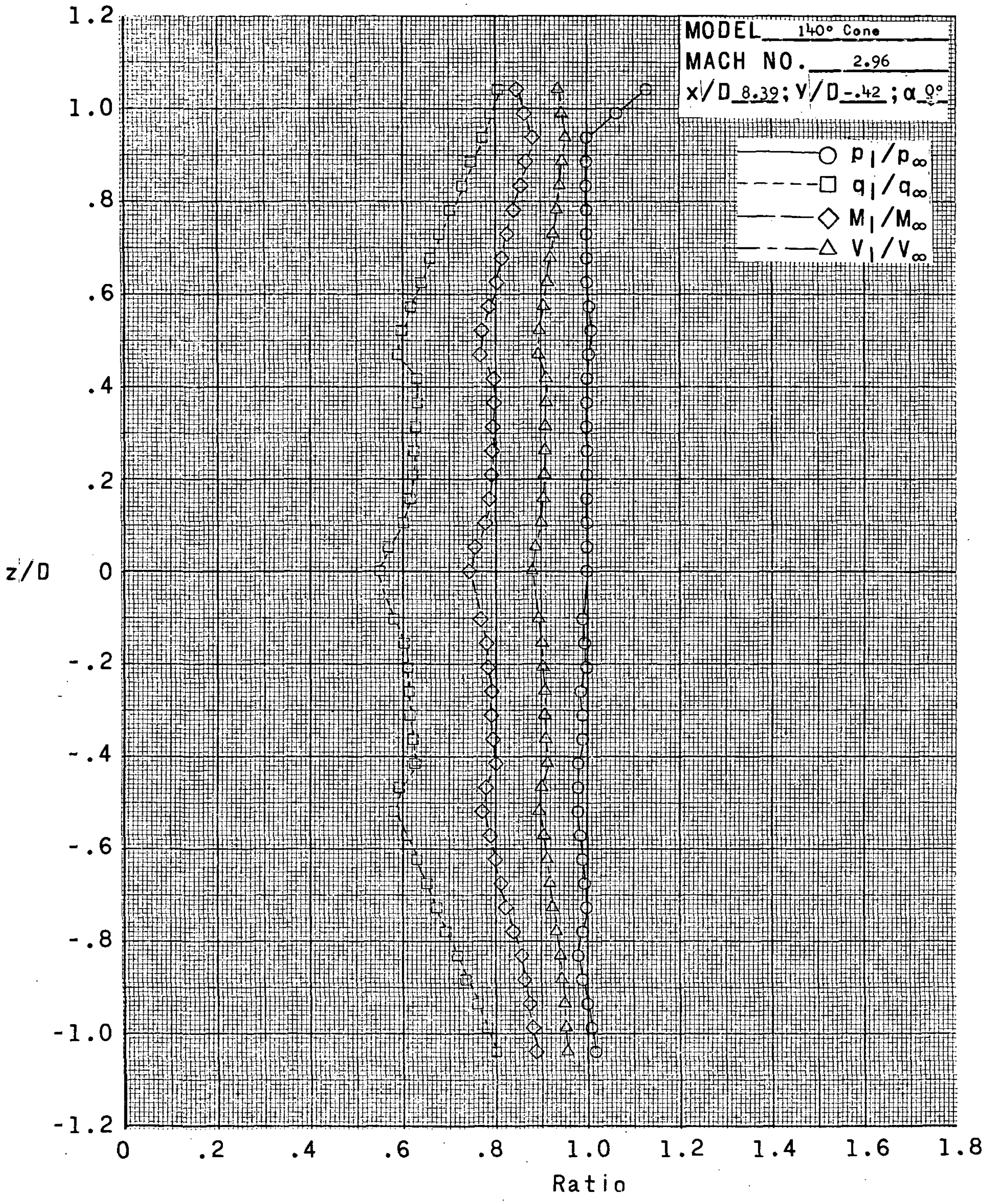
(jj) $x/D = 8.39$; $y/D = 0.21$; $\alpha = 0^0$.

Figure 7.- Continued.



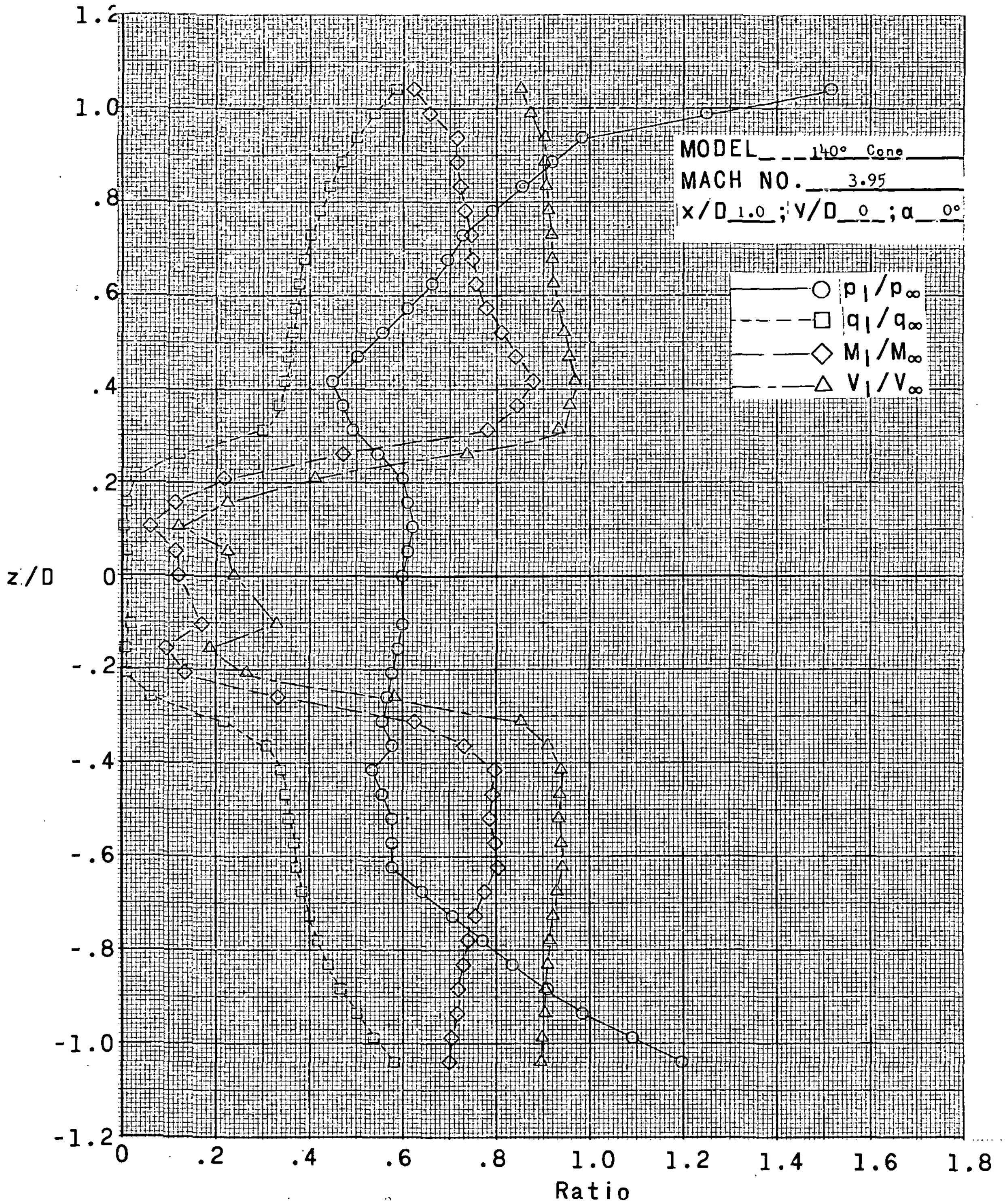
(kk) $x/D = 8.39$; $y/D = 0$; $\alpha = 0^o$.

Figure 7.- Continued.



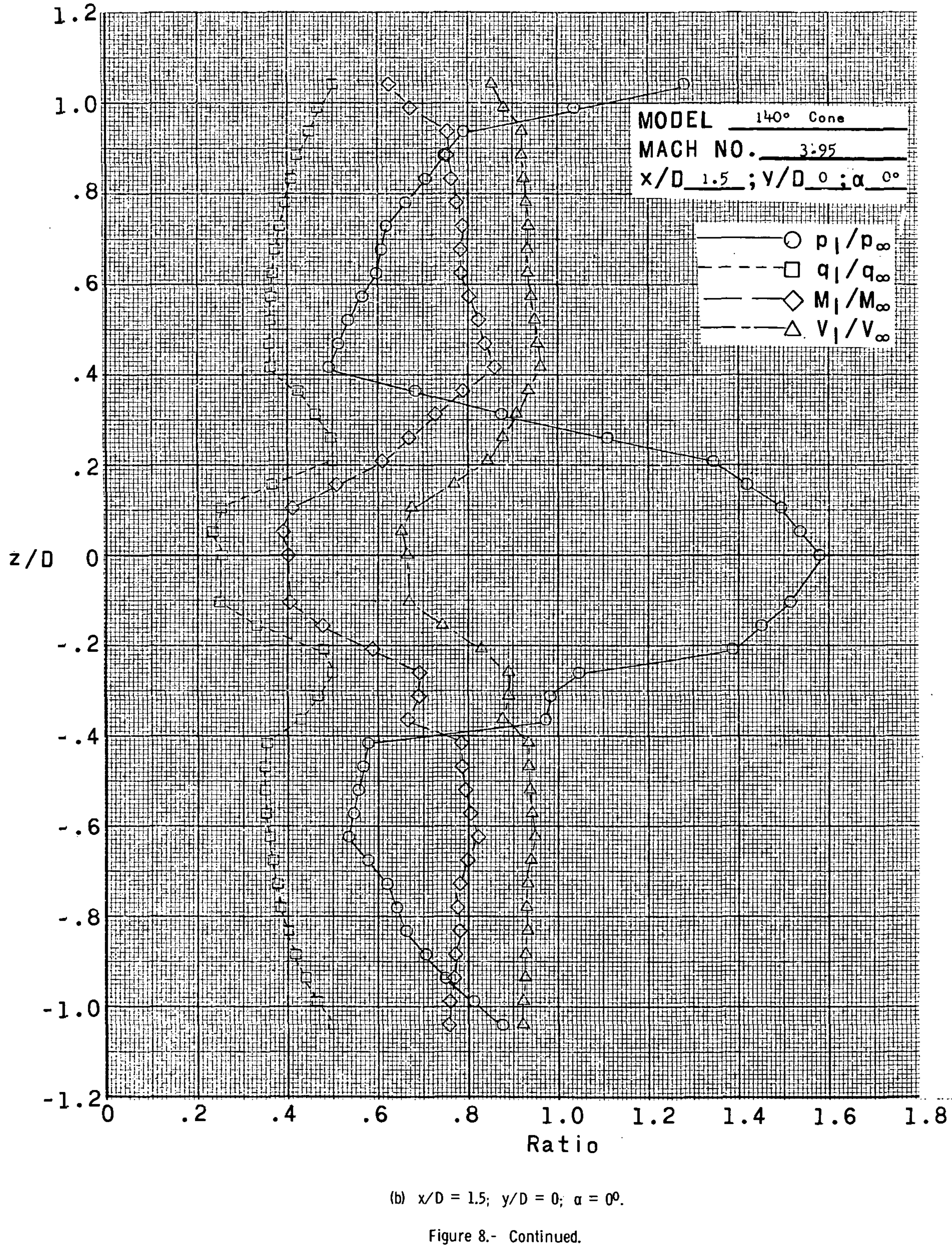
(II) x/D = 8.39; y/D = -0.42; α = 0°.

Figure 7.- Concluded.



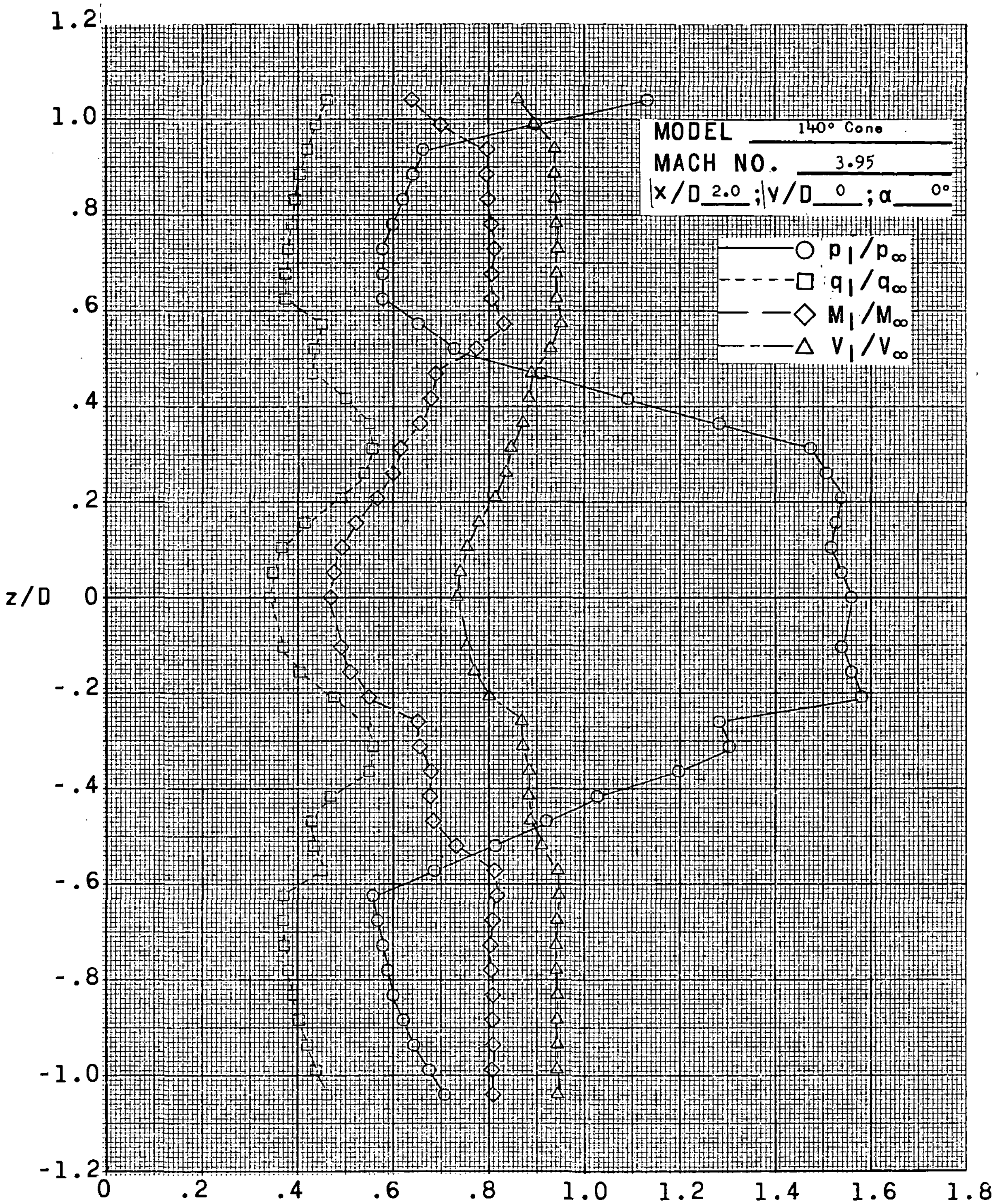
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 8.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D in wake of 140°-included-angle cone at Mach number of 3.95 and Reynolds number of 5.42×10^6 per meter (1.65×10^6 per foot).



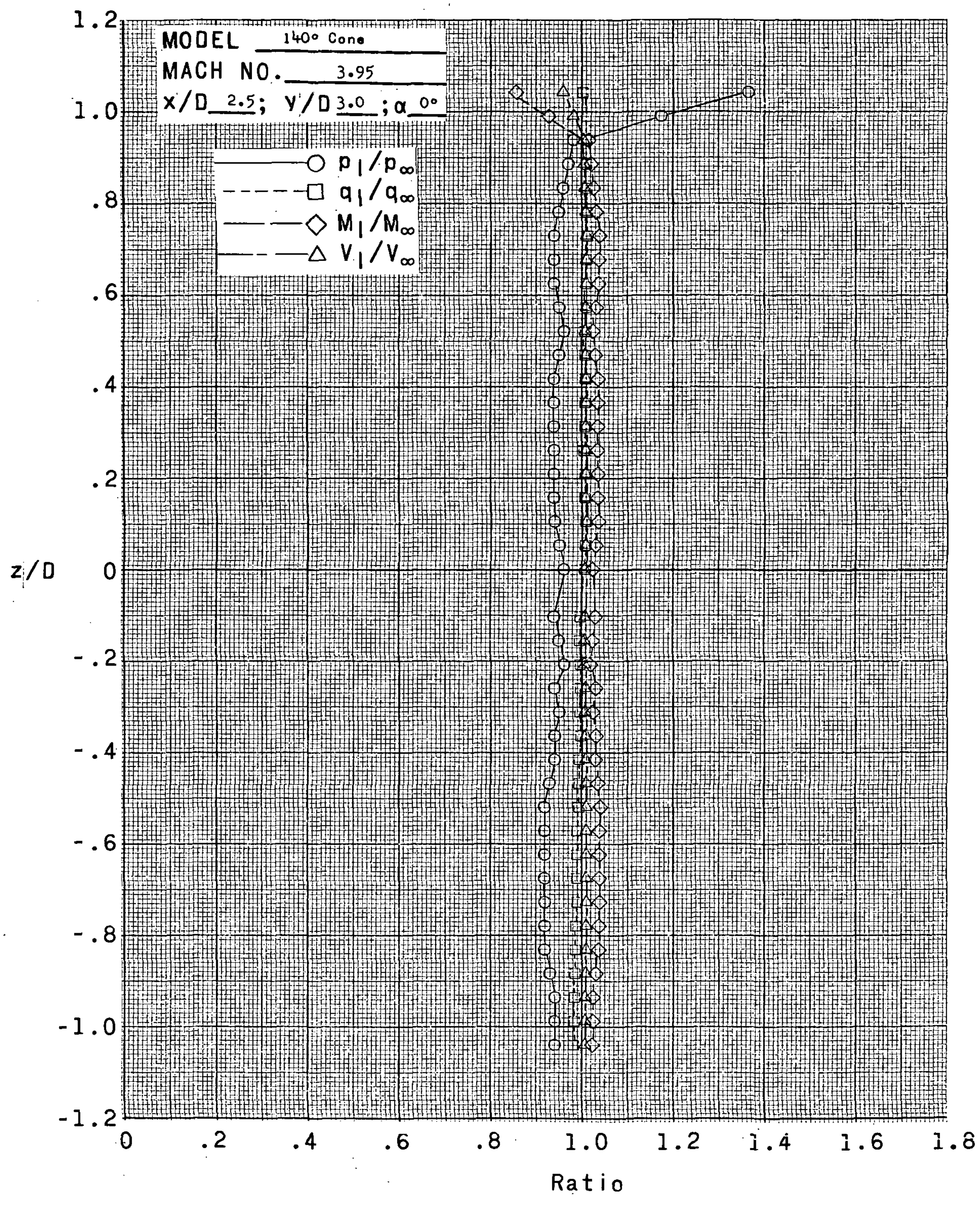
(b) x/D = 1.5; y/D = 0; α = 0°.

Figure 8.- Continued.



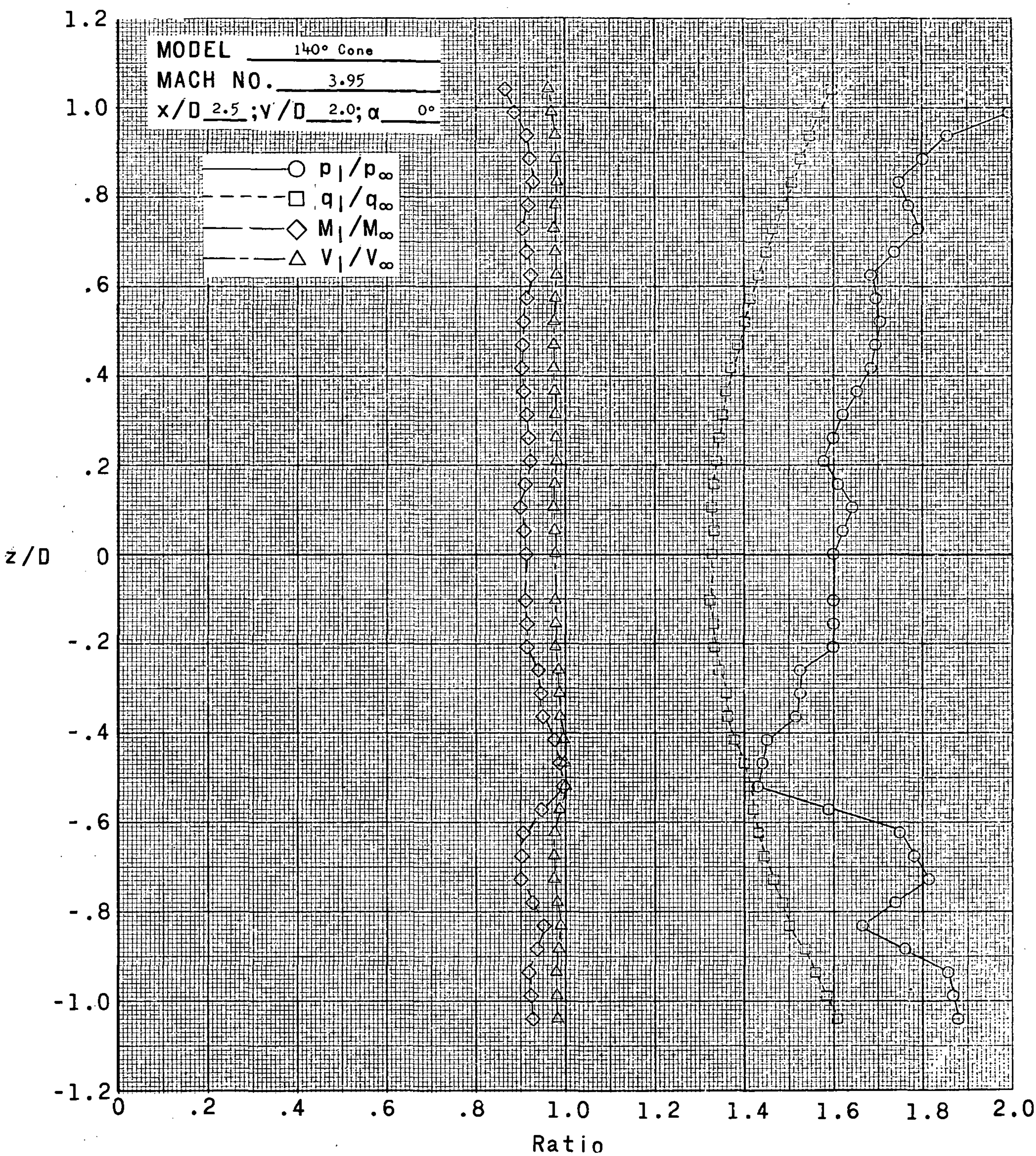
(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 0^{0}$.

Figure 8.- Continued.



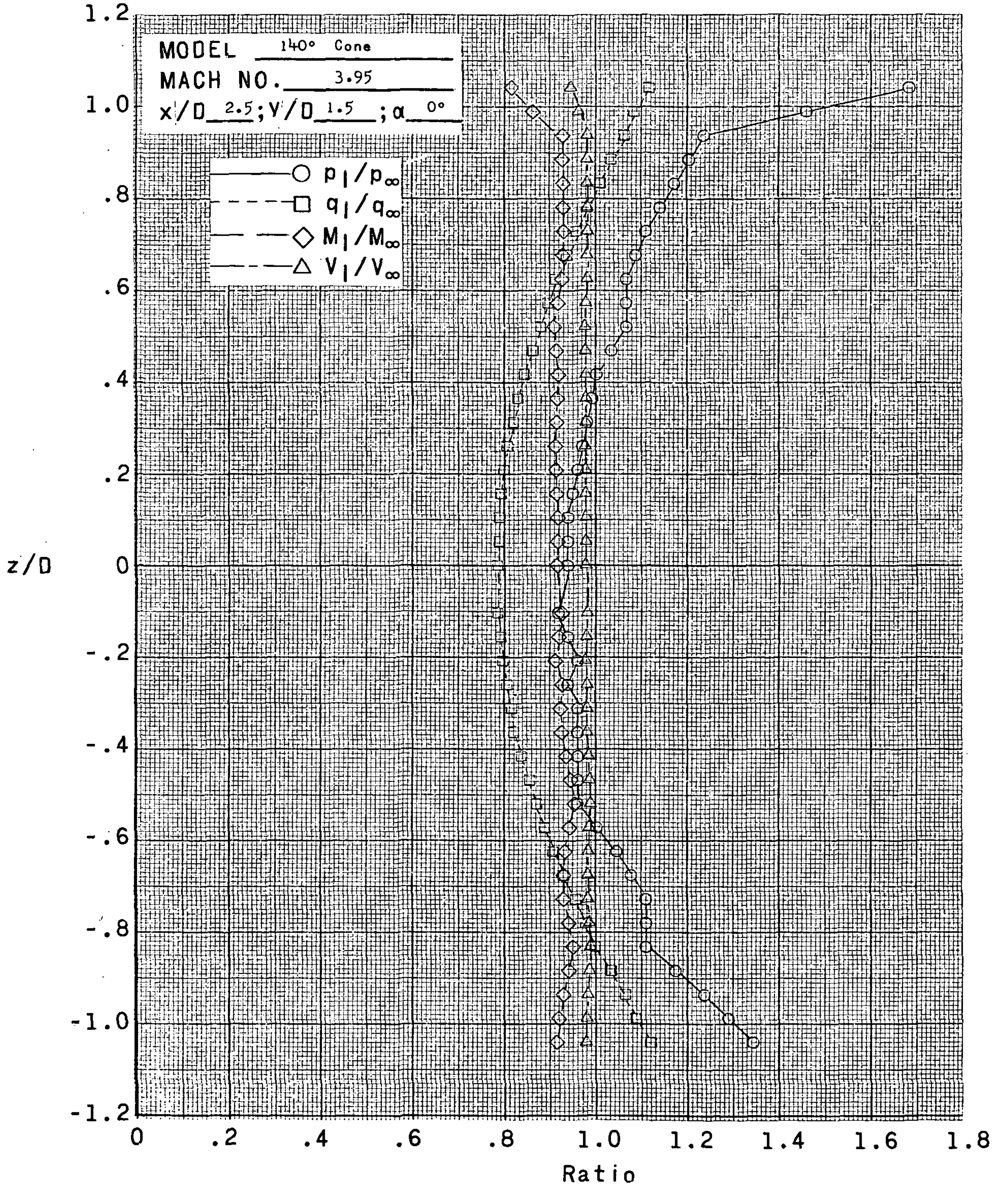
(d) x/D = 2.5; y/D = 3.0; α = 0°.

Figure 8.- Continued.



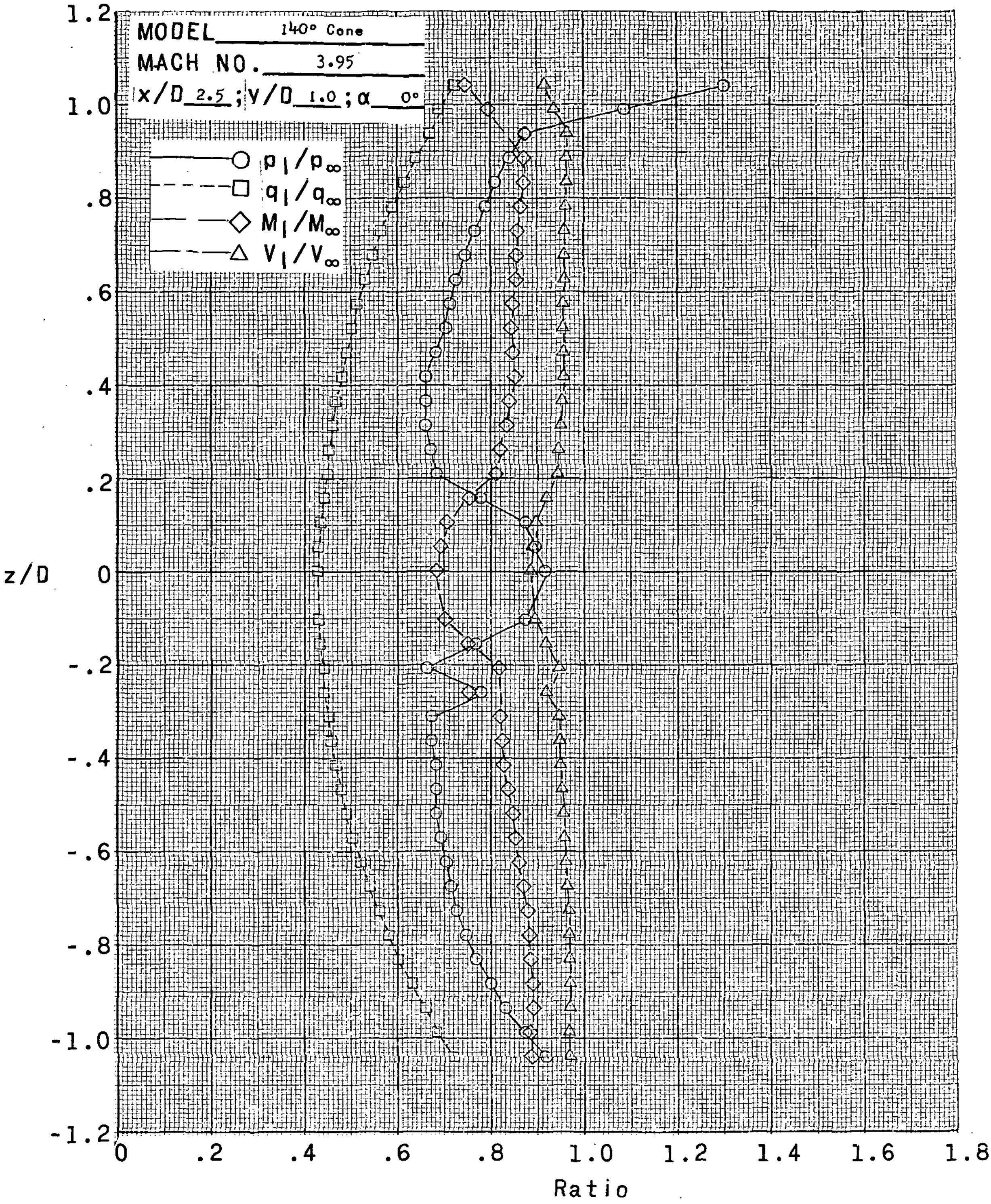
(e) $x/D = 2.5$; $y/D = 2.0$; $\alpha = 0^0$.

Figure 8.- Continued.



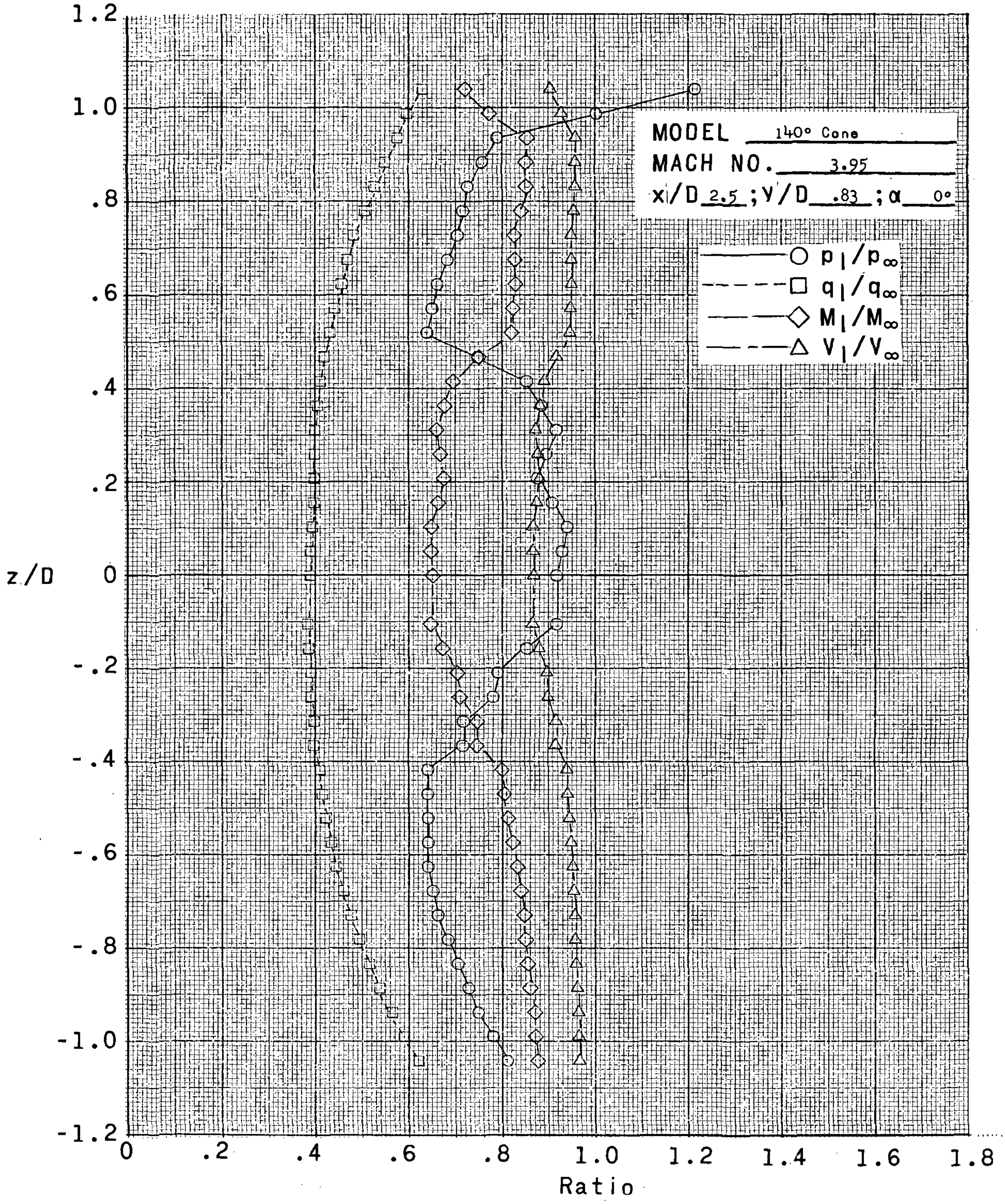
(f) $x/D = 2.5$; $y/D = 1.5$; $\alpha = 0^0$.

Figure 8.- Continued.



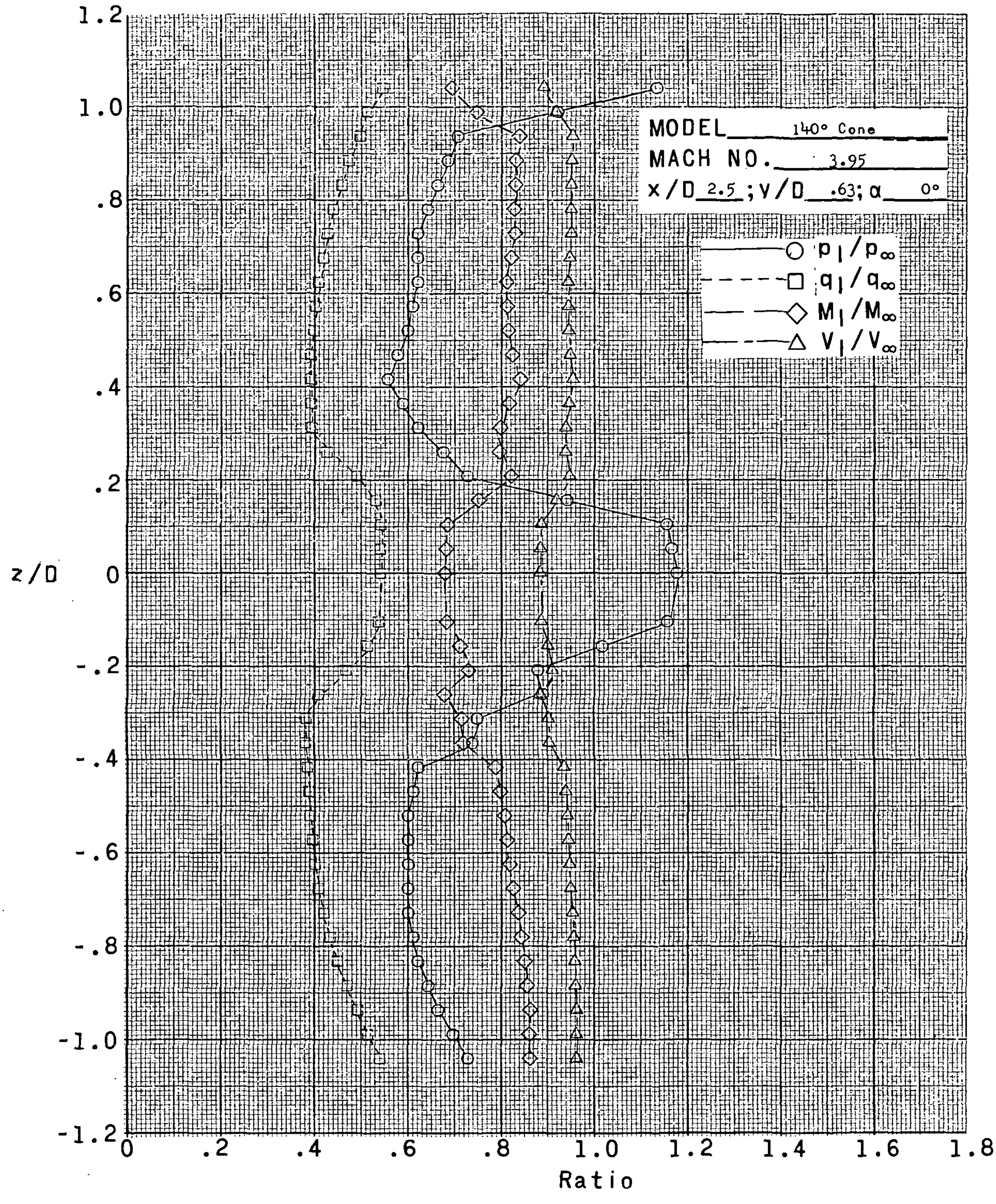
(g) $x/D = 2.5$; $y/D = 1.0$; $\alpha = 0^{\circ}$.

Figure 8.- Continued.



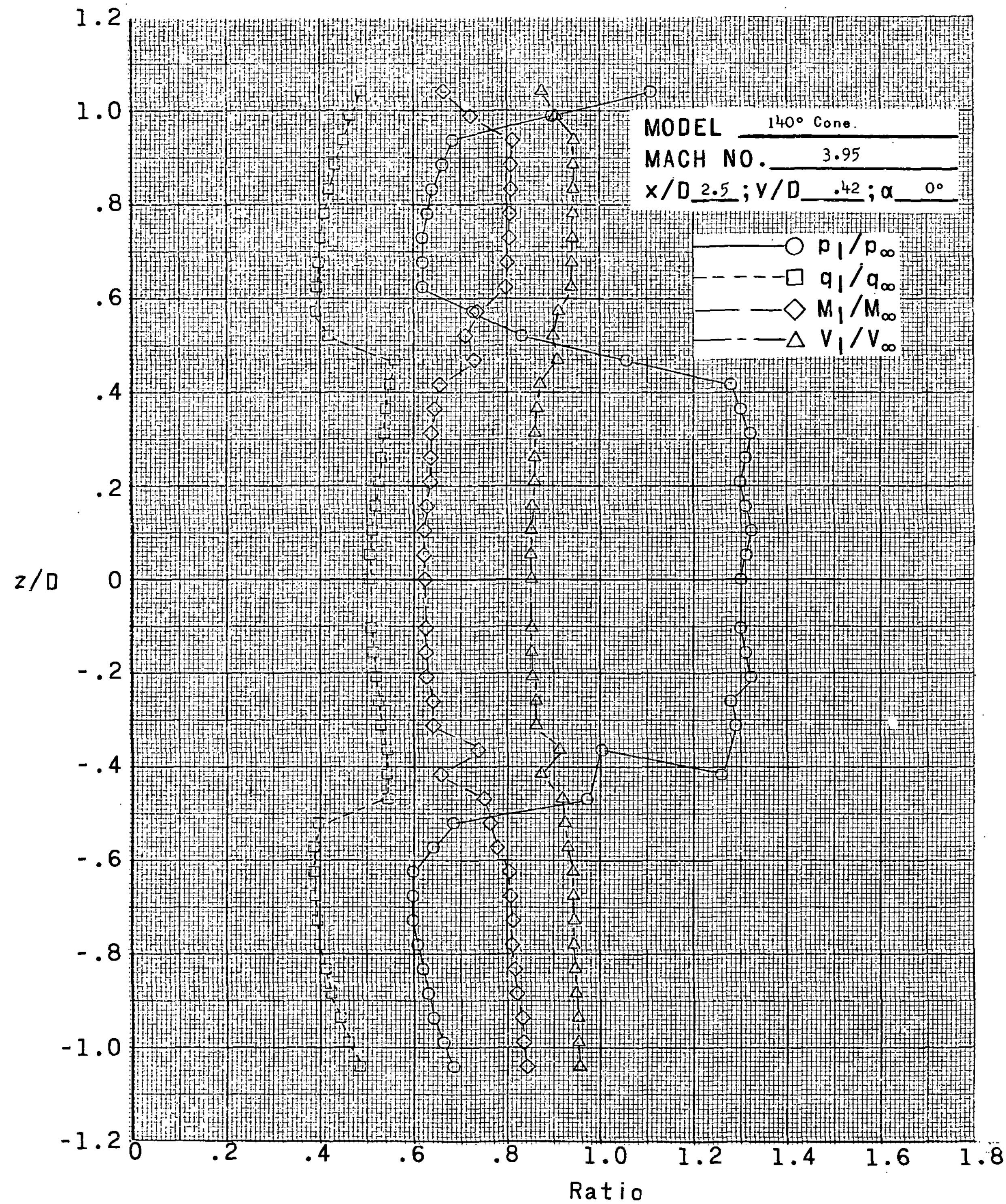
(h) $x/D = 2.5$; $y/D = 0.83$; $\alpha = 0^{0}$.

Figure 8.- Continued.



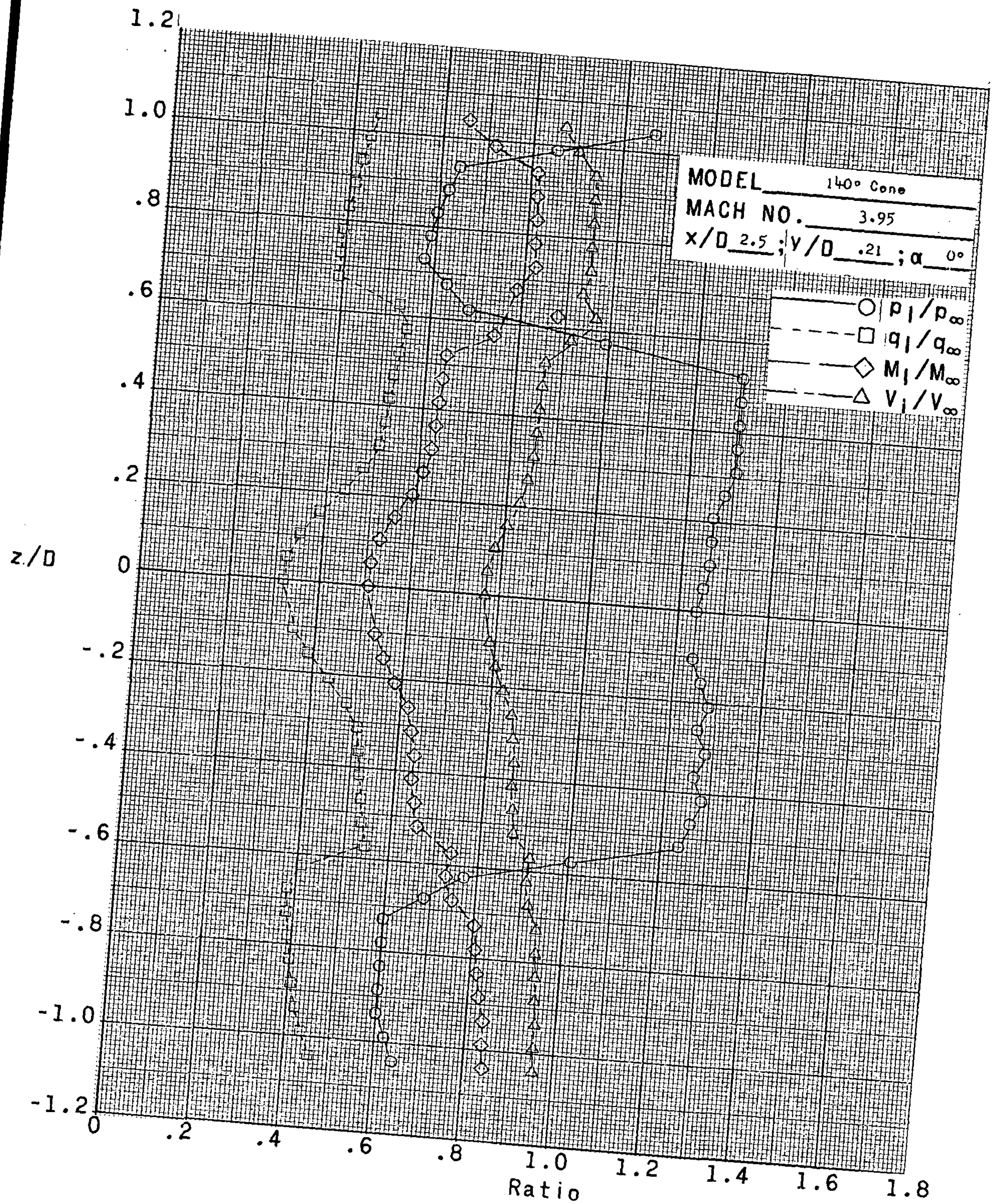
(i) x/D = 2.5; y/D = 0.63; α = 0°.

Figure 8.- Continued.



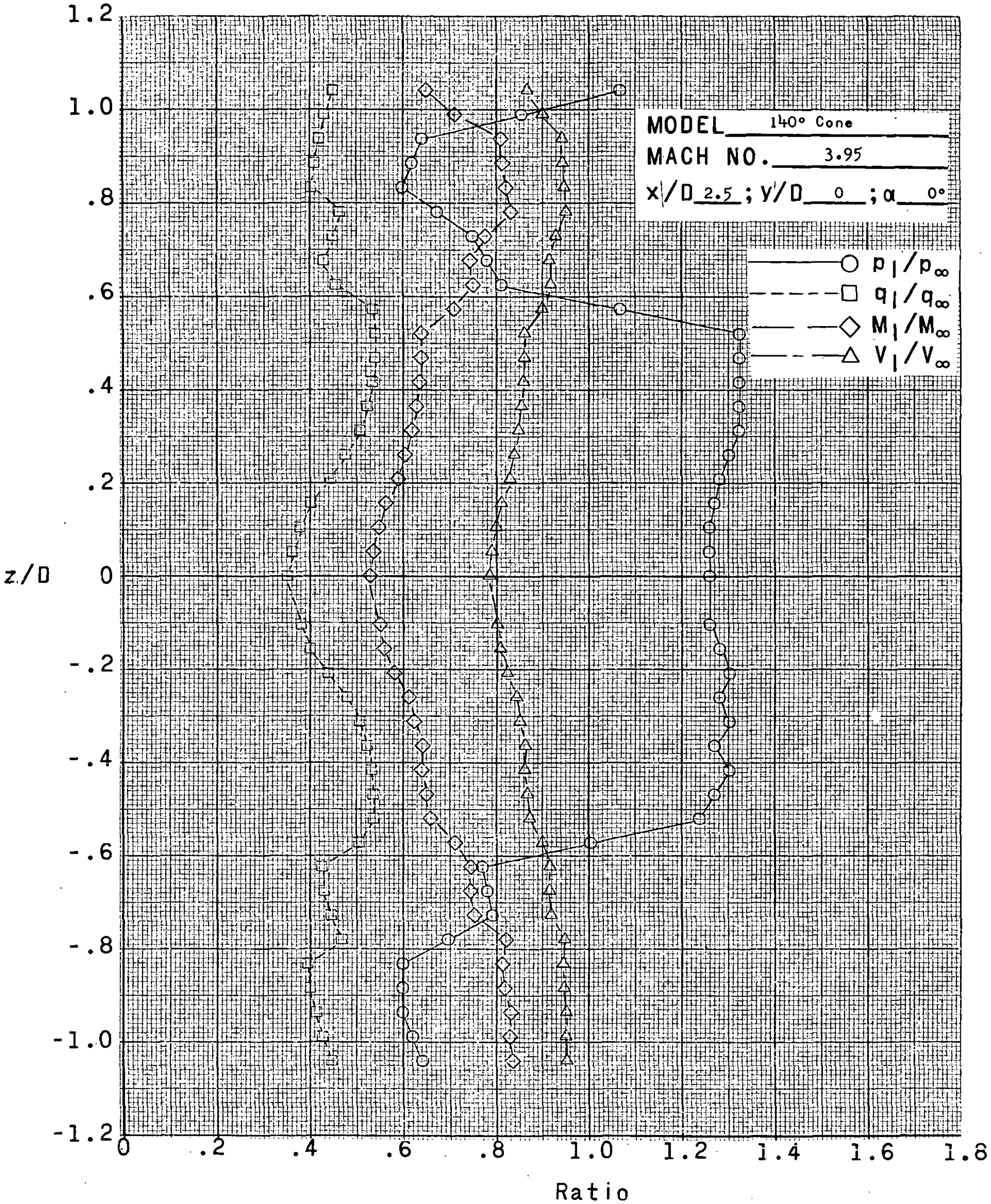
(j) $x/D = 2.5$; $y/D = 0.42$; $\alpha = 0^{0}$.

Figure 8.- Continued.



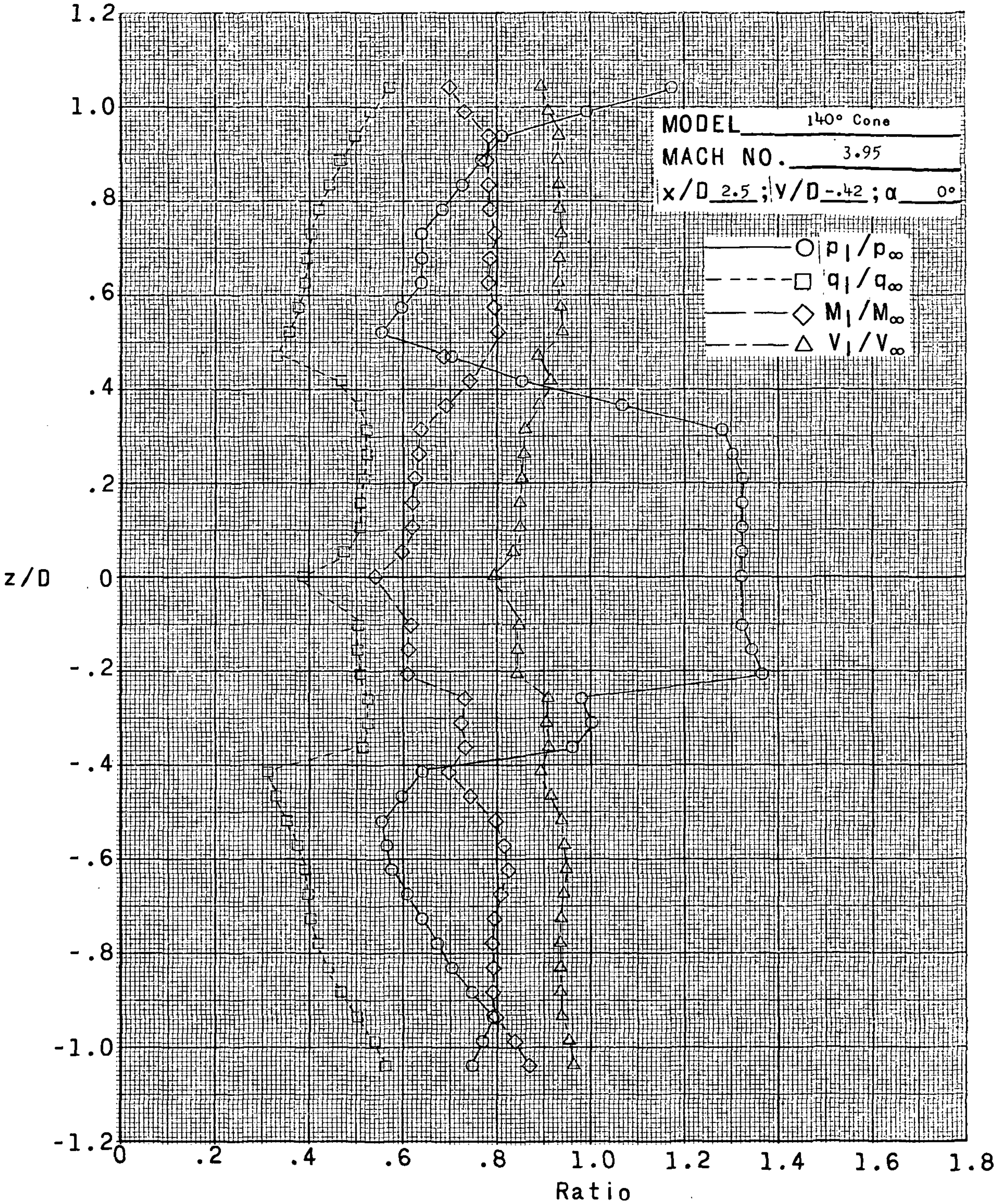
(k) $x/D = 2.5$; $y/D = 0.21$; $\alpha = 0^o$.

Figure 8.- Continued.



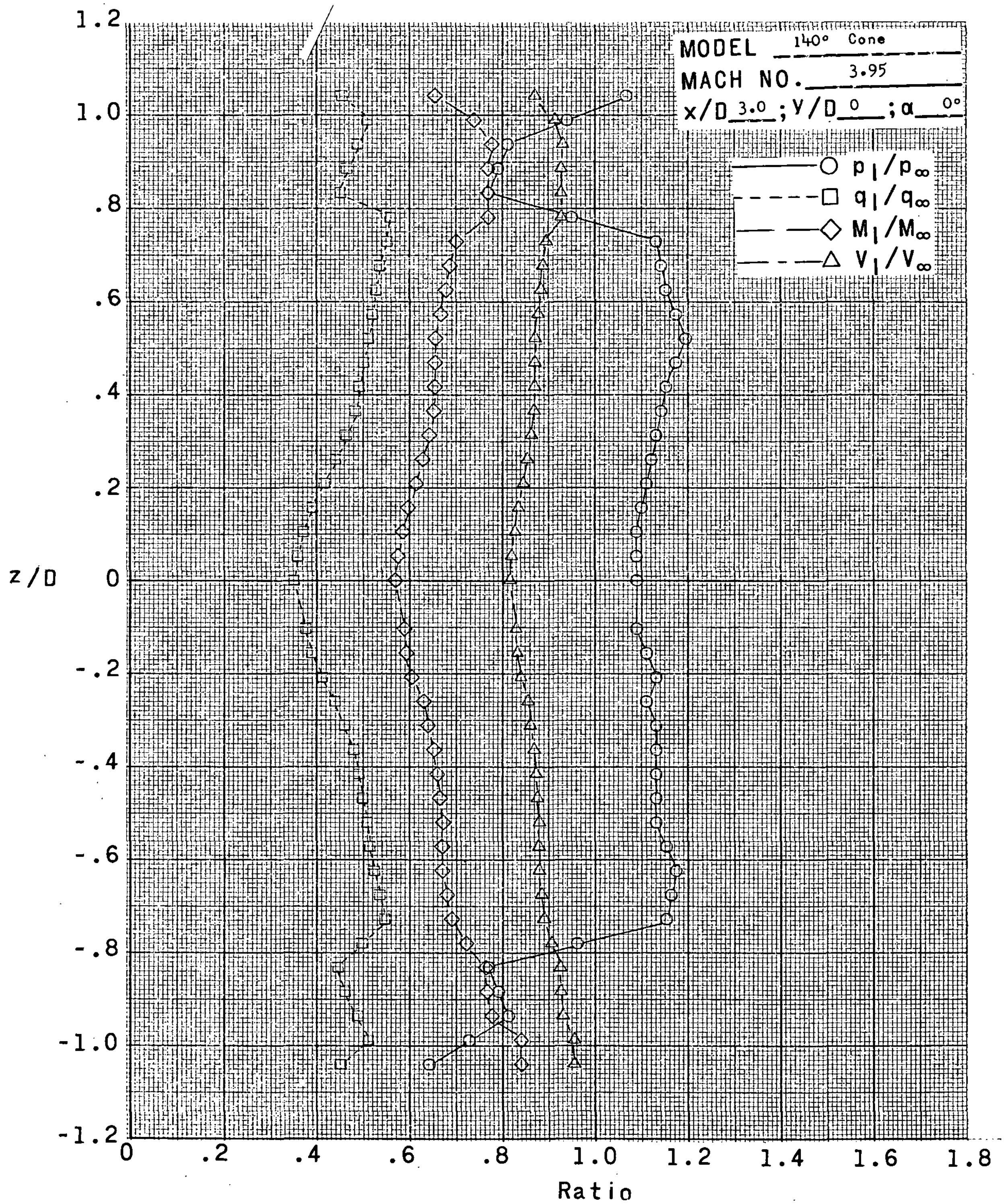
(l) $x/D = 2.5$; $y/D = 0$; $\alpha = 0^{0}$.

Figure 8.- Continued.



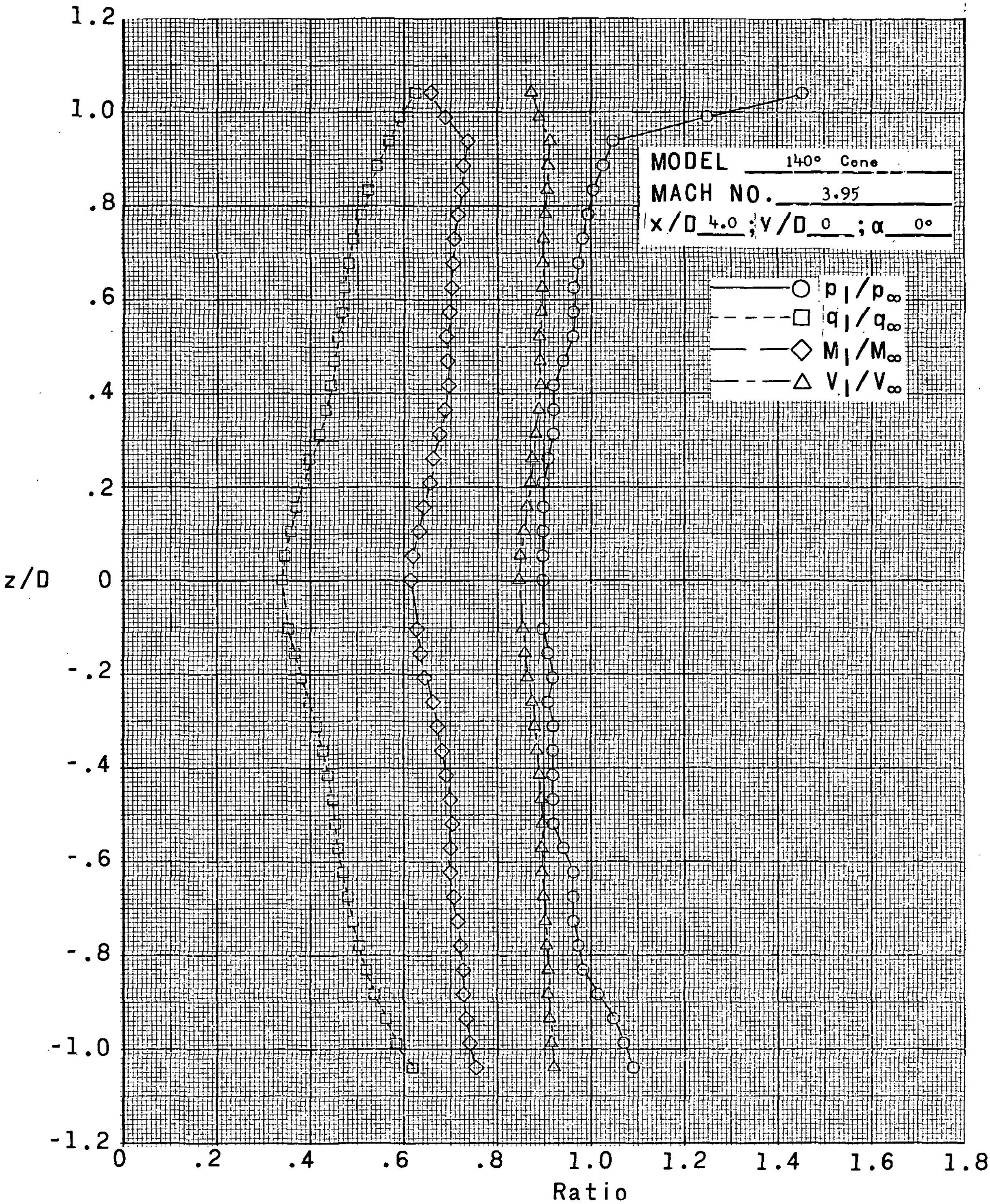
(m) x/D = 2.5; y/D = -0.42; α = 0°.

Figure 8.- Continued.



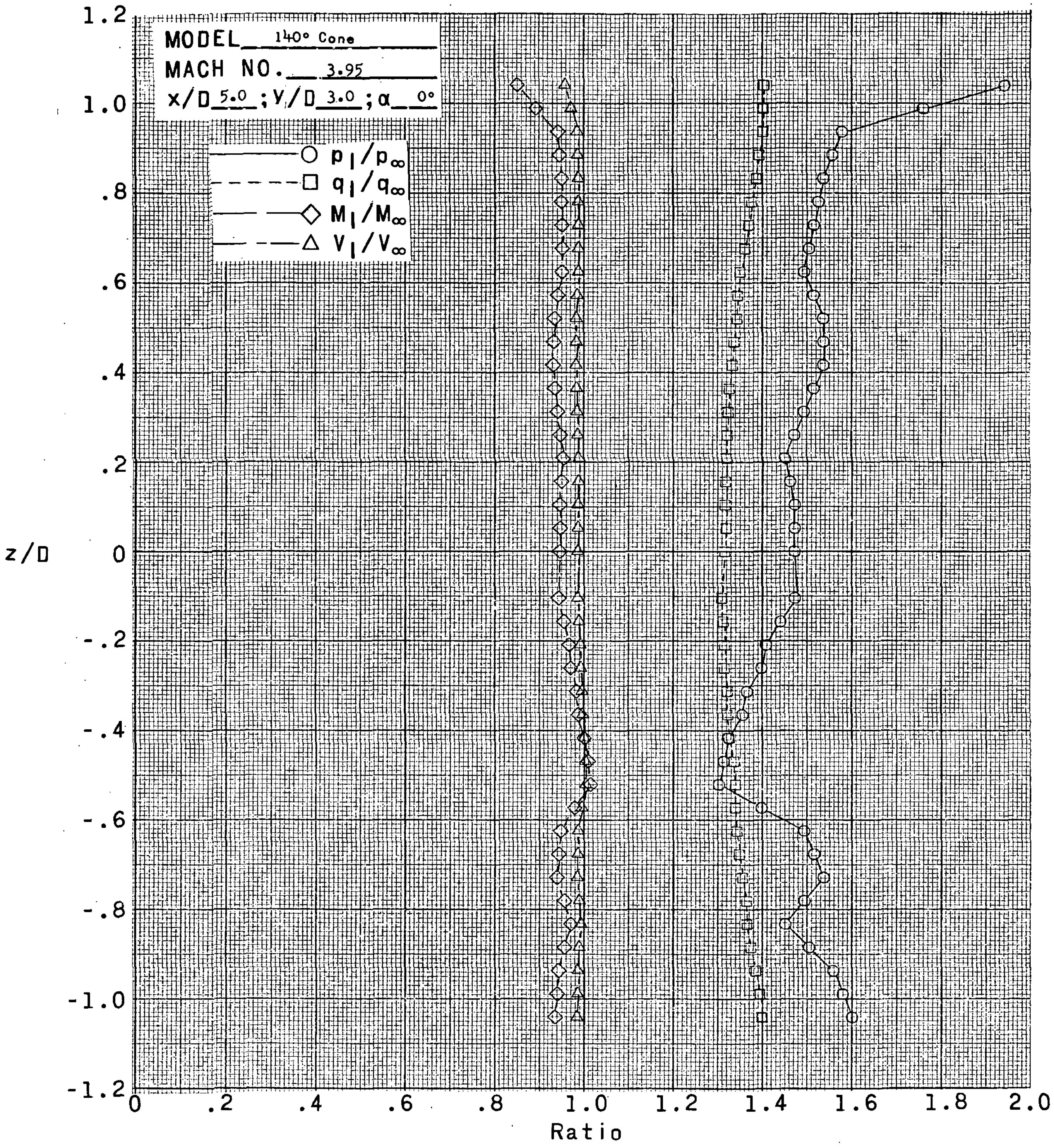
(n) $x/D = 3.0$; $y/D = 0$; $\alpha = 0^{0}$.

Figure 8.- Continued.



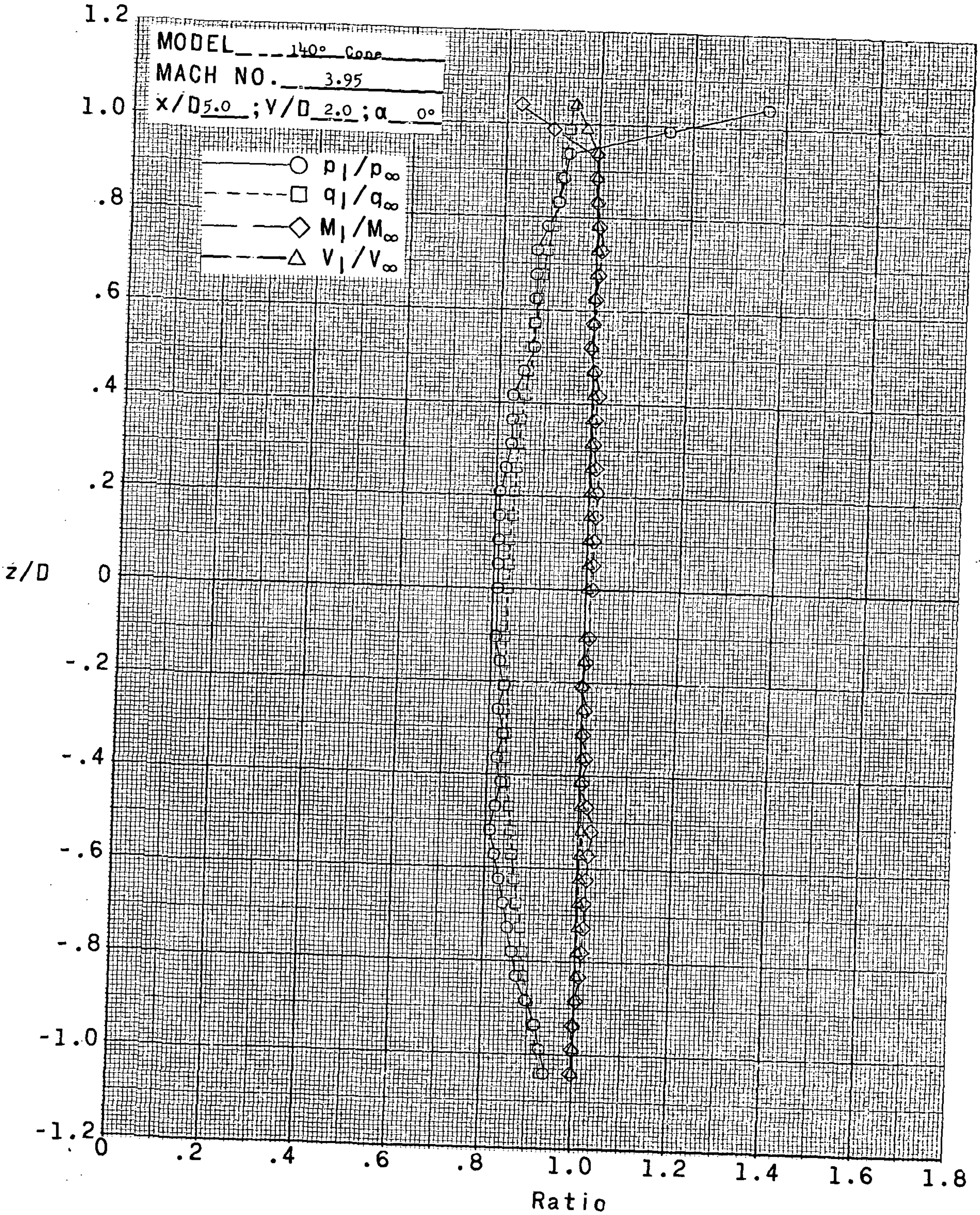
(o) x/D = 4.0; y/D = 0; α = 0°.

Figure 8.- Continued.



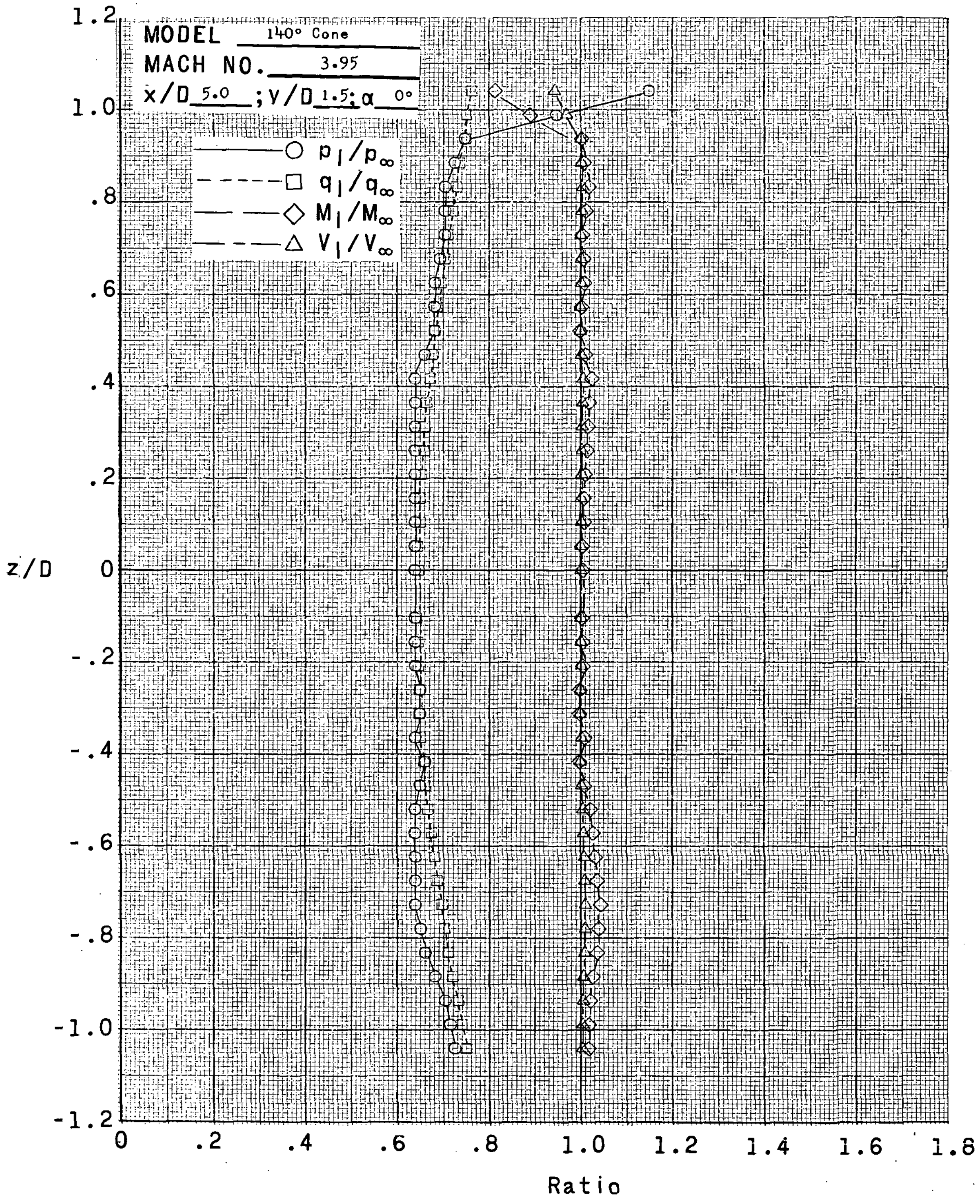
(p) $x/D = 5.0$; $y/D = 3.0$; $\alpha = 0^0$.

Figure 8.- Continued.



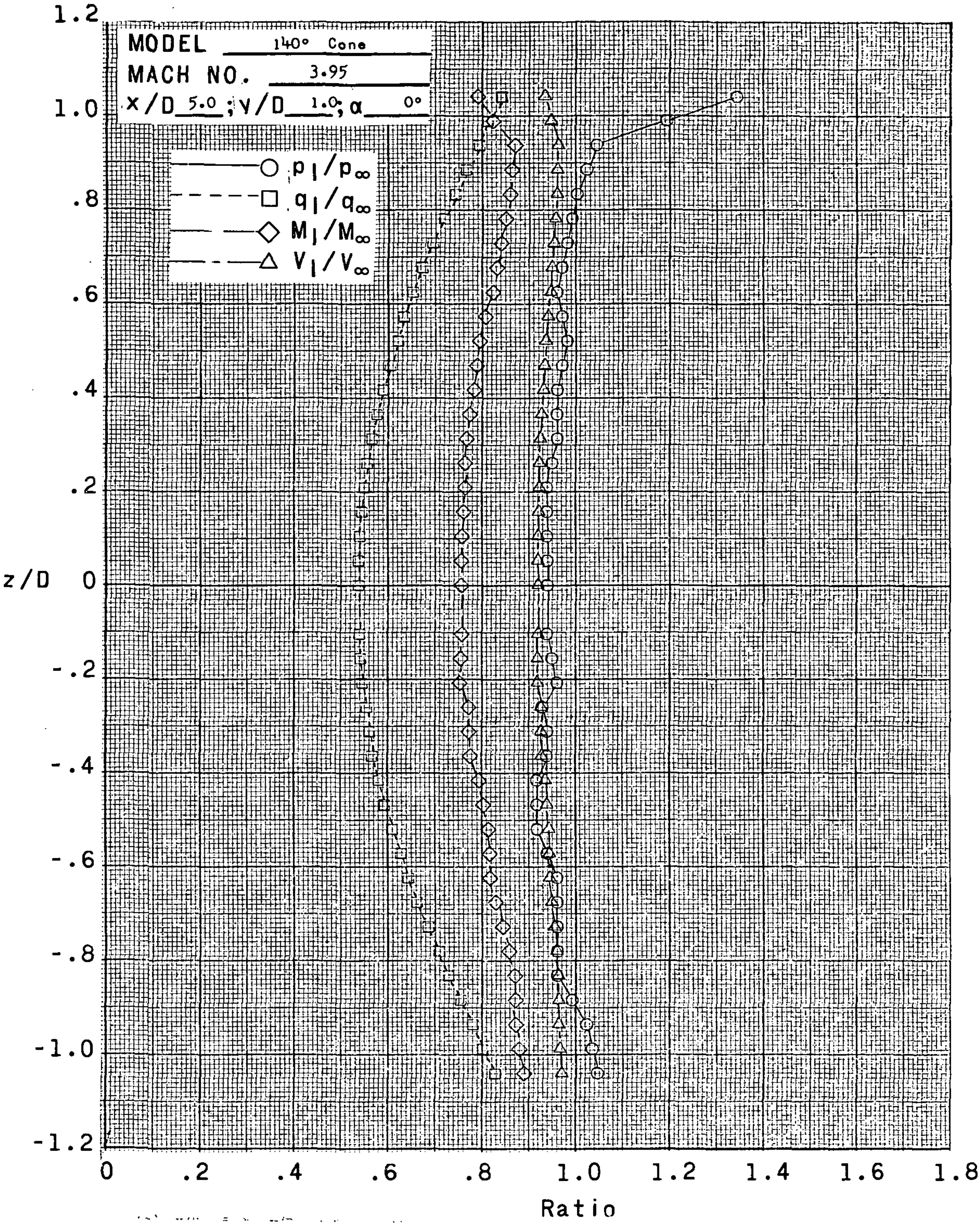
(q) $x/D = 5.0$; $y/D = 2.0$; $\alpha = 0^{0}$.

Figure 8.- Continued.



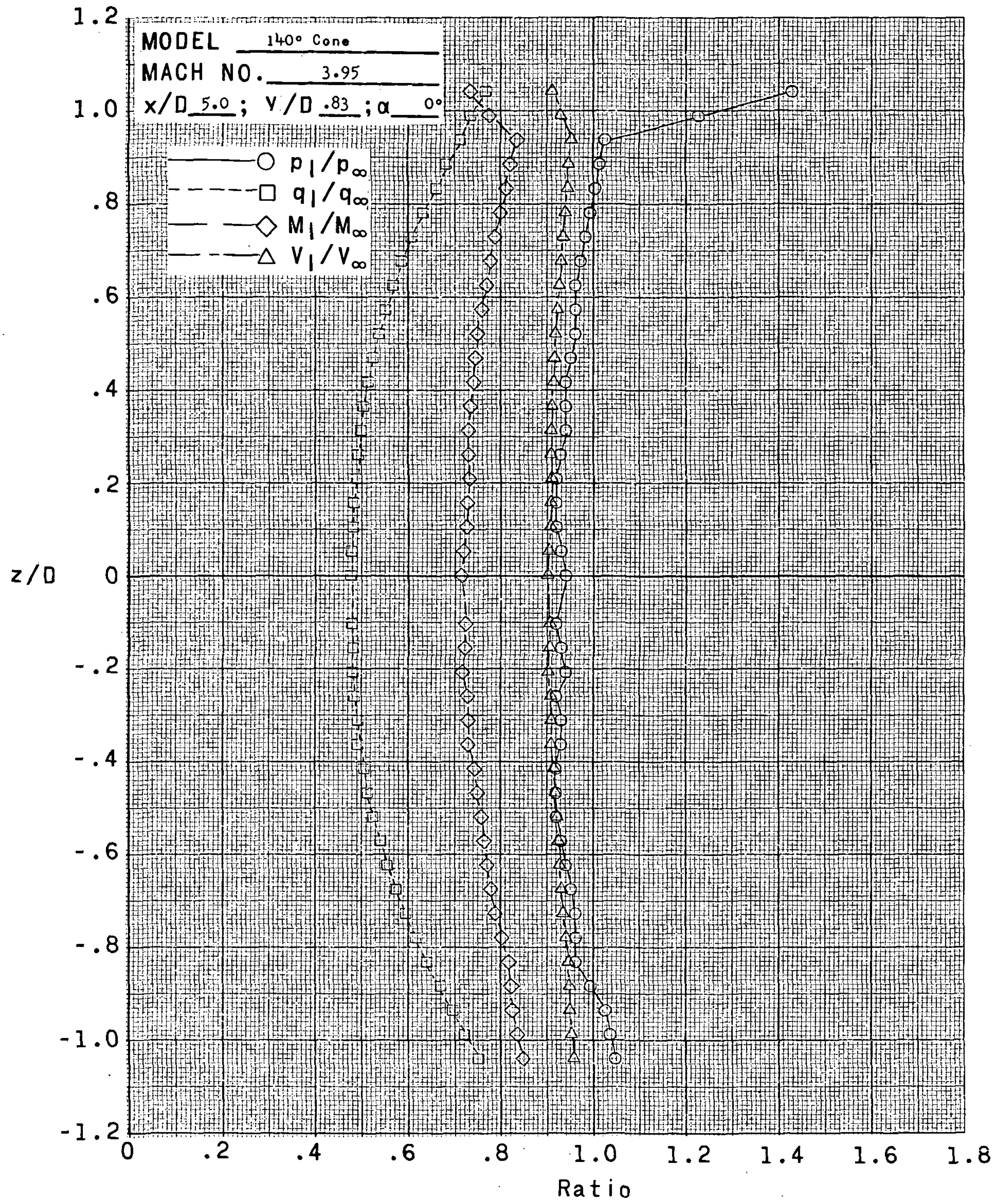
(r) x/D = 5.0; y/D = 1.5; α = 0°.

Figure 8.- Continued.



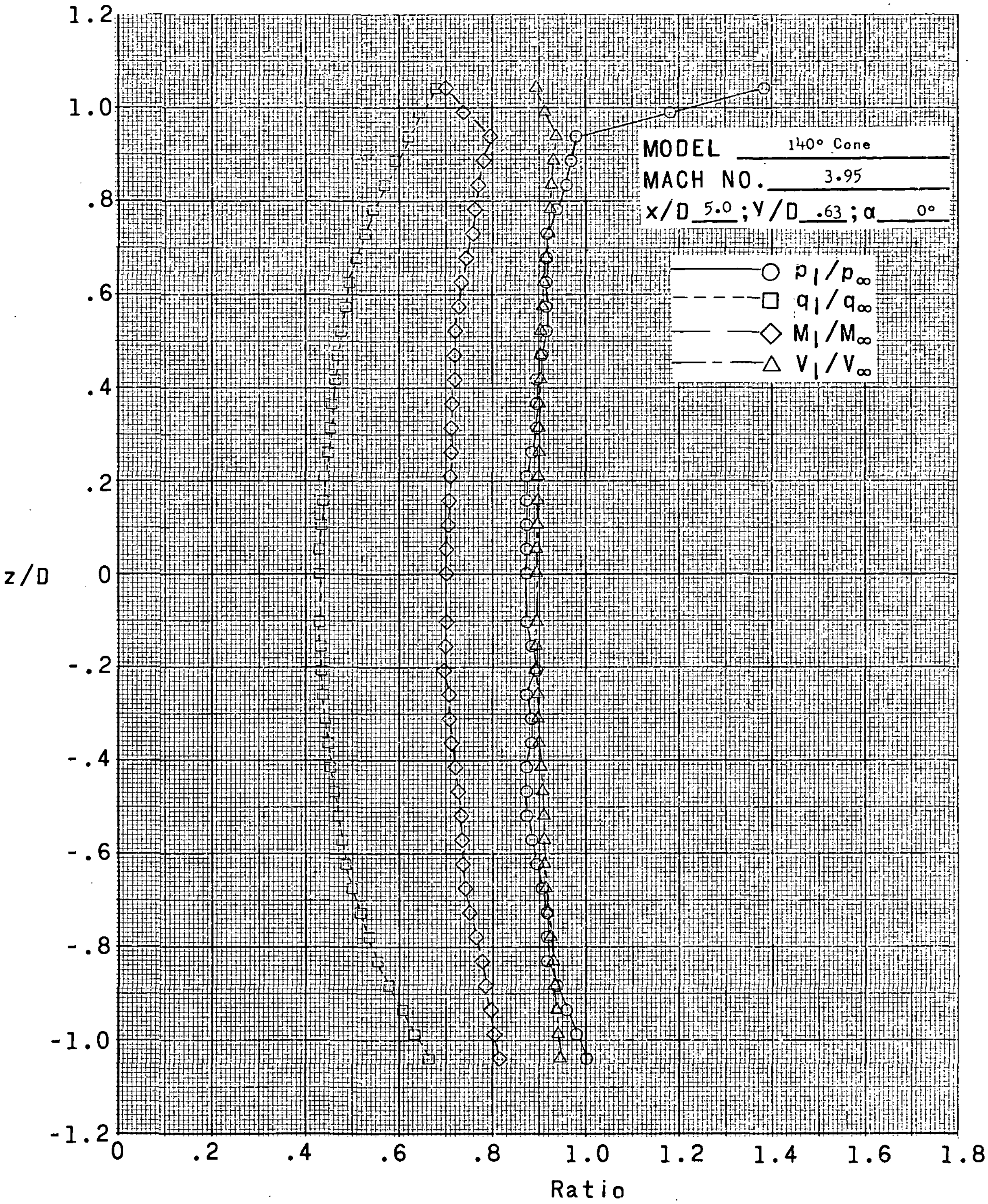
(s) x/D = 5.0; y/D = 1.0; α = 0°.

Figure 8.- Continued.



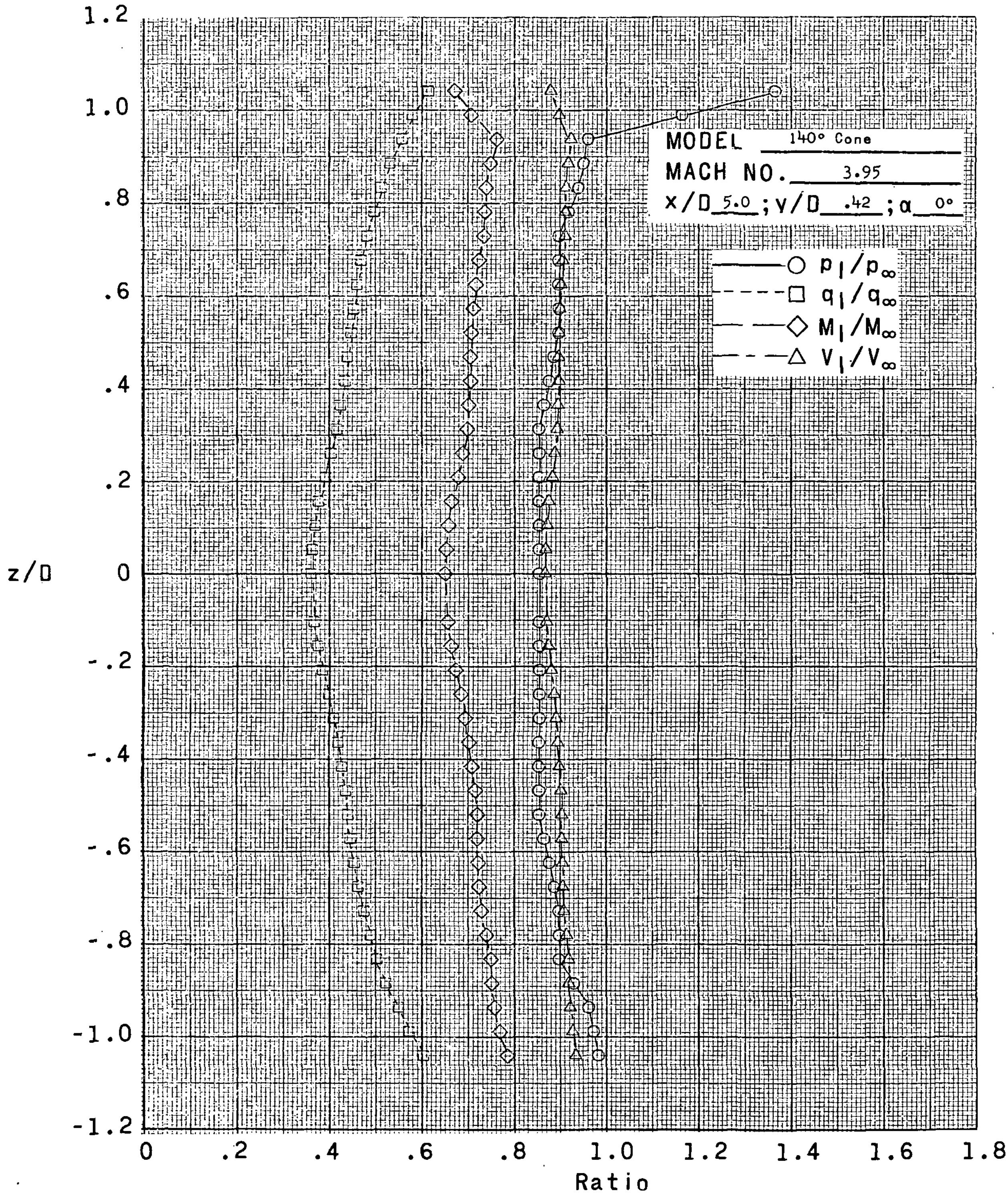
(t) $x/D = 5.0$; $y/D = 0.83$; $\alpha = 0^0$.

Figure 8.- Continued.



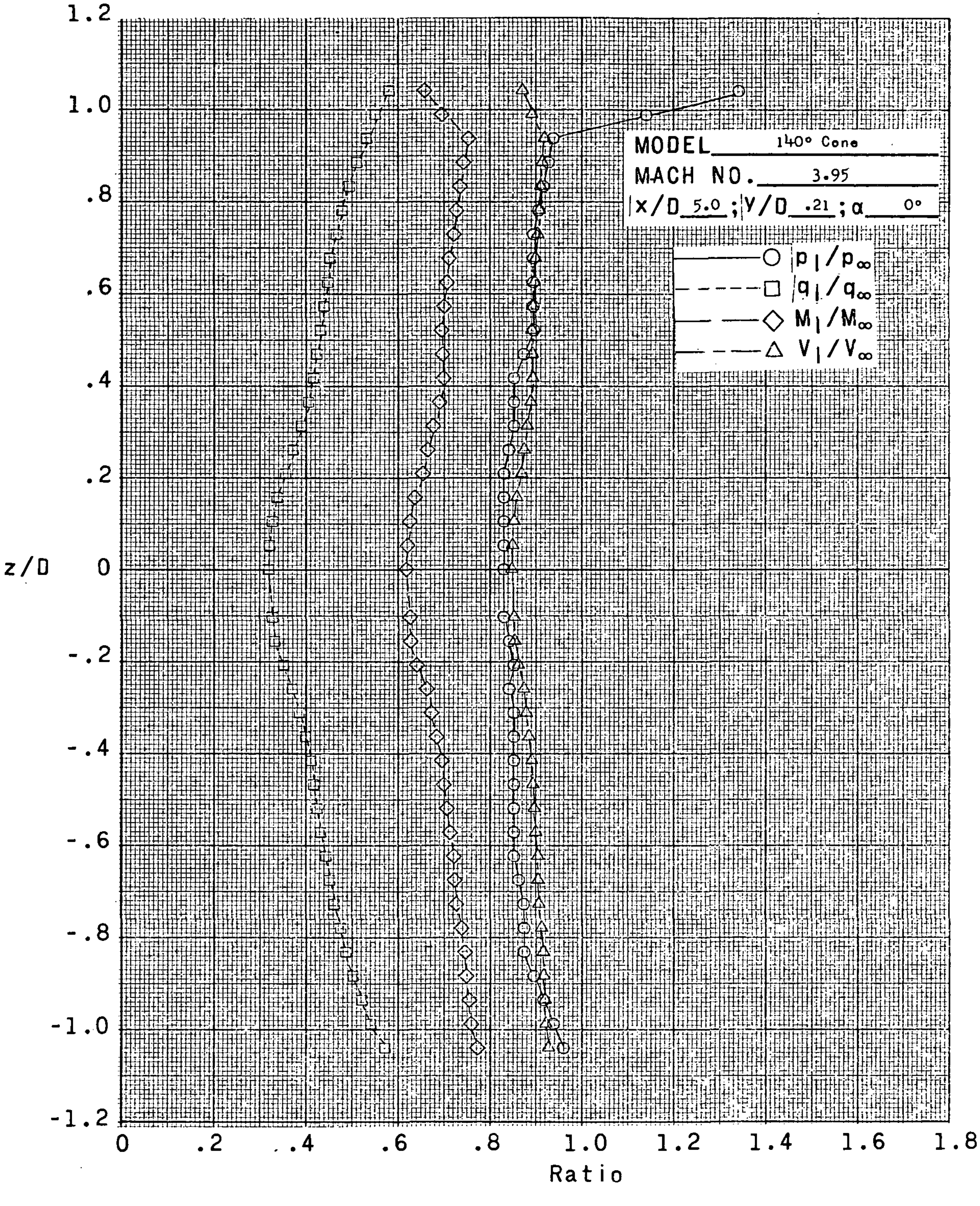
(u) x/D = 5.0; y/D = 0.63; α = 0°.

Figure 8.- Continued.



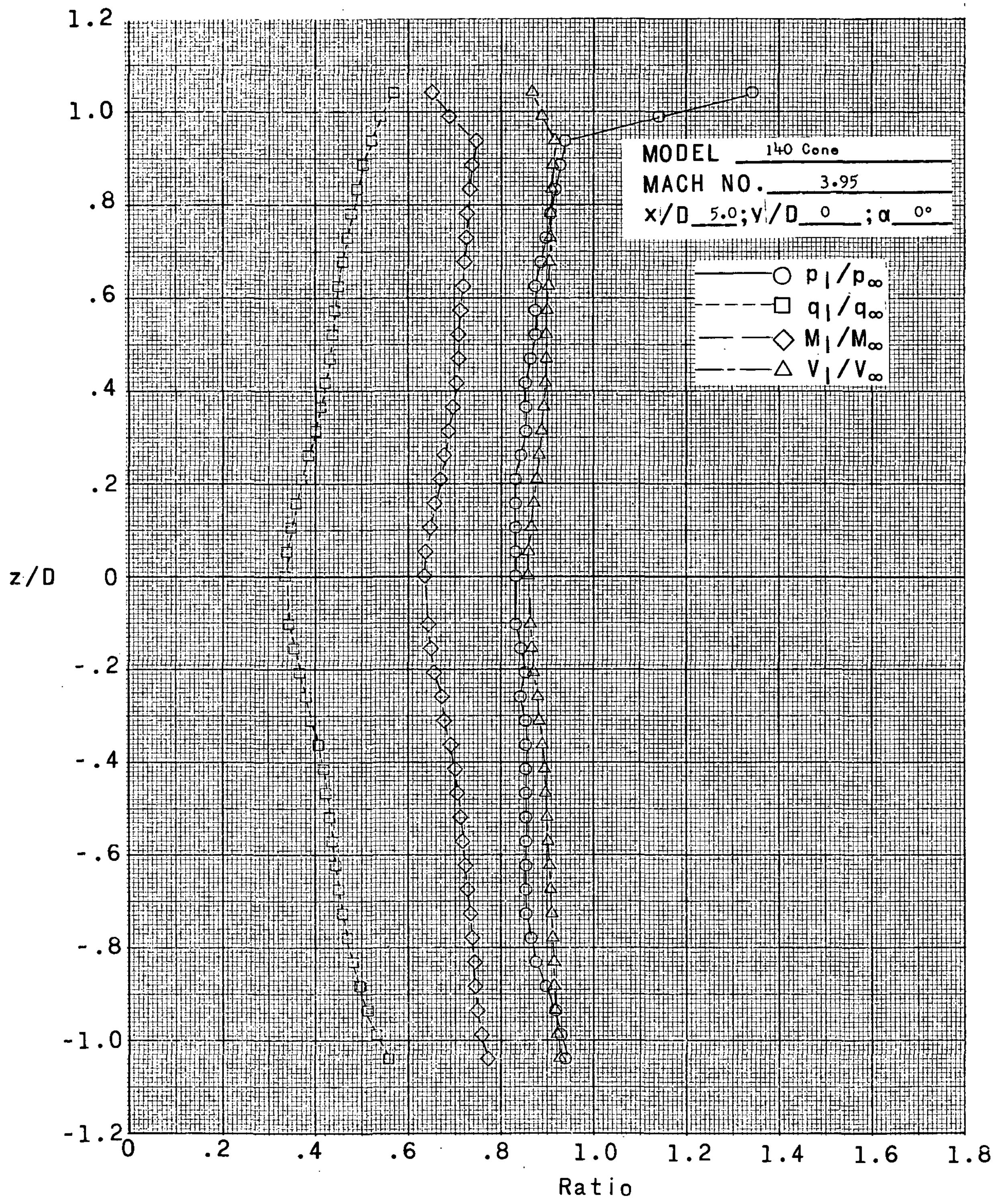
(v) $x/D = 5.0$; $y/D = 0.42$; $\alpha = 0^{0}$.

Figure 8.- Continued.



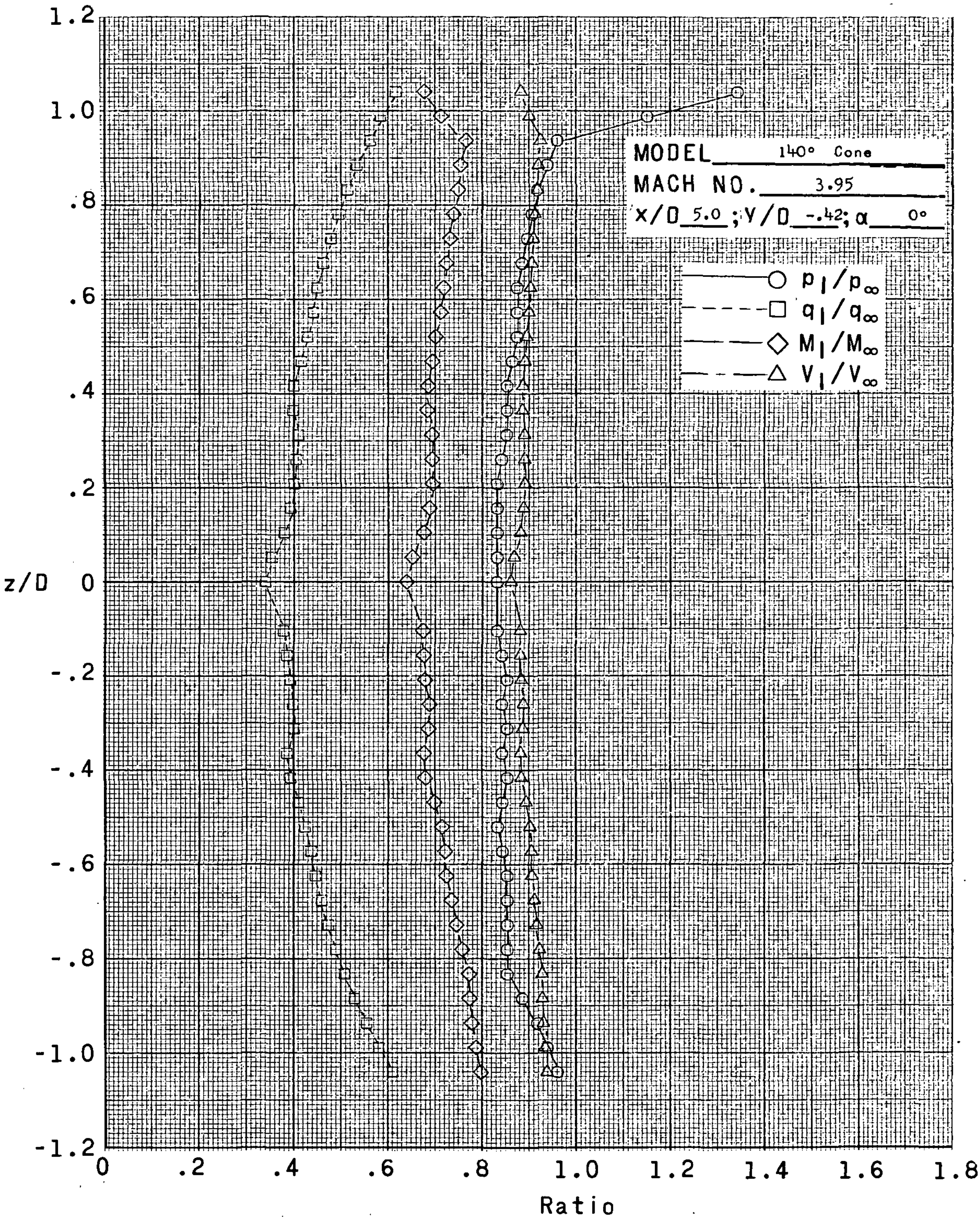
(w) x/D = 5.0; y/D = 0.21; α = 0°.

Figure 8.- Continued.



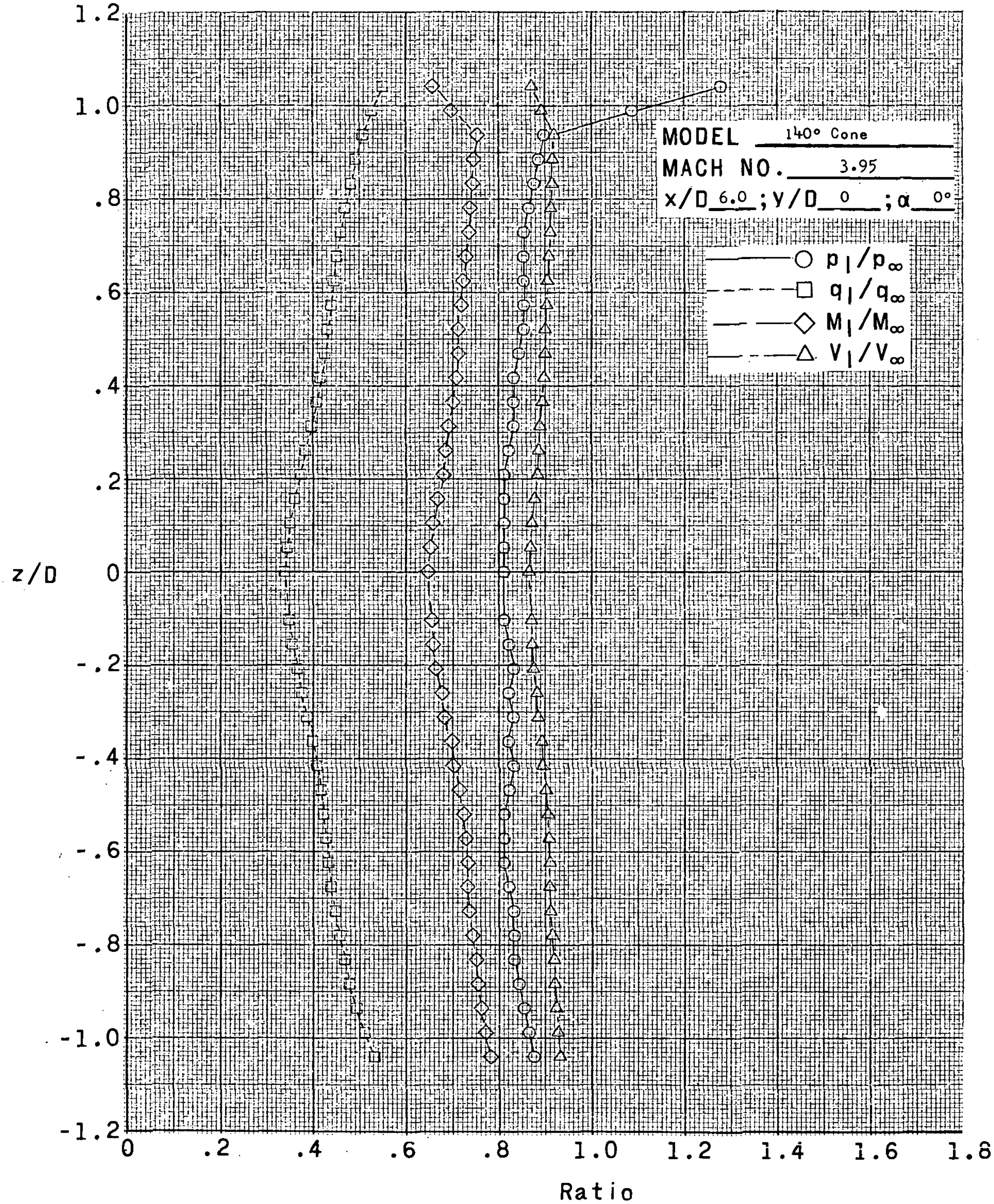
(x) x/D = 5.0; y/D = 0; α = 0°.

Figure 8.- Continued.



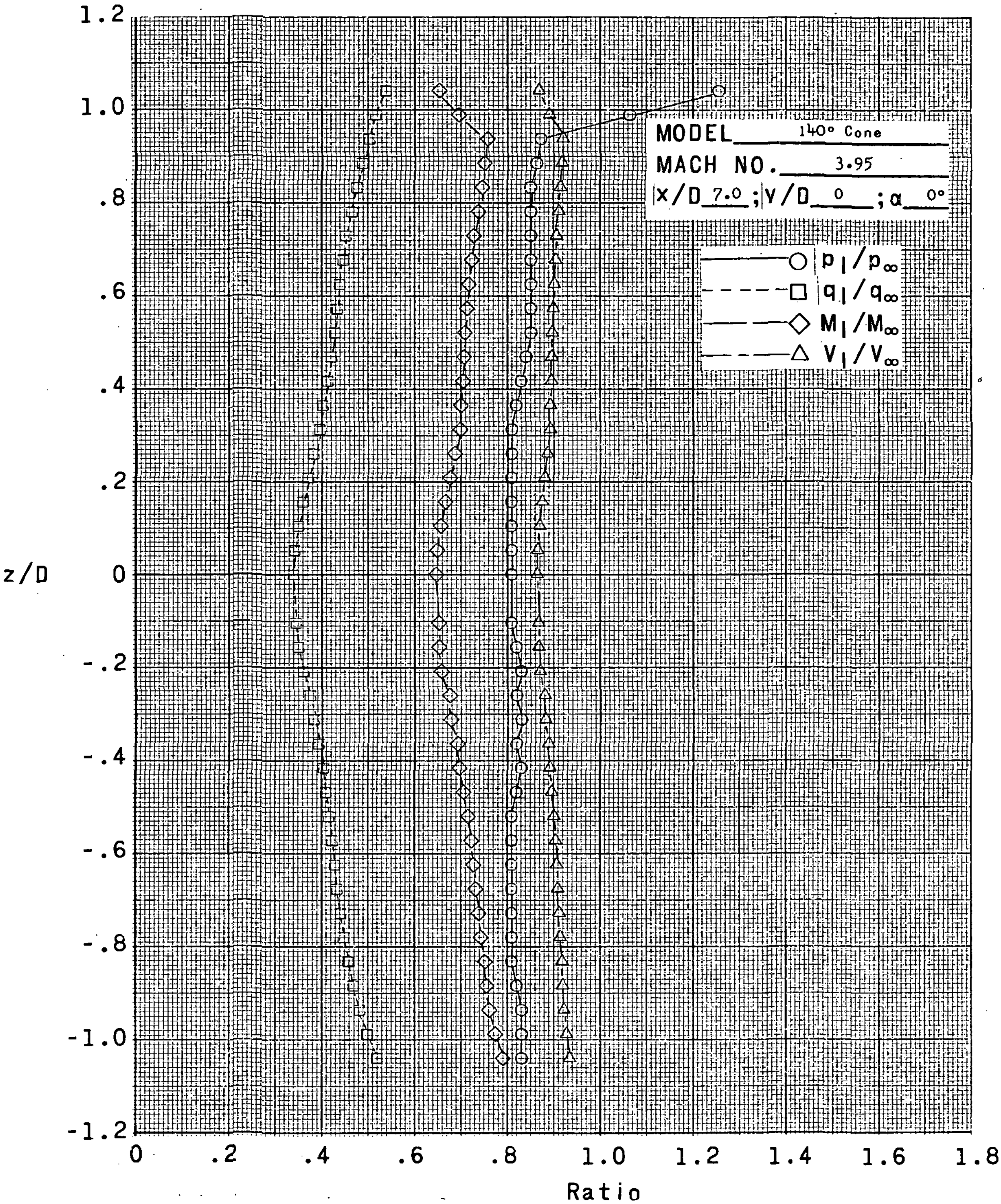
(y) $x/D = 5.0$; $y/D = -0.42$; $\alpha = 0^o$.

Figure 8.- Continued.



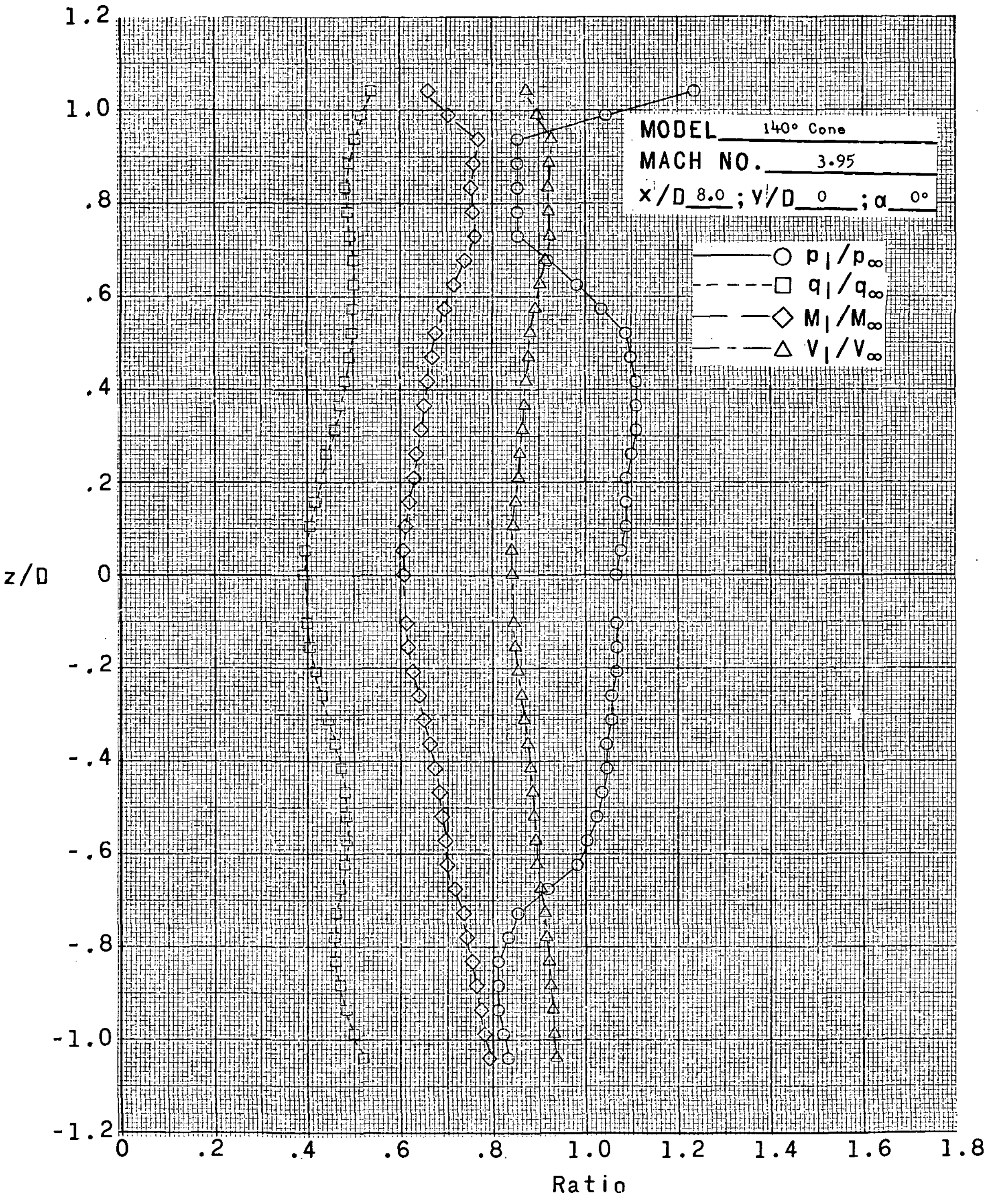
(z) x/D = 6.0; y/D = 0; α = 0°.

Figure 8.- Continued.



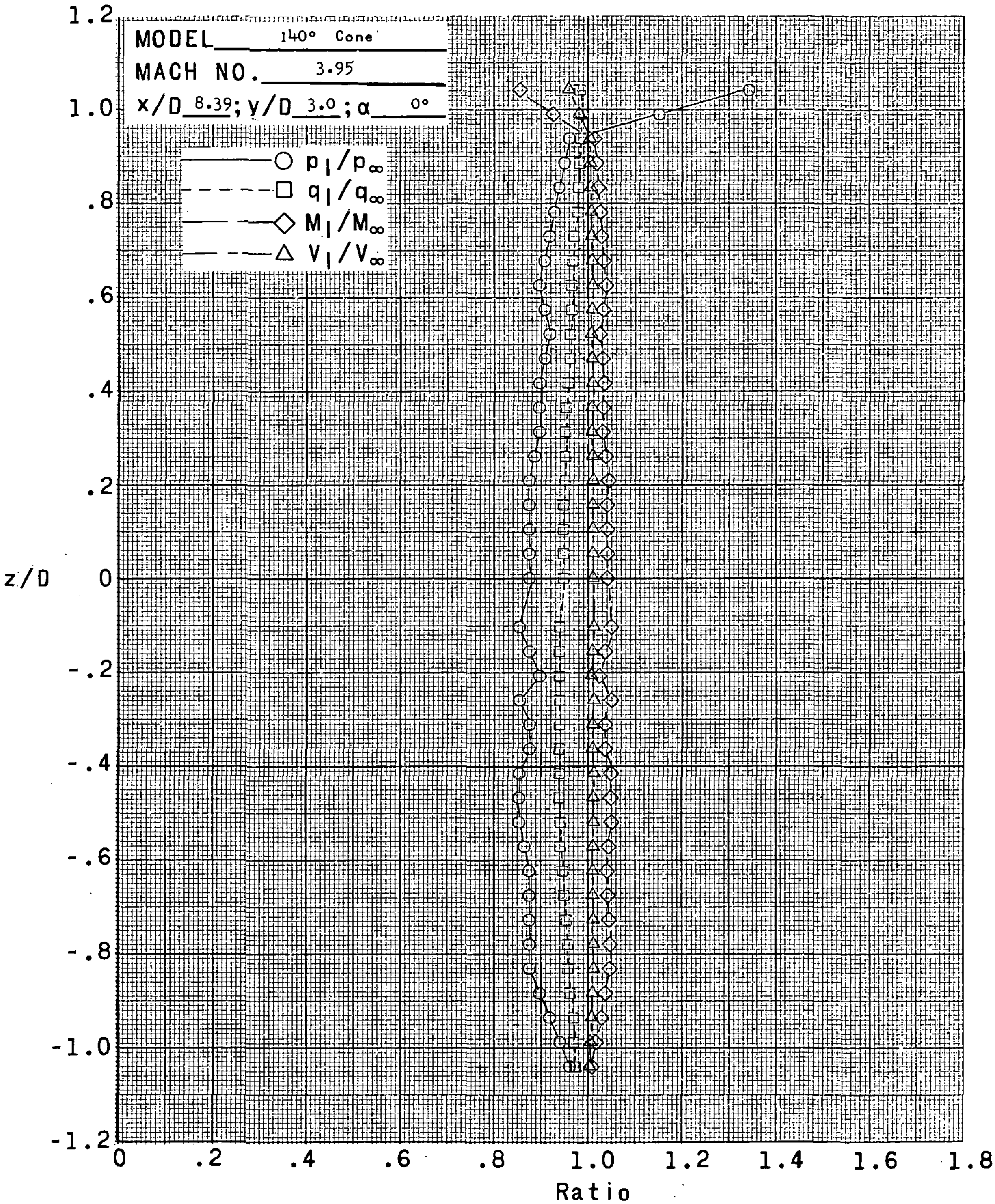
(aa) x/D = 7.0; y/D = 0; α = 0°.

Figure 8.- Continued.



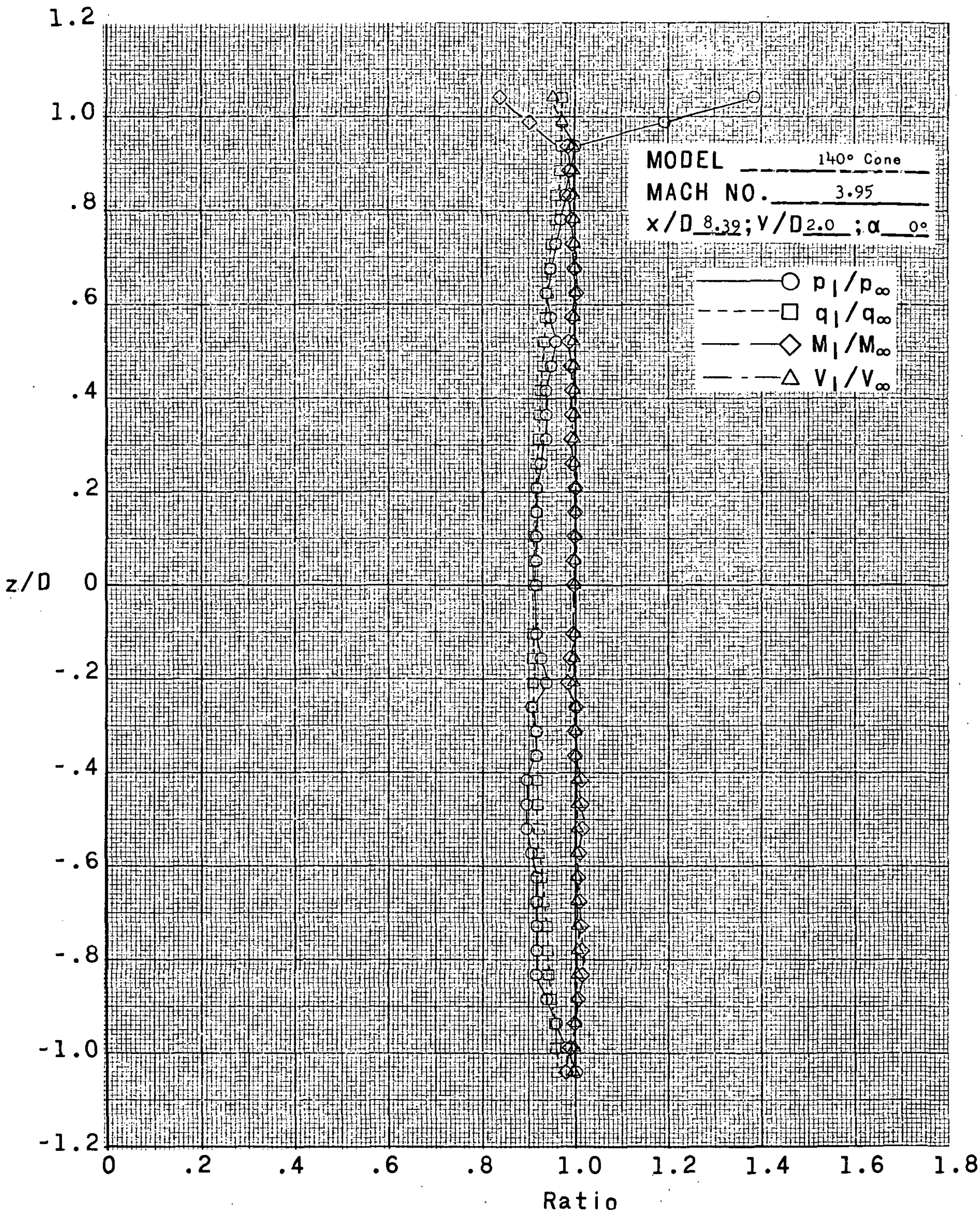
(bb) $x/D = 8.0$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 8.- Continued.



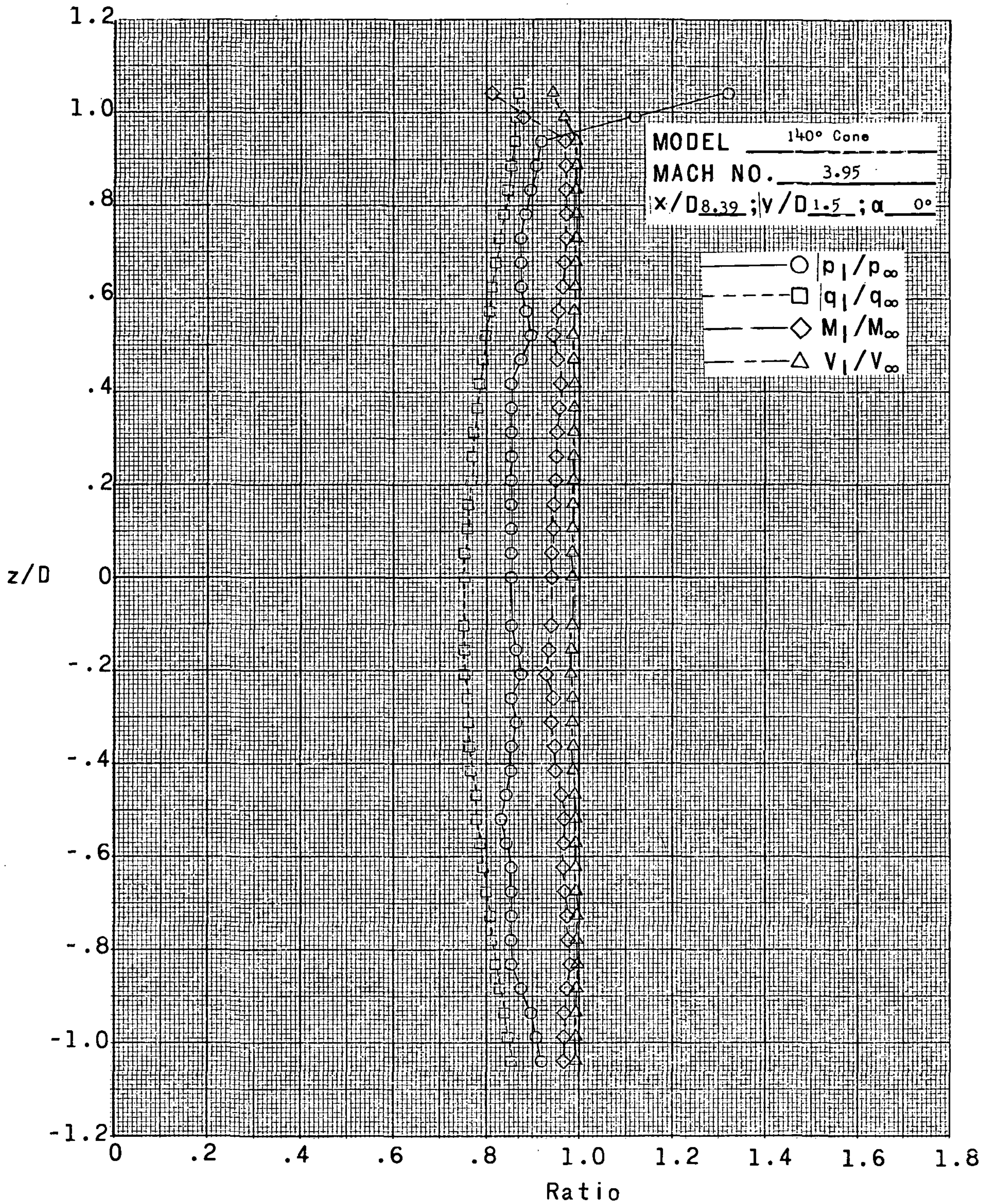
(cc) x/D = 8.39; y/D = 3.0; α = 0°.

Figure 8.- Continued.



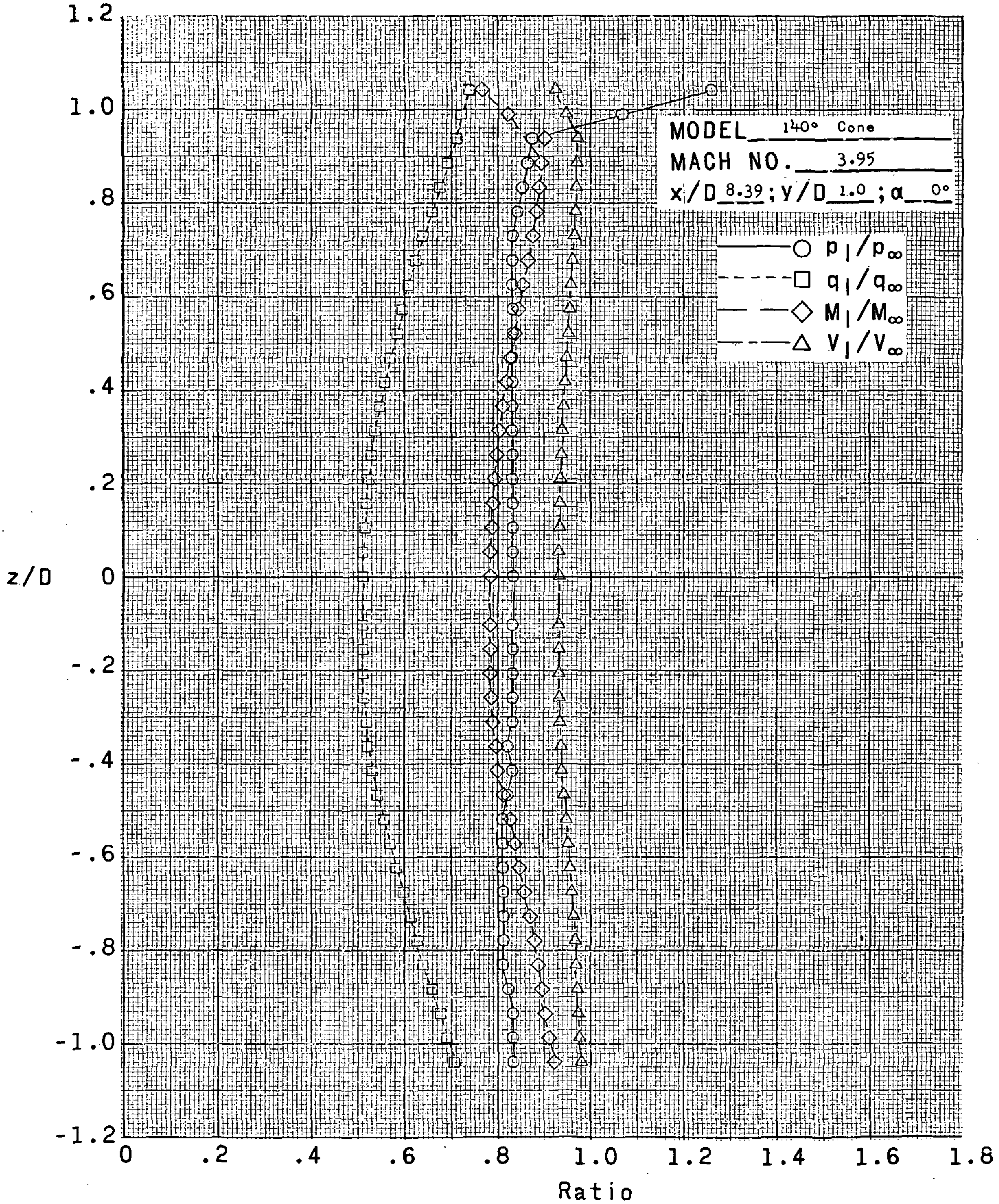
(dd) $x/D = 8.39$; $y/D = 2.0$; $\alpha = 0^0$.

Figure 8.- Continued.



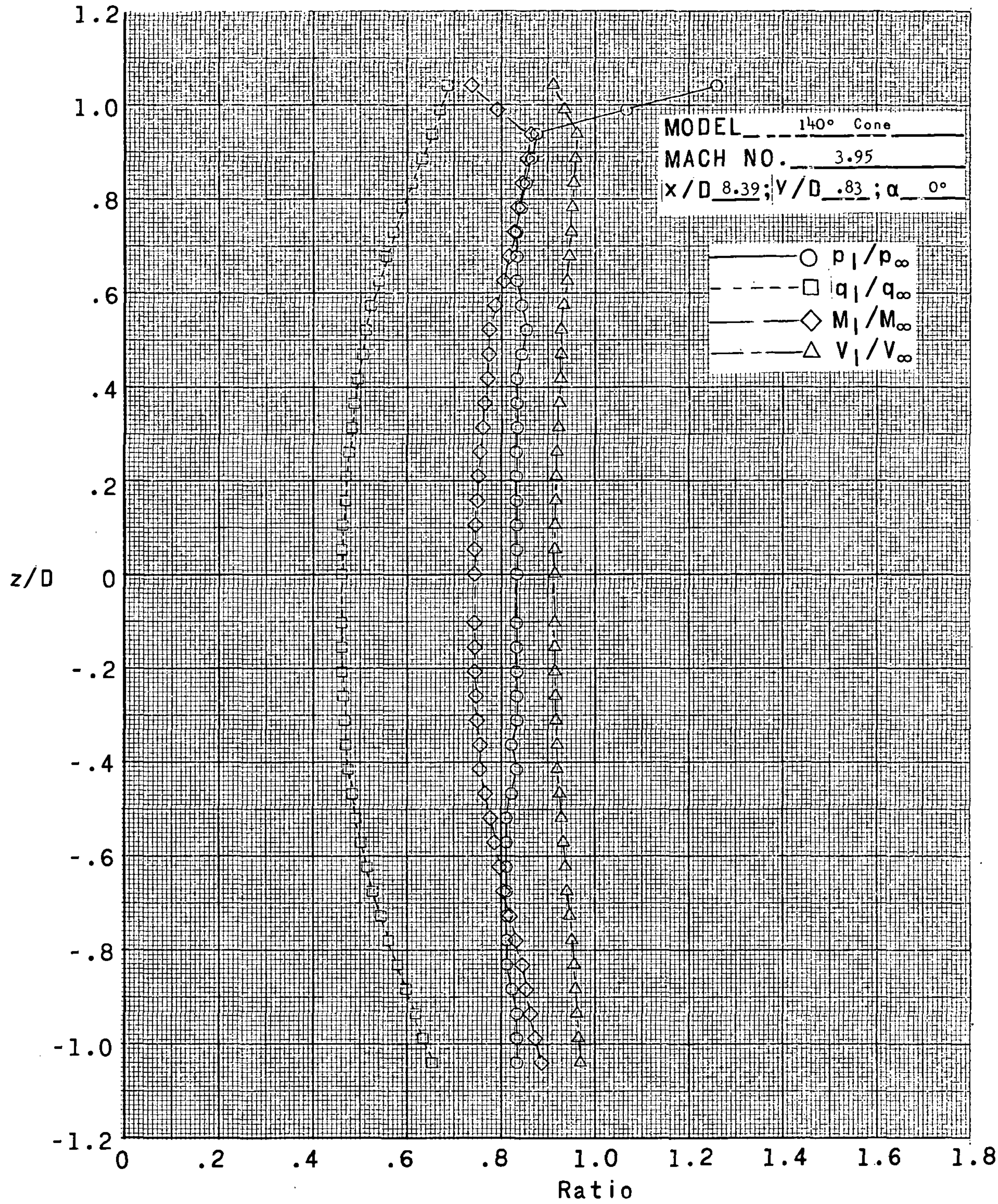
(ee) $x/D = 8.39$; $y/D = 1.5$; $\alpha = 0^{\circ}$.

Figure 8.- Continued.



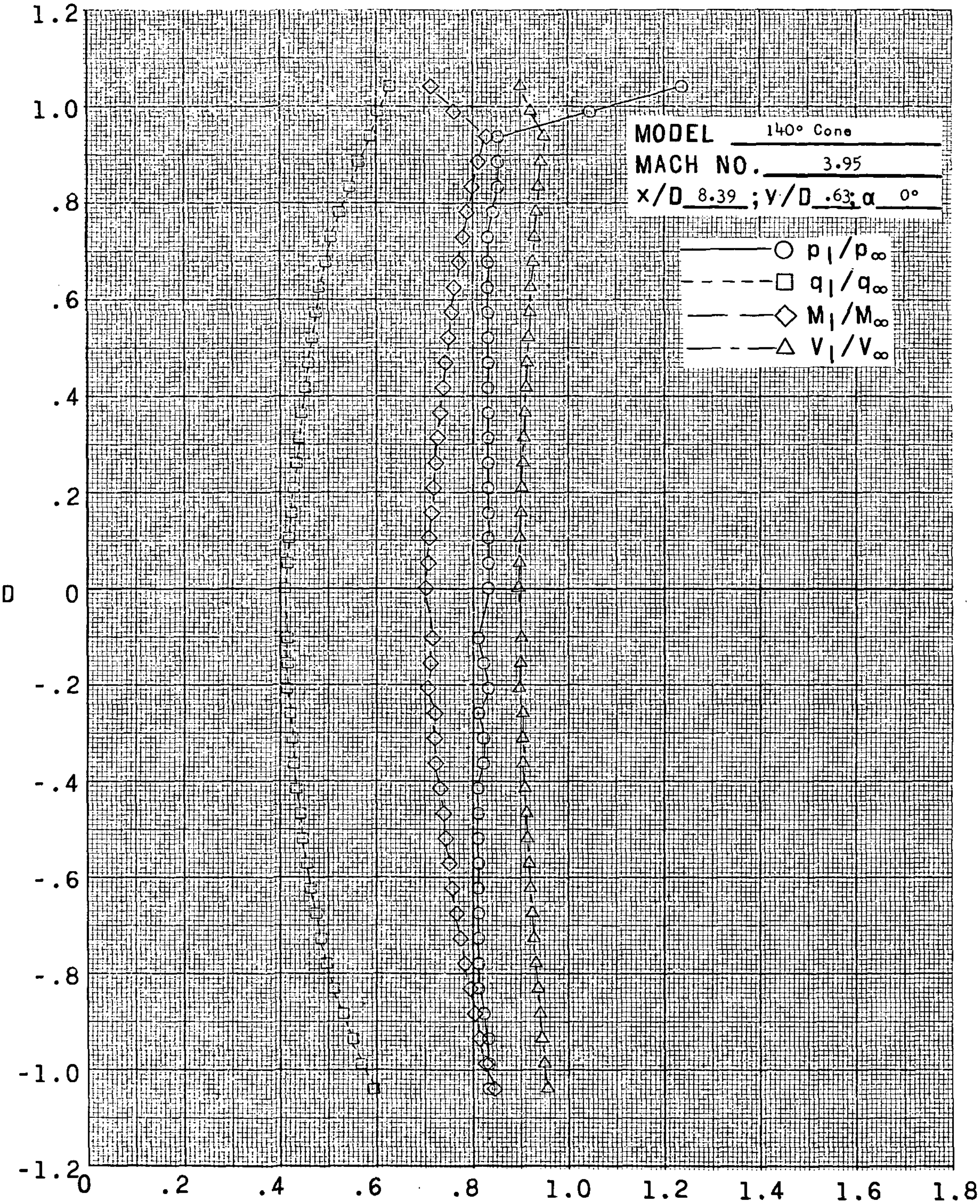
(ff) $x/D = 8.39$; $y/D = 1.0$; $\alpha = 0^\circ$.

Figure 8.- Continued.



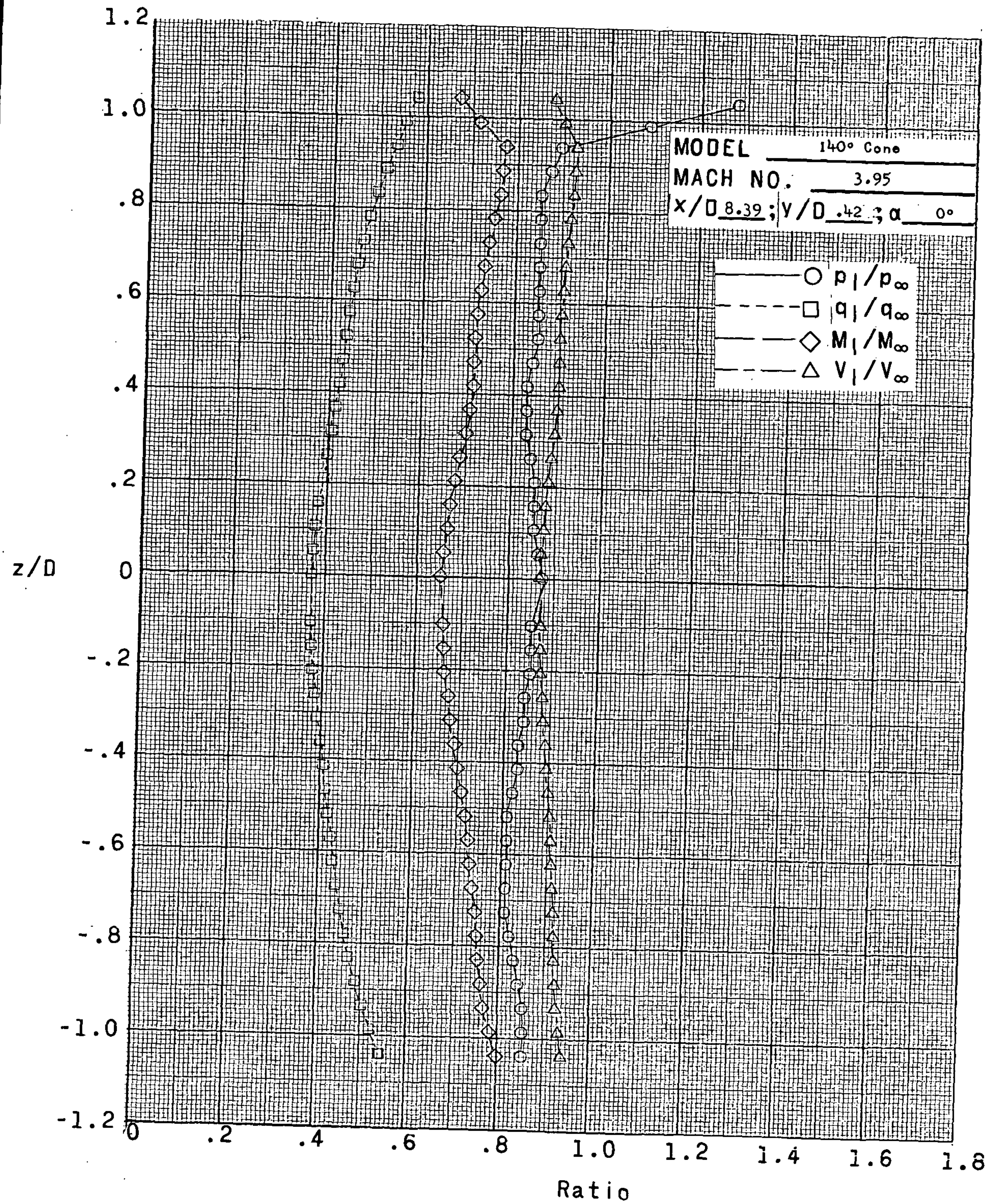
(gg) $x/D = 8.39$; $y/D = 0.83$; $\alpha = 0^0$.

Figure 8.- Continued.



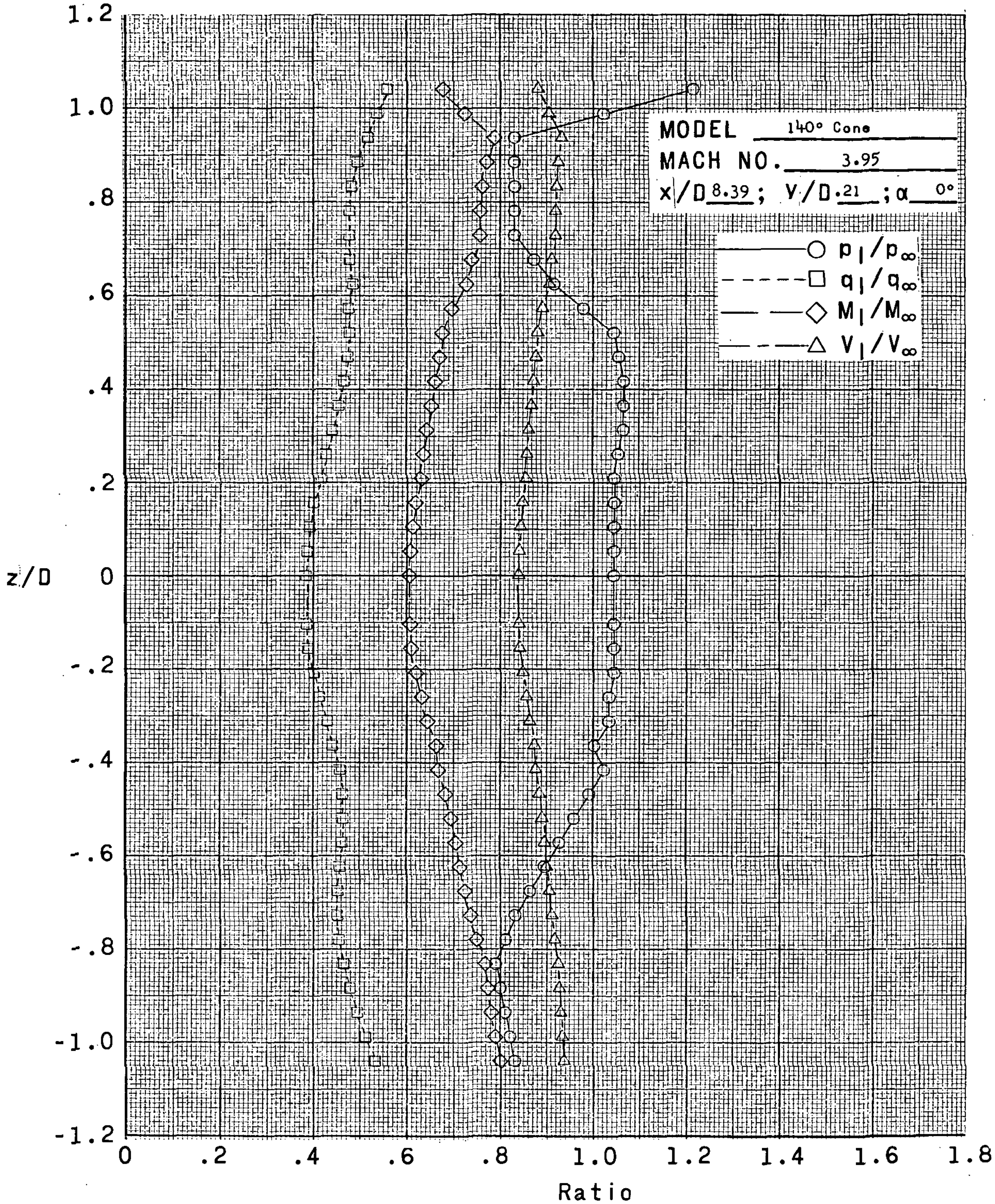
(hh) x/D = 8.39; y/D = 0.63; α = 0°.

Figure 8.- Continued.



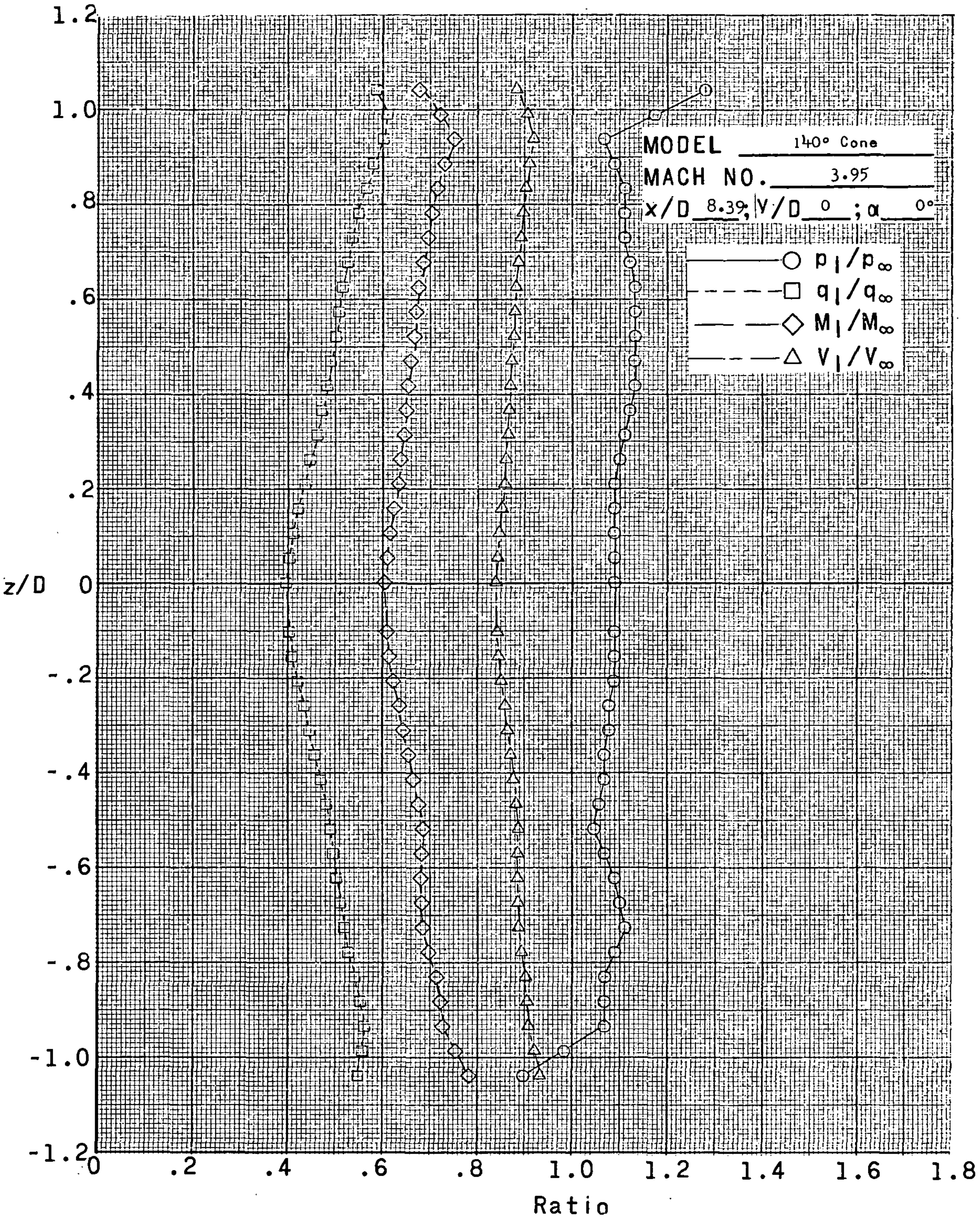
(ii) $x/D = 8.39$; $y/D = 0.42$; $\alpha = 0^o$.

Figure 8.- Continued.



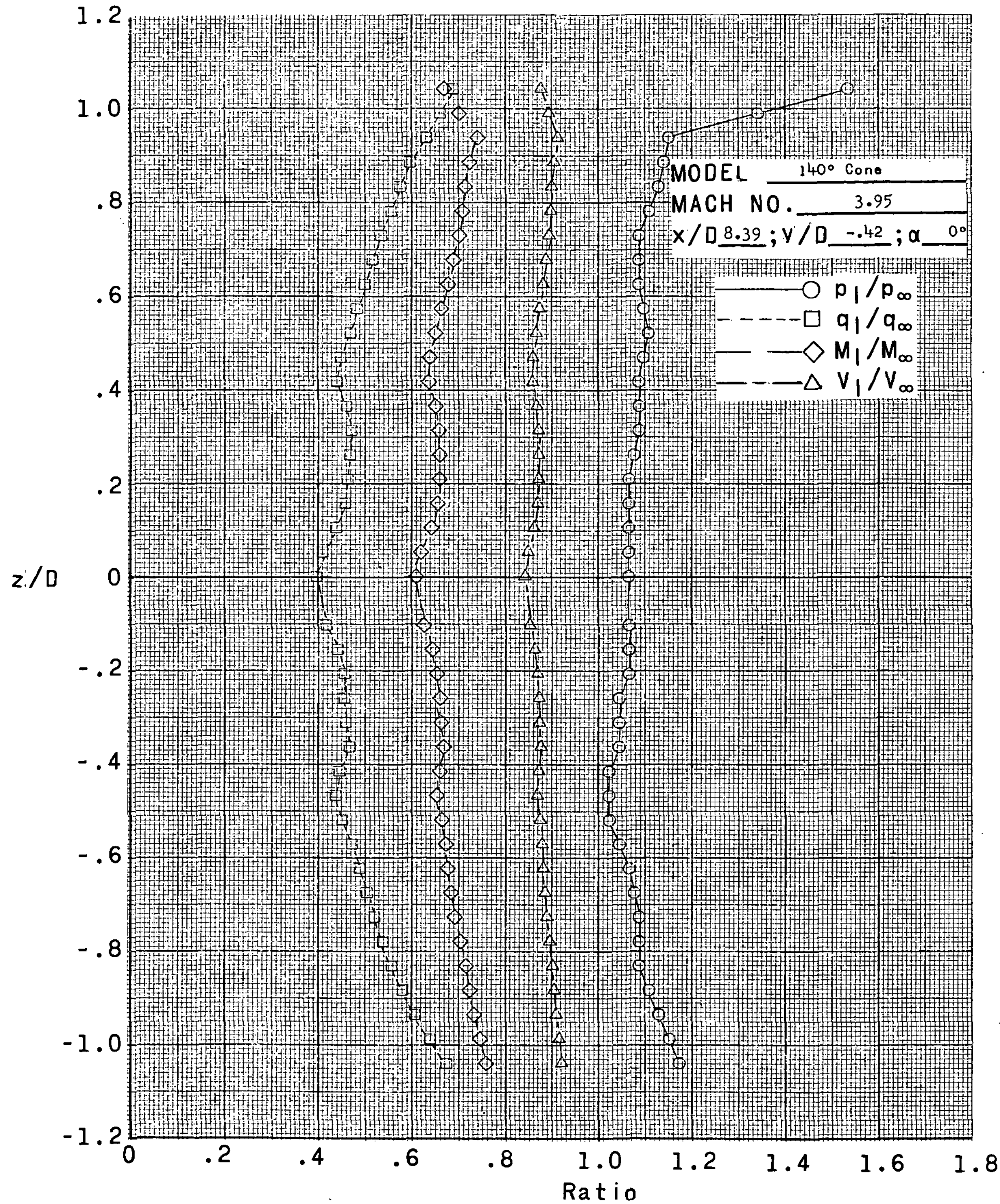
(jj) $x/D = 8.39$; $y/D = 0.21$; $\alpha = 0^0$.

Figure 8.- Continued.



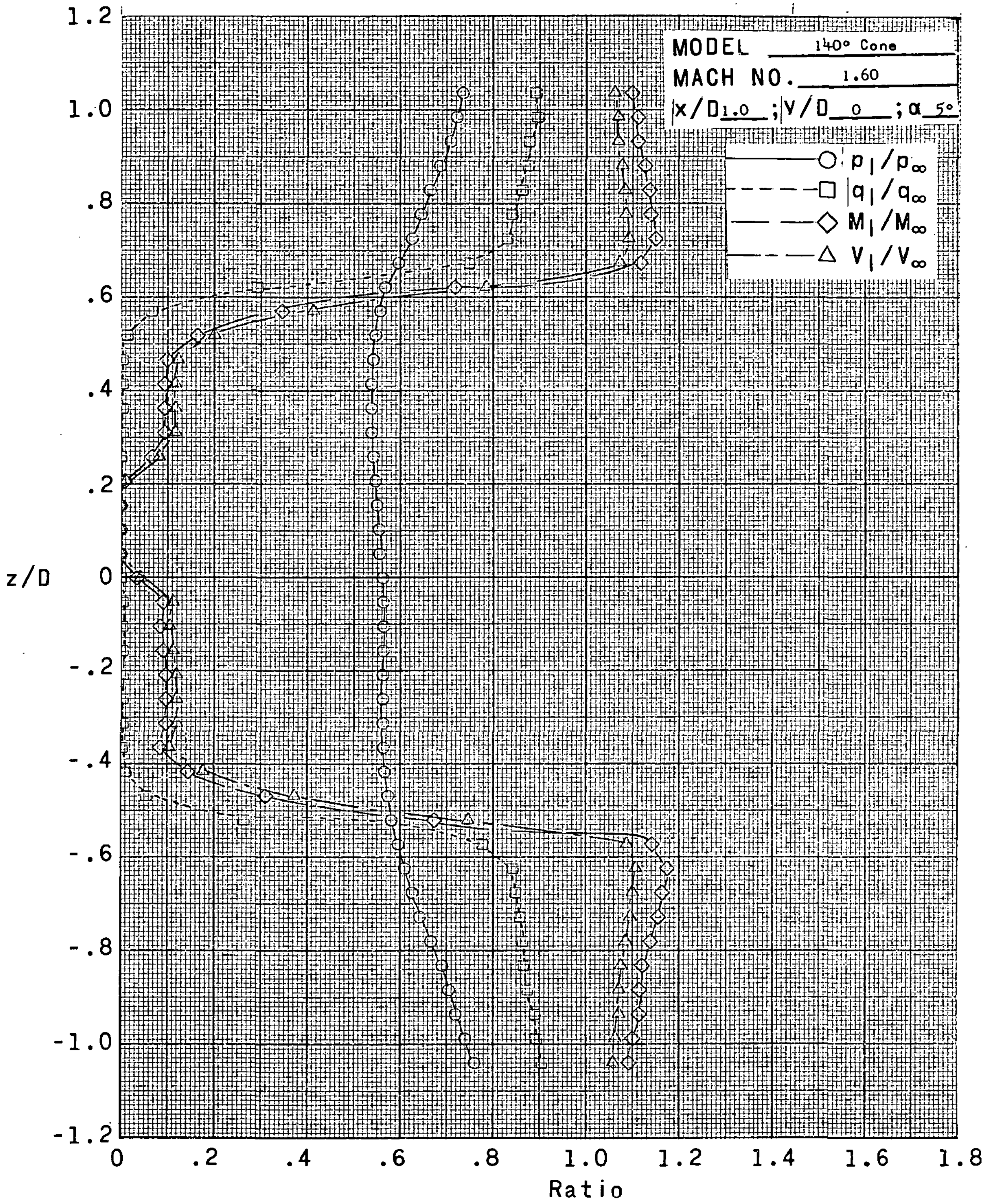
(kk) x/D = 8.39; y/D = 0; α = 0°.

Figure 8.- Continued.



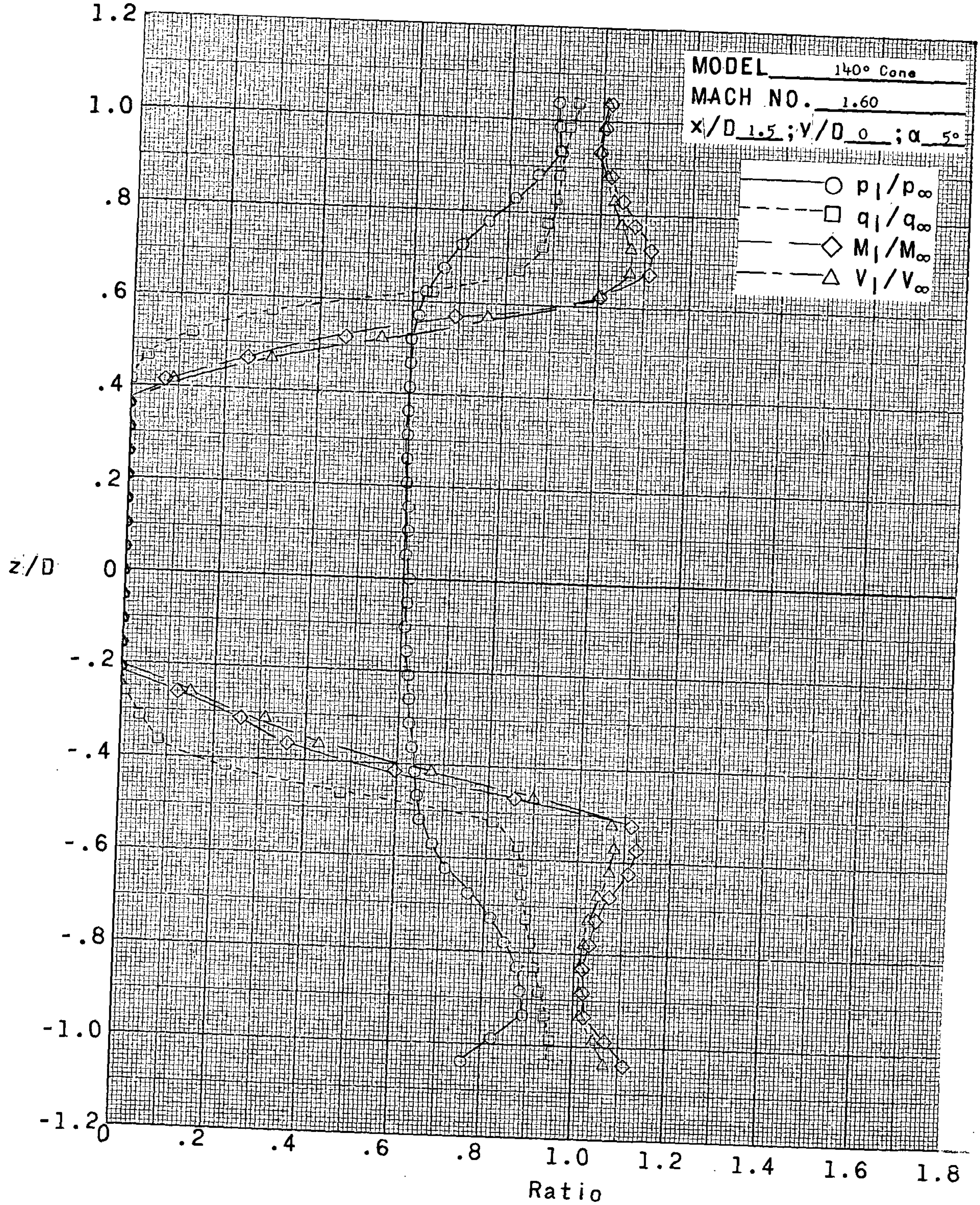
(ll) x/D = 8.39; y/D = -0.42; α = 0°.

Figure 8.- Concluded.



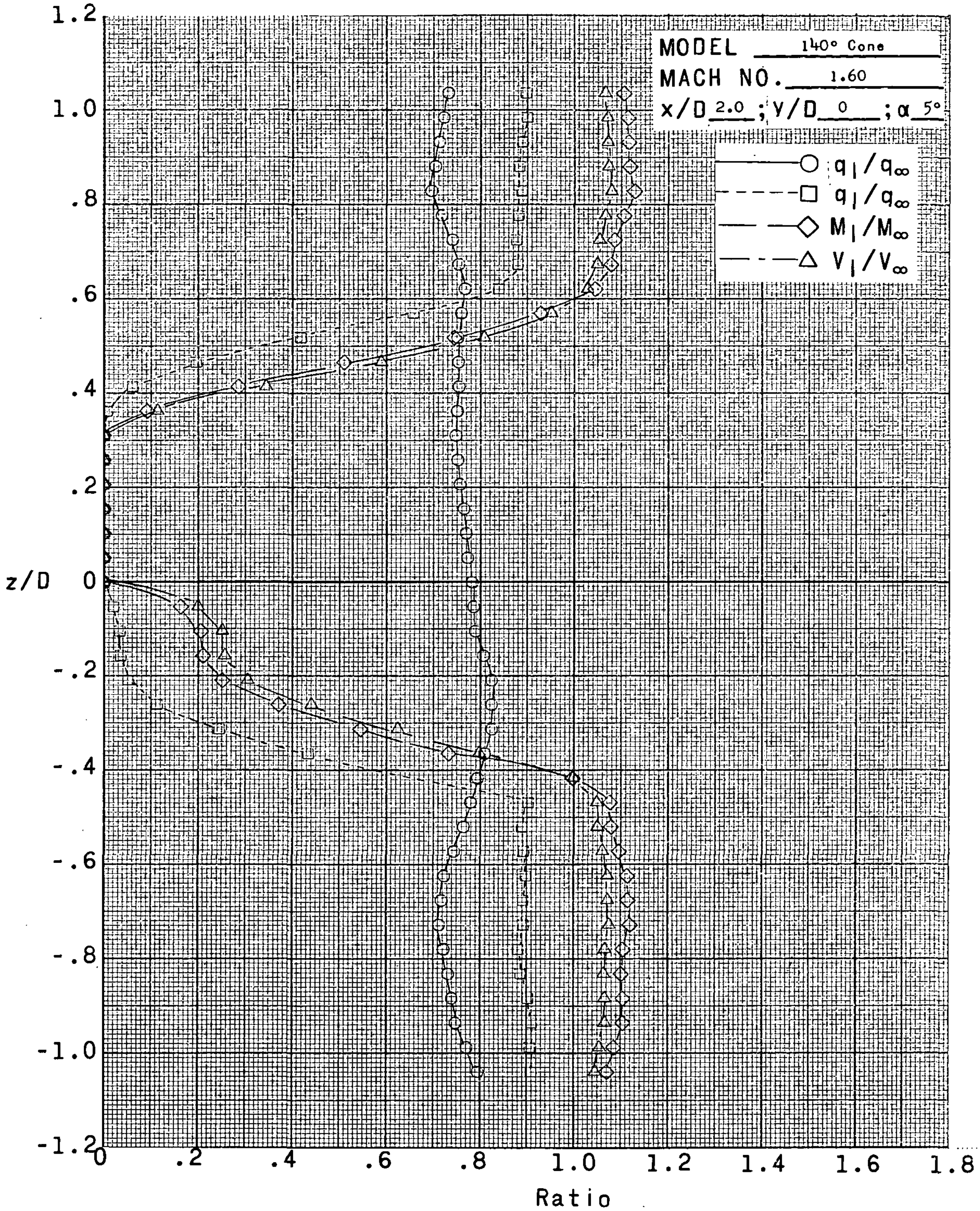
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 9.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D in center of wake of a 140°-included-angle cone at a Mach number of 1.60 and a Reynolds number of 5.42×10^6 per meter (1.65×10^6 per foot).



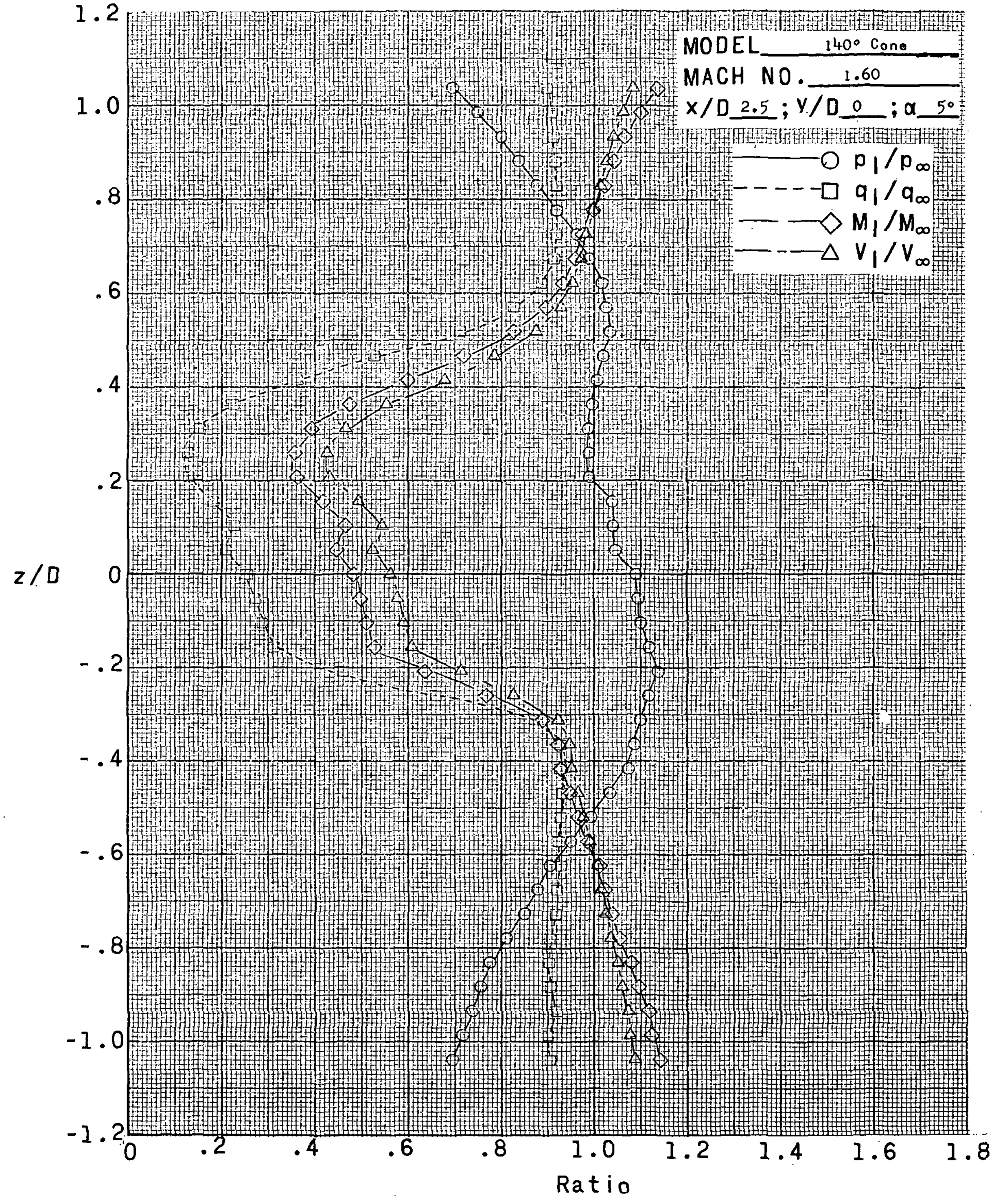
(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 9.- Continued.



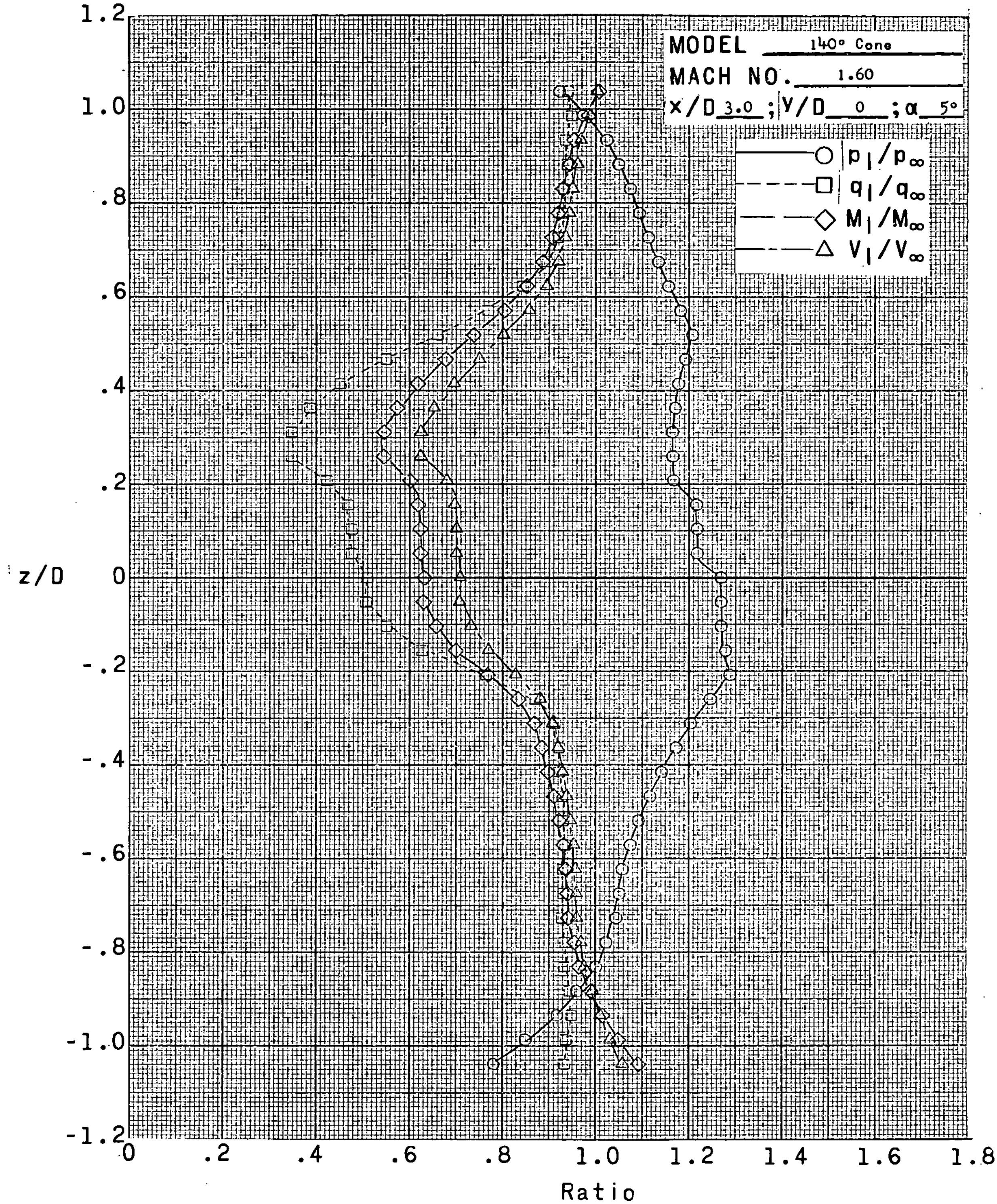
(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 9.- Continued.



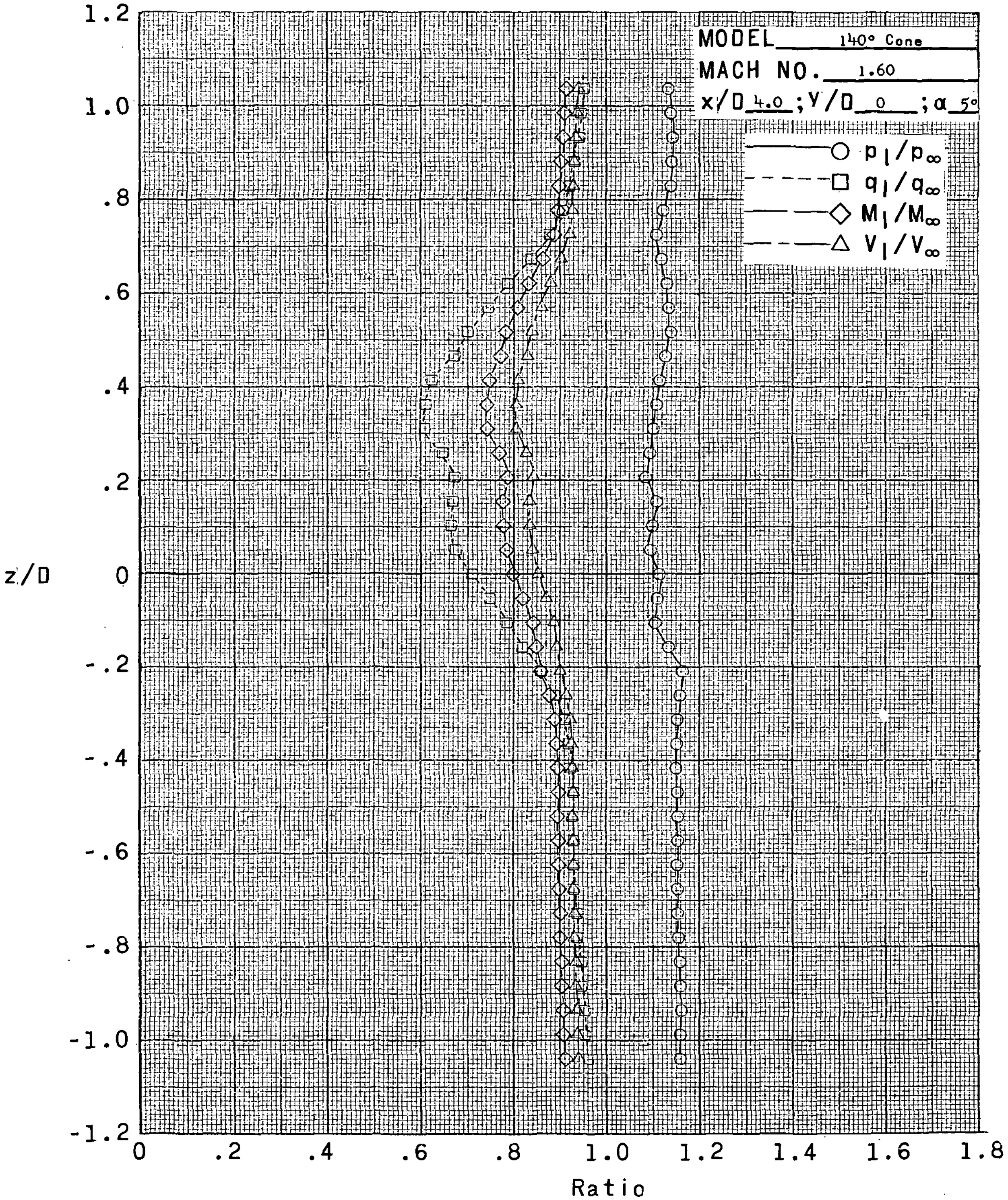
(d) $x/D = 2.5$; $y/D = 0$; $\alpha = 5^0$.

Figure 9.- Continued.



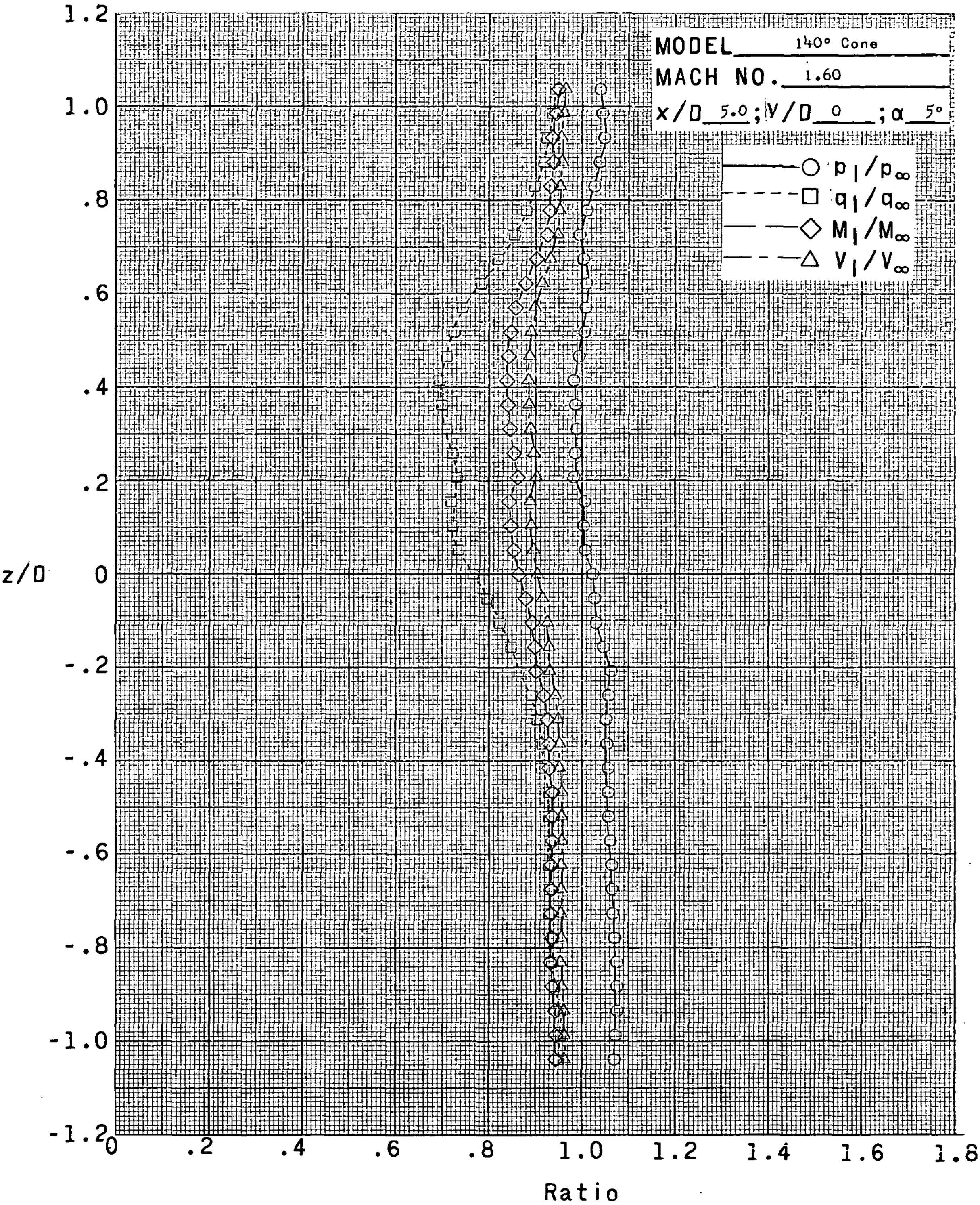
(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 9.- Continued.



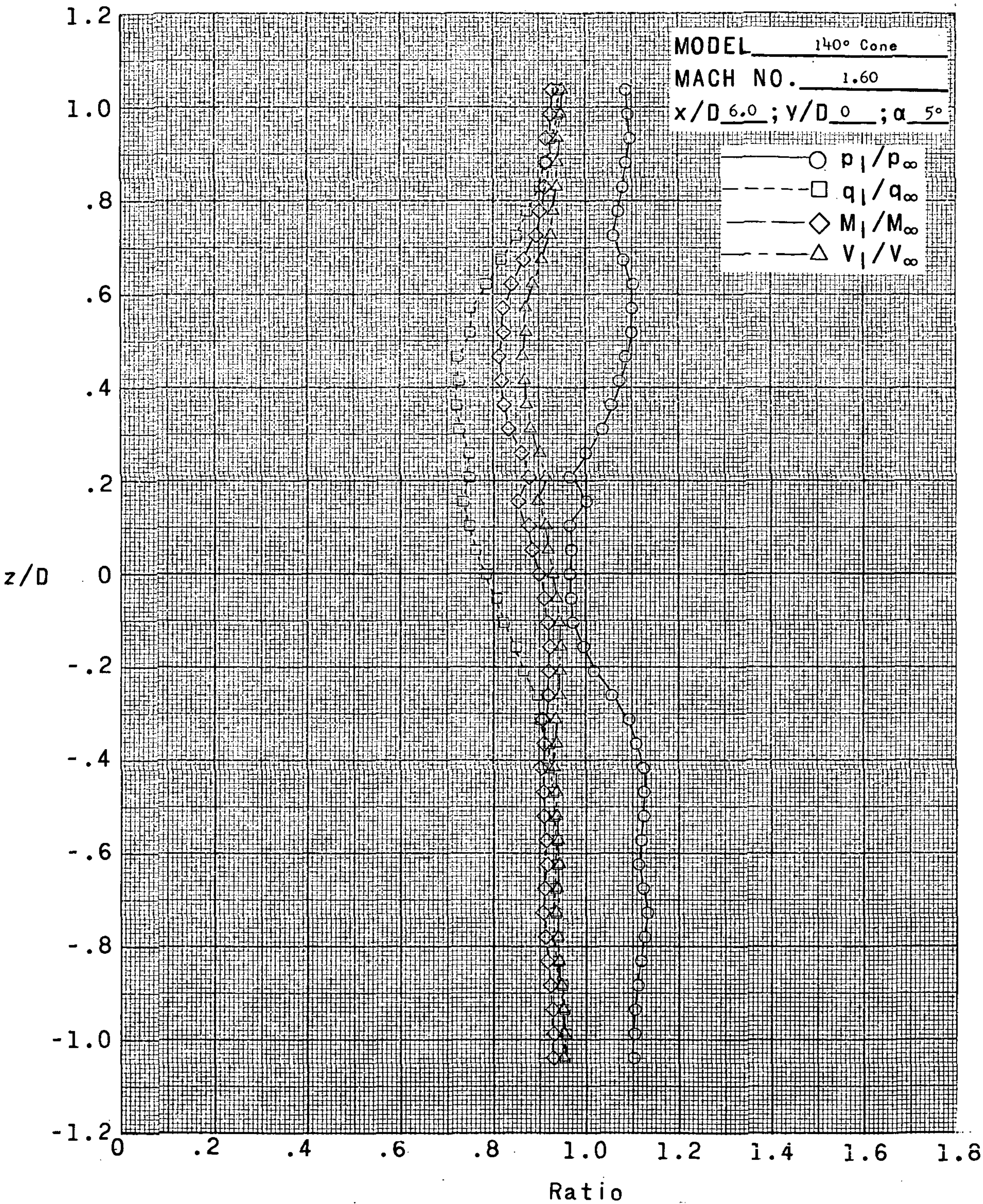
(f) x/D = 4.0; y/D = 0; α = 5°.

Figure 9.- Continued.



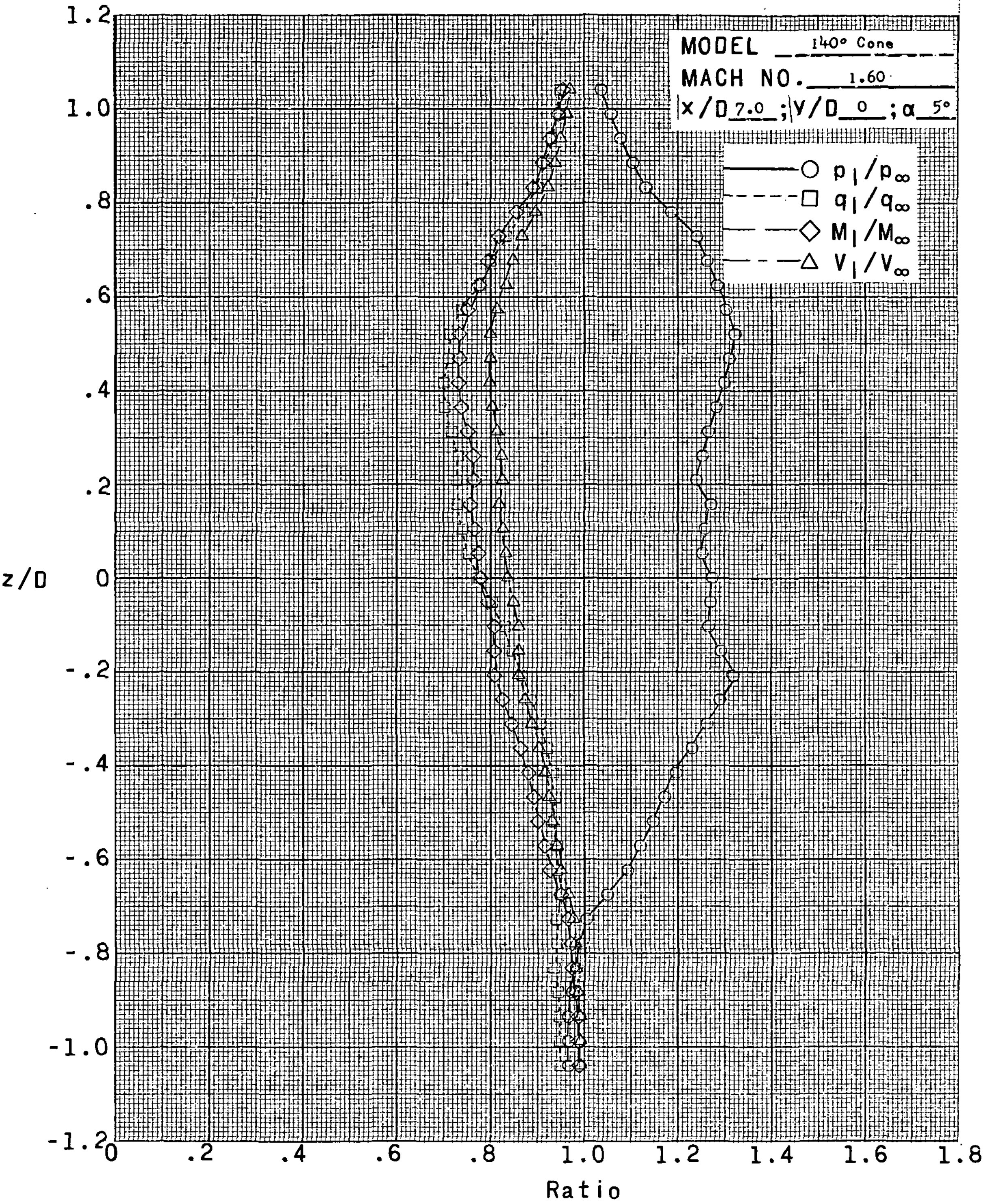
(g) x/D = 5.0; y/D = 0; α = 5°.

Figure 9.- Continued.



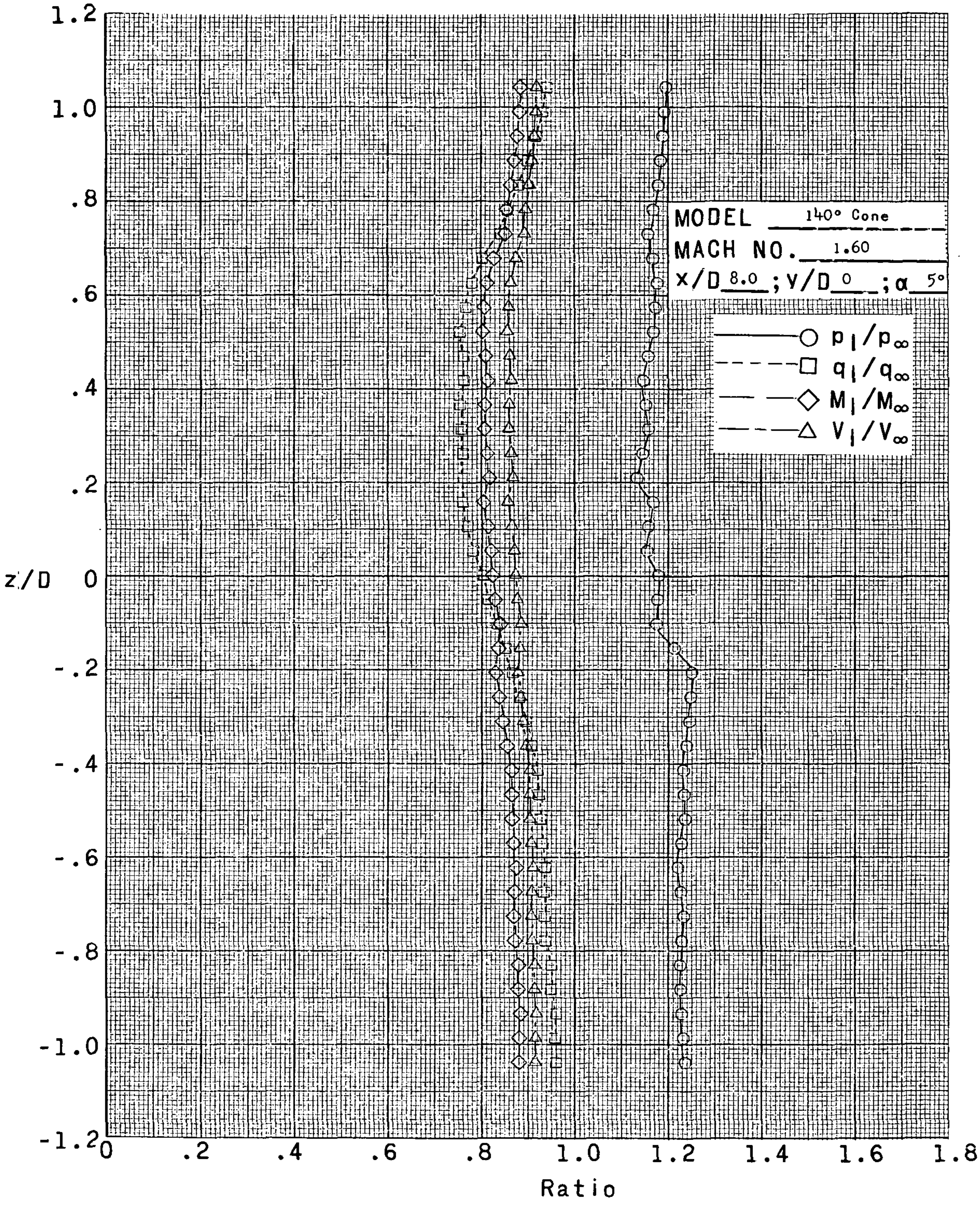
(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 9.- Continued.



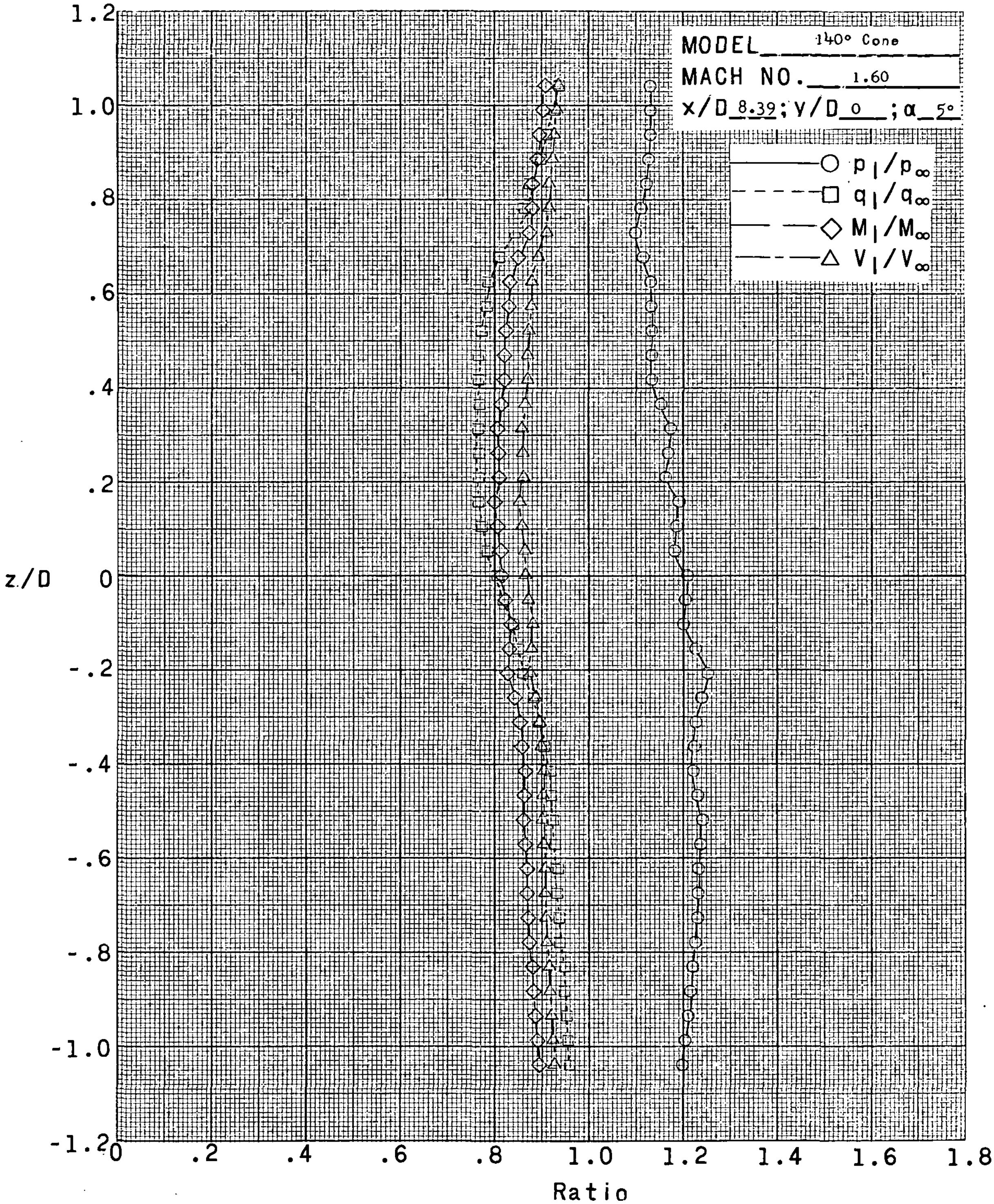
(i) x/D = 7.0; y/D = 0; α = 5°.

Figure 9.- Continued.



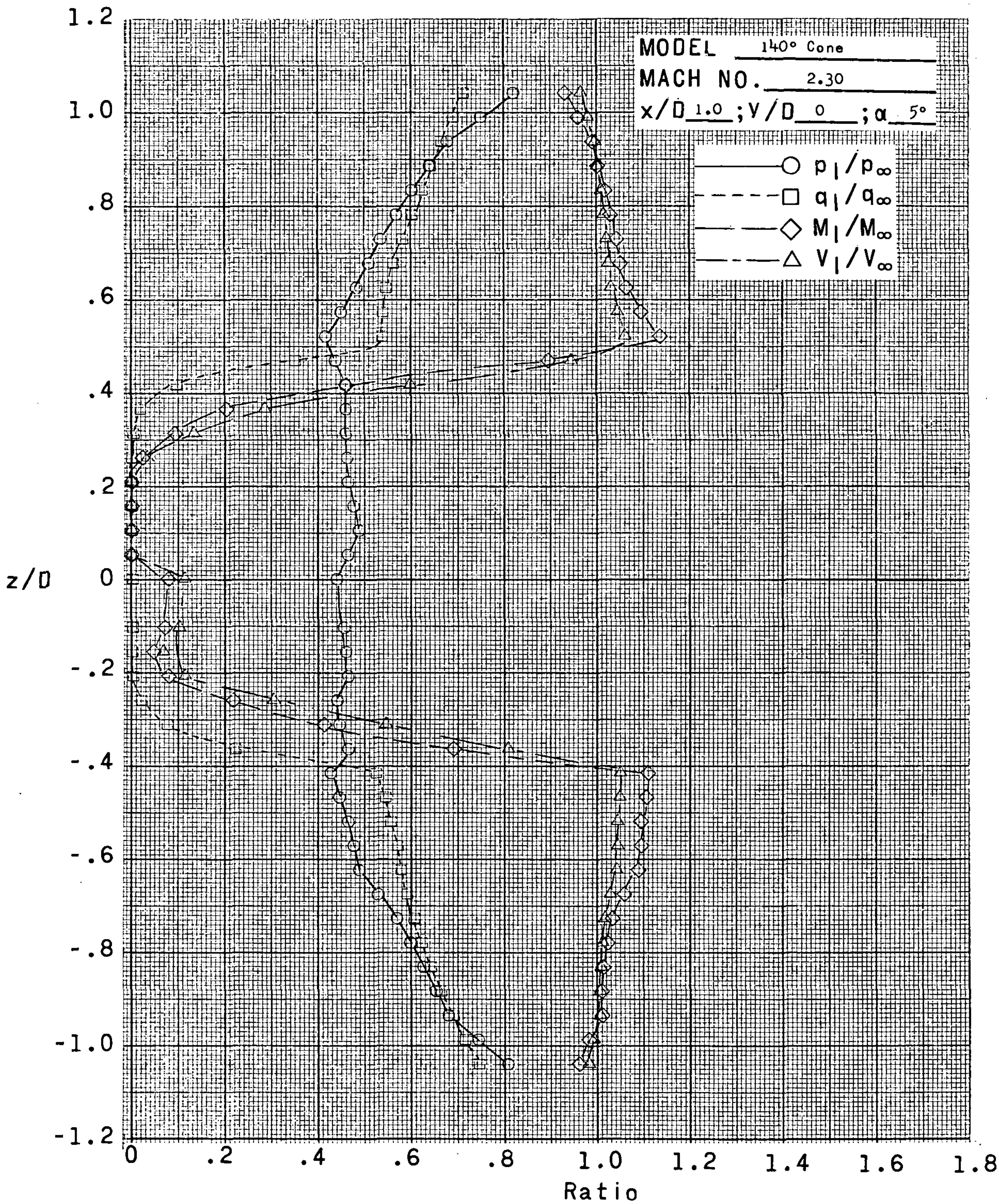
(j) $x/D = 8.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 9.- Continued.



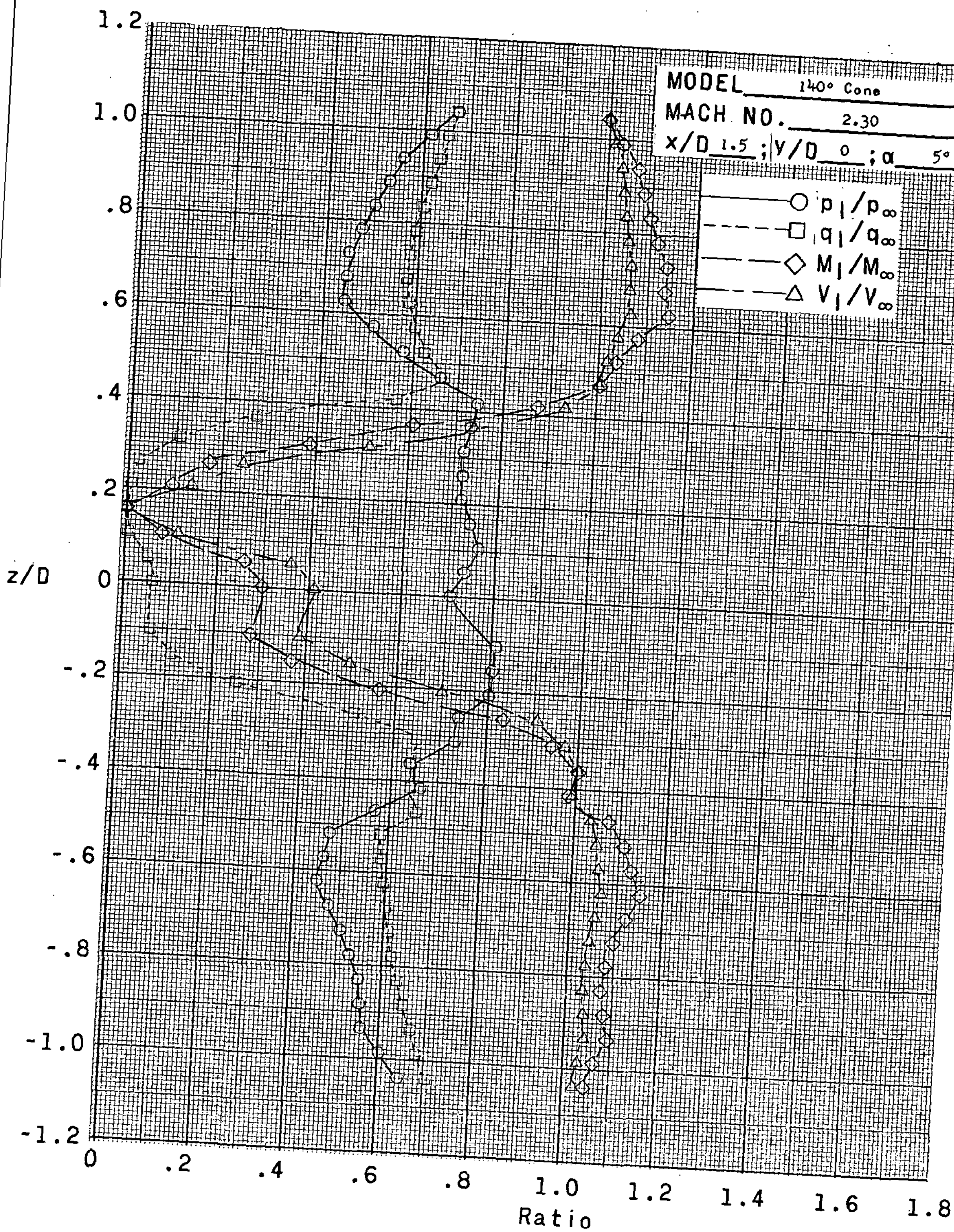
(k) $x/D = 8.39$; $y/D = 0$; $\alpha = 5^{0}$.

Figure 9.- Concluded.



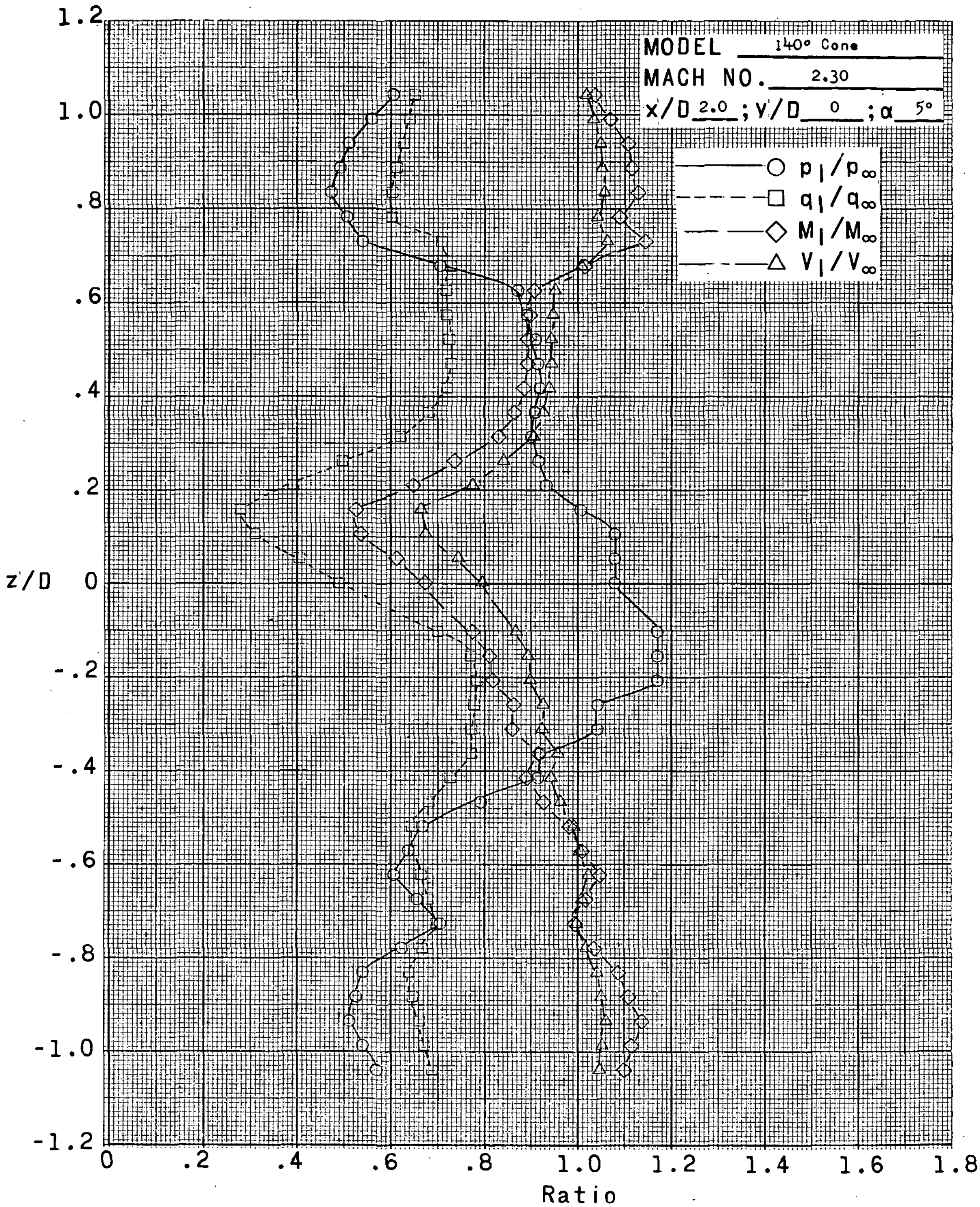
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 10.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D at center of wake of 140°-included-angle cone at Mach number of 2.30 and Reynolds number of 5.42×10^6 per meter $(1.65 \times 10^6$ per foot).



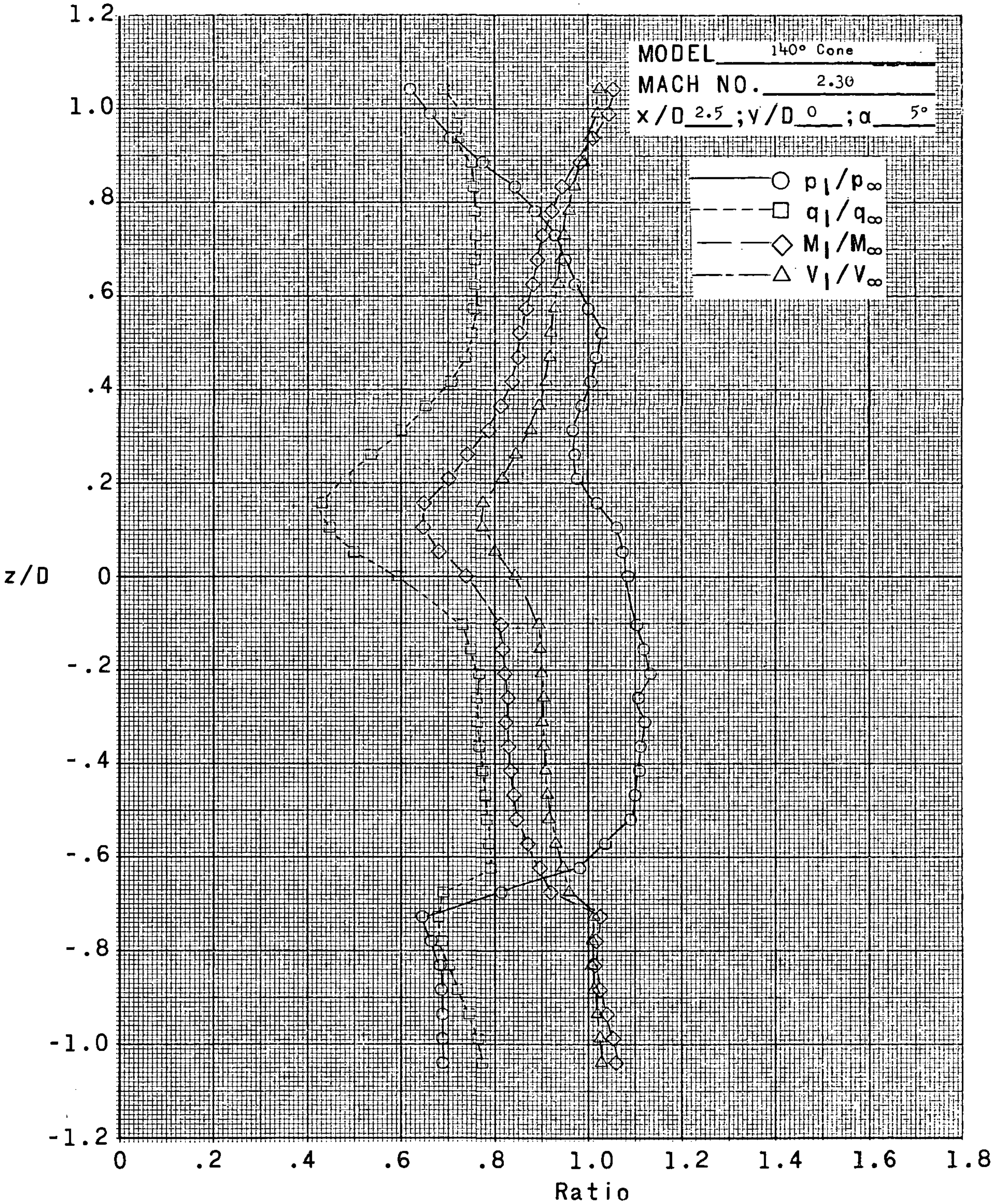
(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 5^0$.

Figure 10.- Continued.



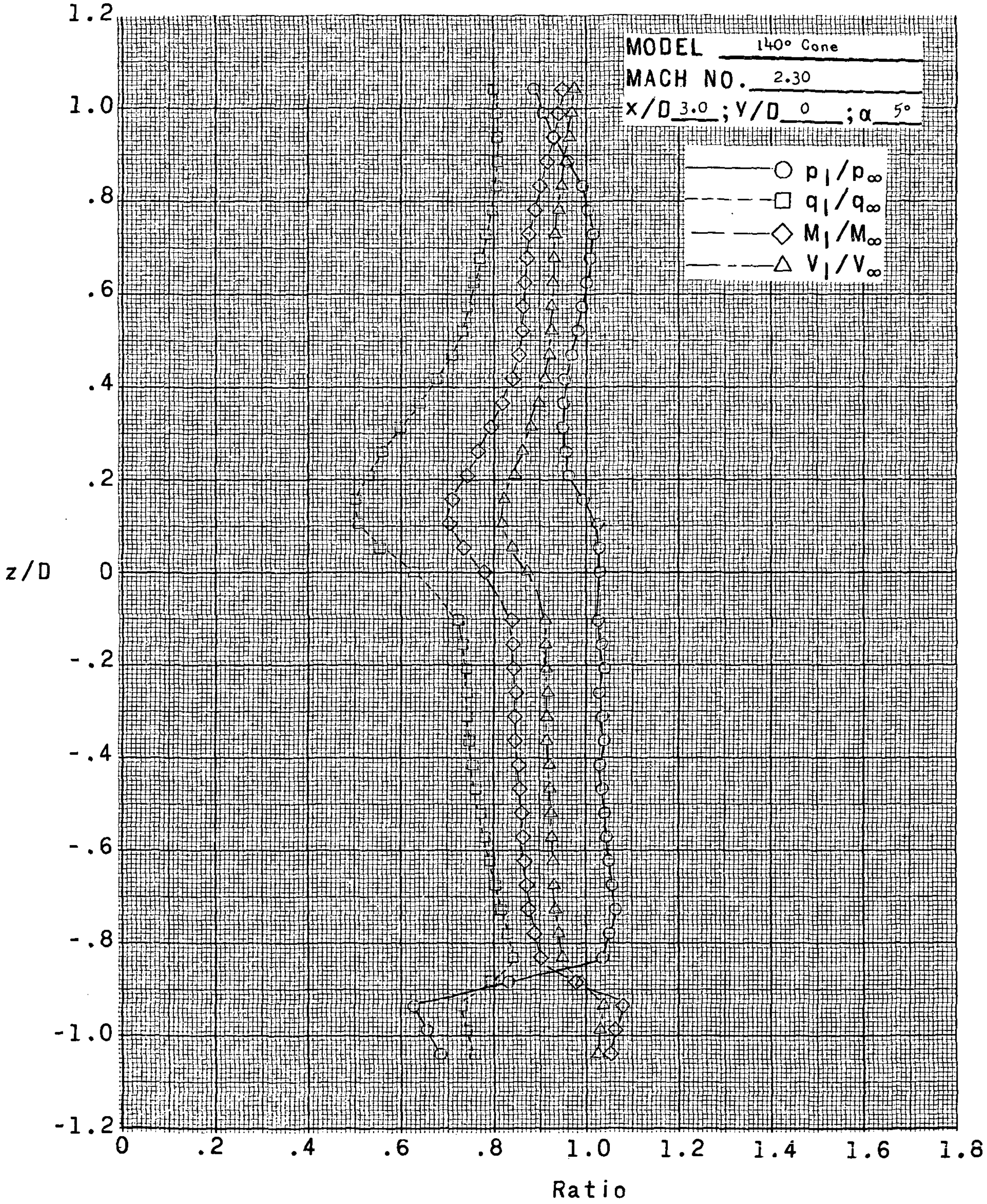
(c) x/D = 2.0; y/D = 0; α = 5°.

Figure 10.- Continued.



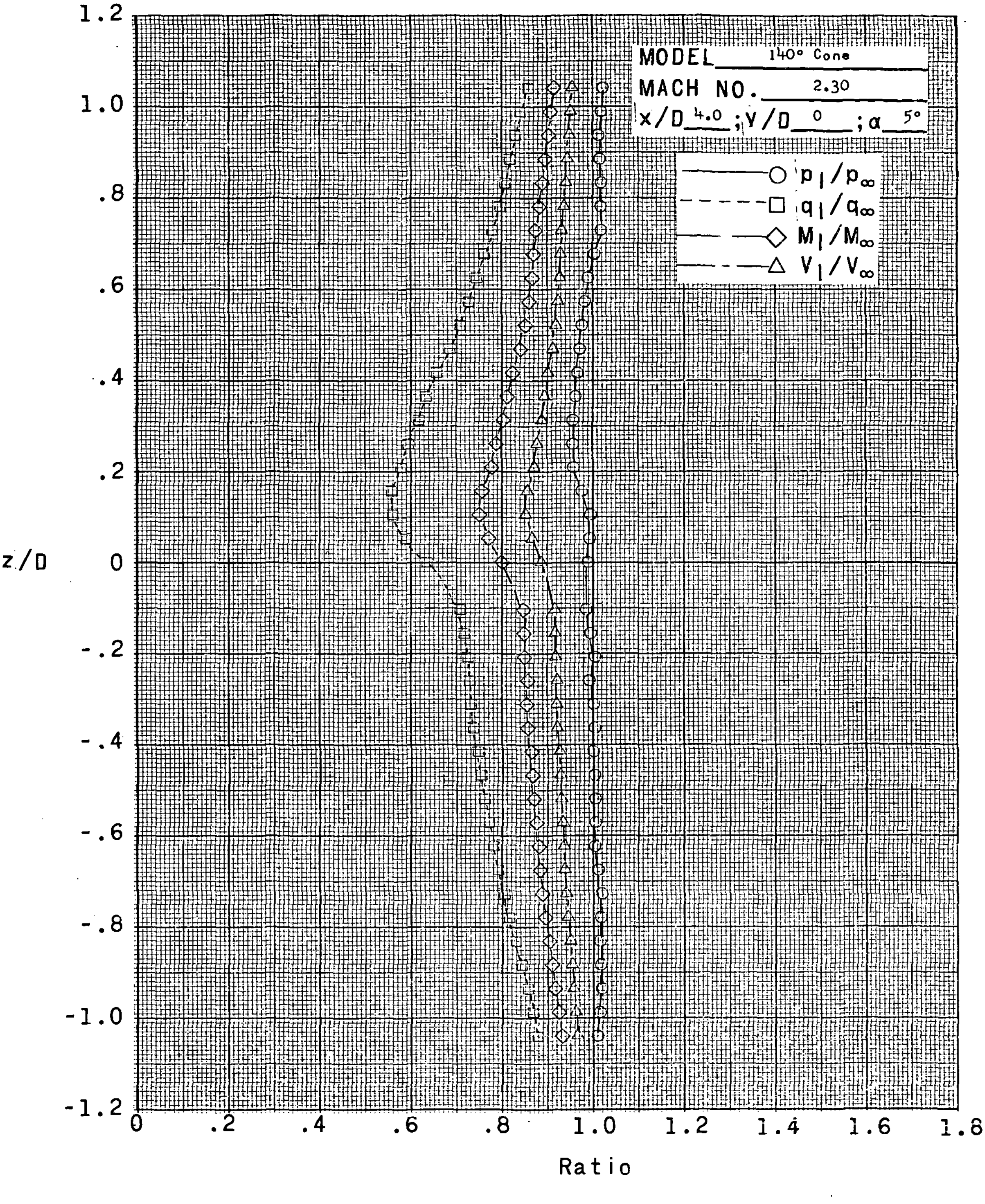
(d) $x/D = 2.5$; $y/D = 0$; $\alpha = 5^0$.

Figure 10.- Continued.



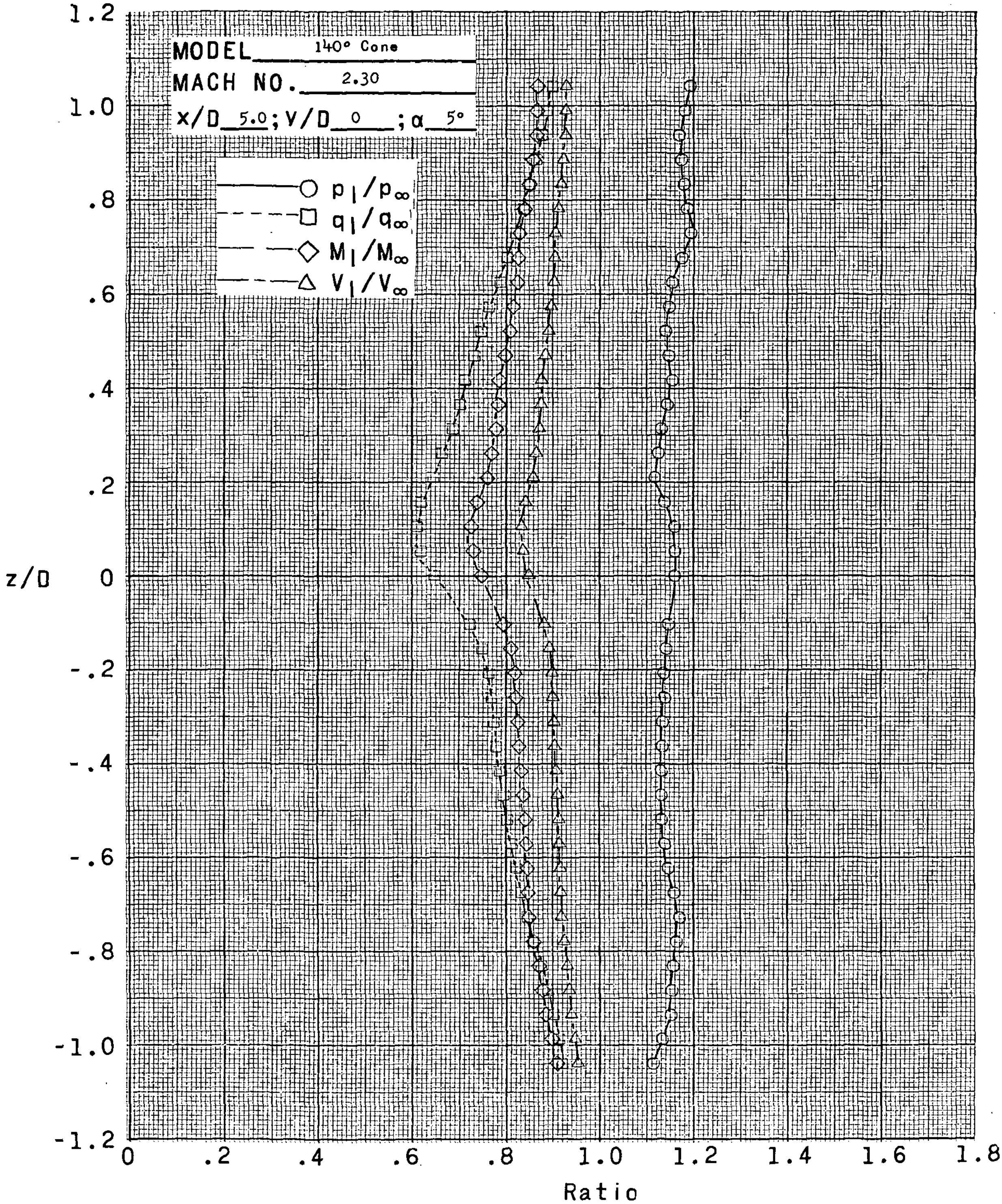
(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 10.- Continued.



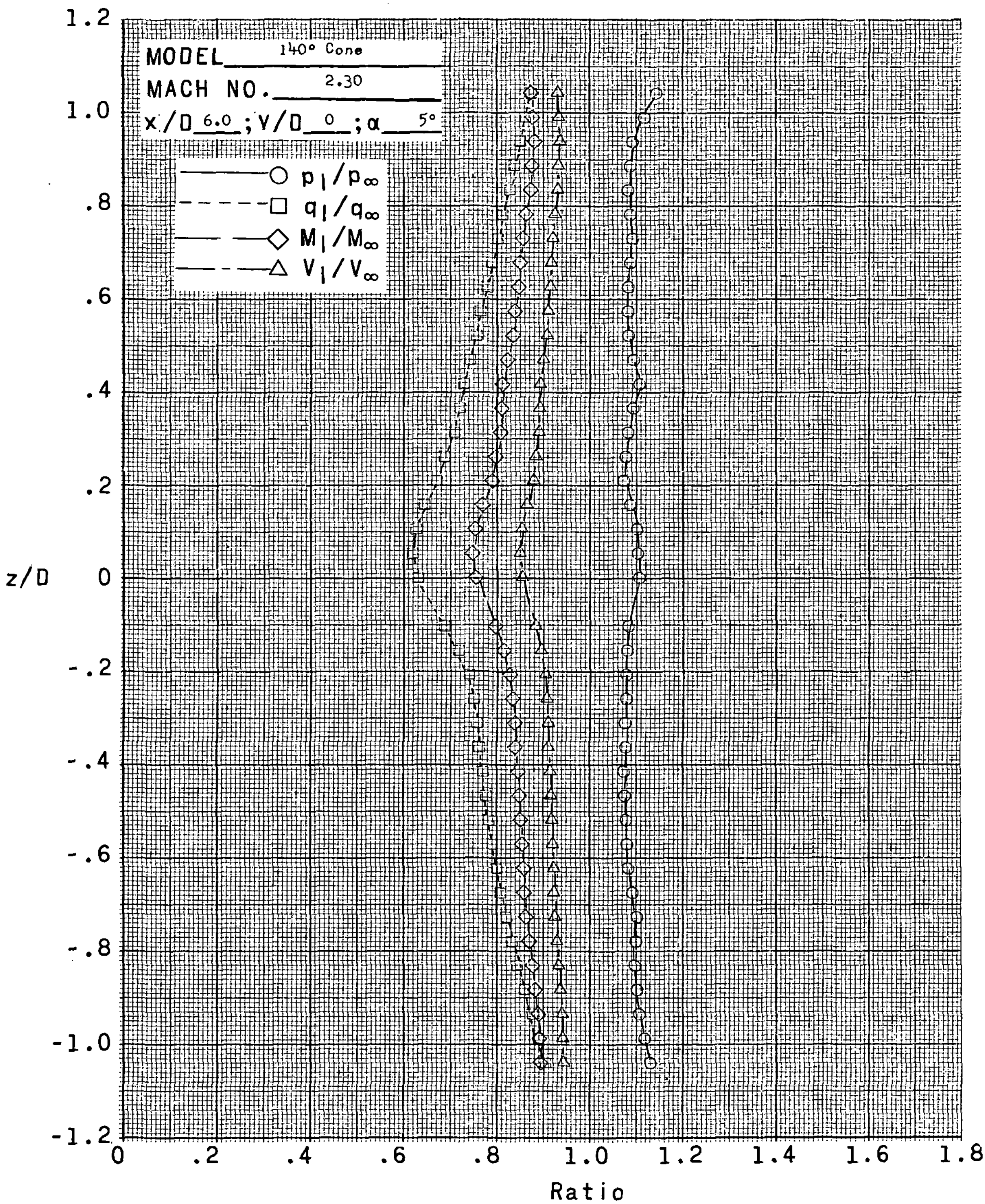
(f) $x/D = 4.0$; $y/D = 0$; $\alpha = 5°$.

Figure 10.- Continued.



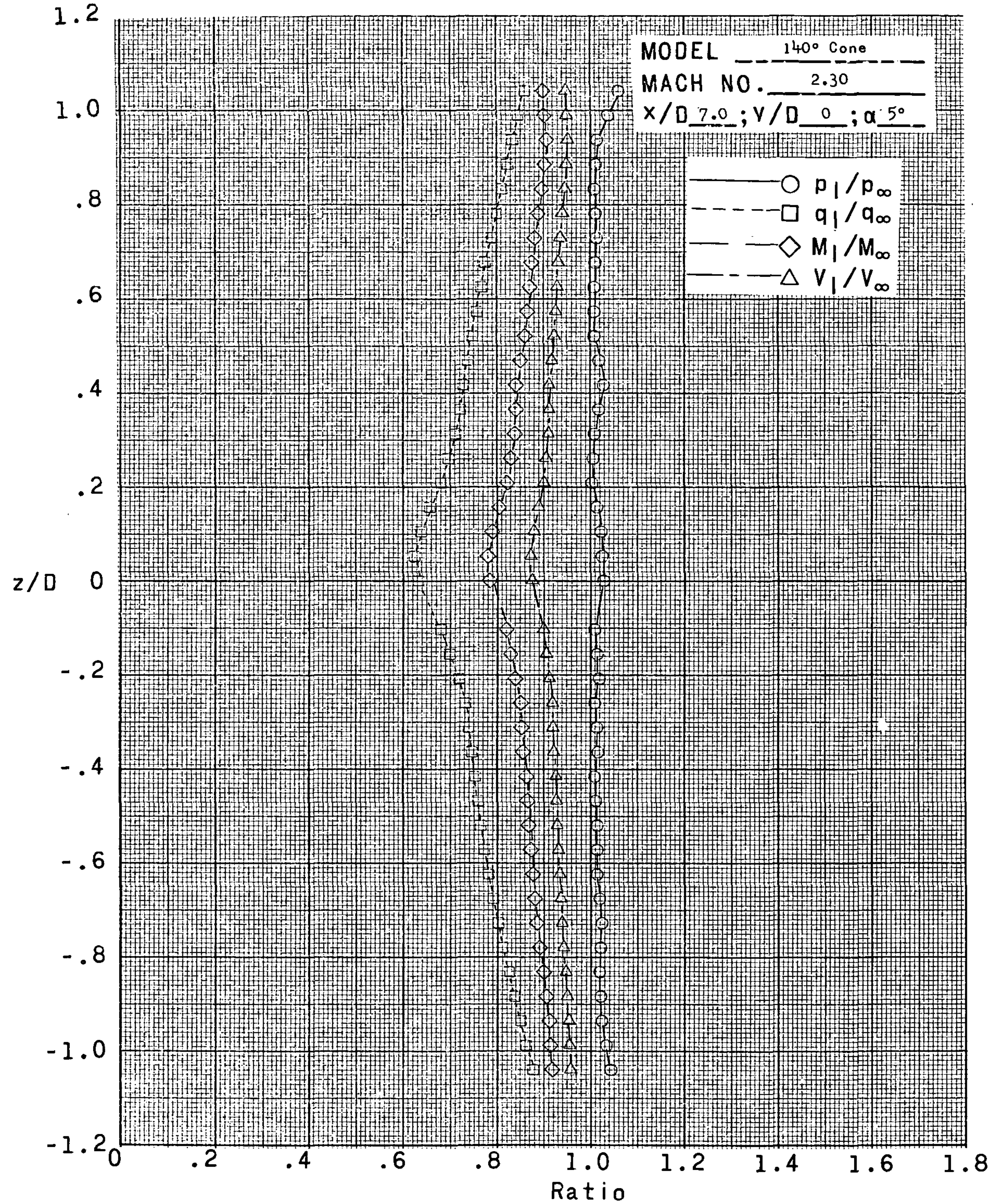
(g) x/D = 5.0; y/D = 0; α = 5°.

Figure 10.- Continued.



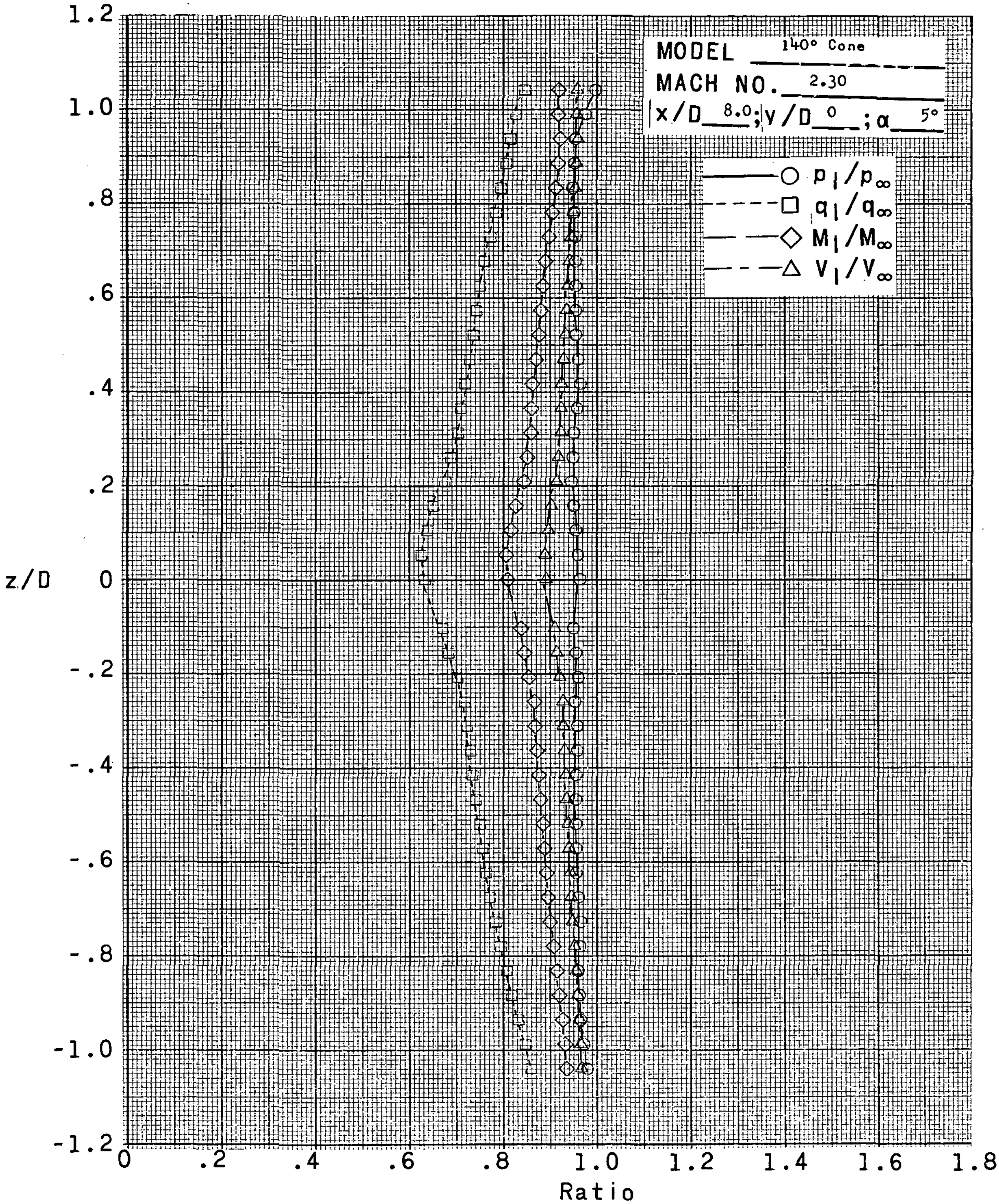
(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 10.- Continued.



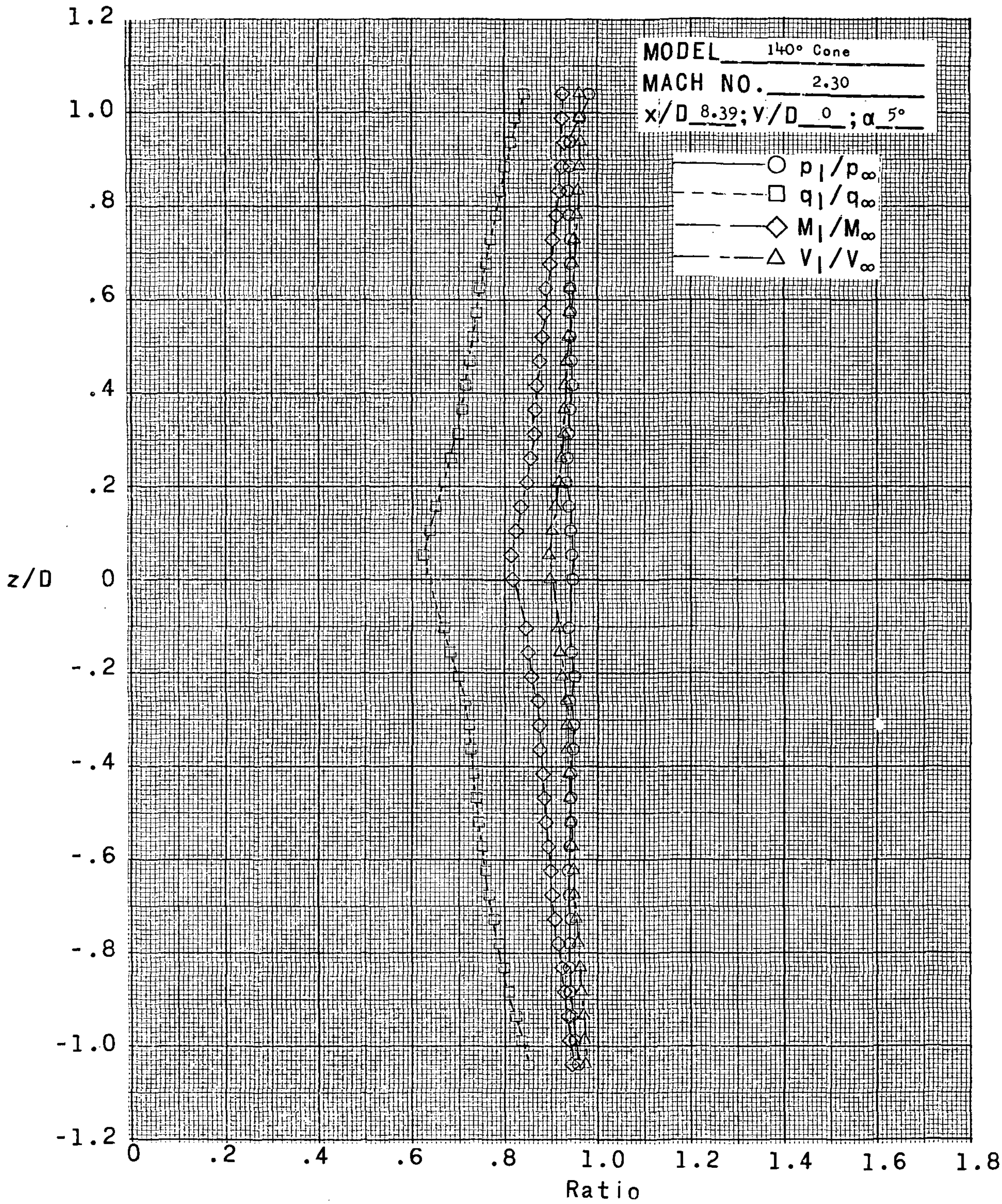
(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 10.- Continued.



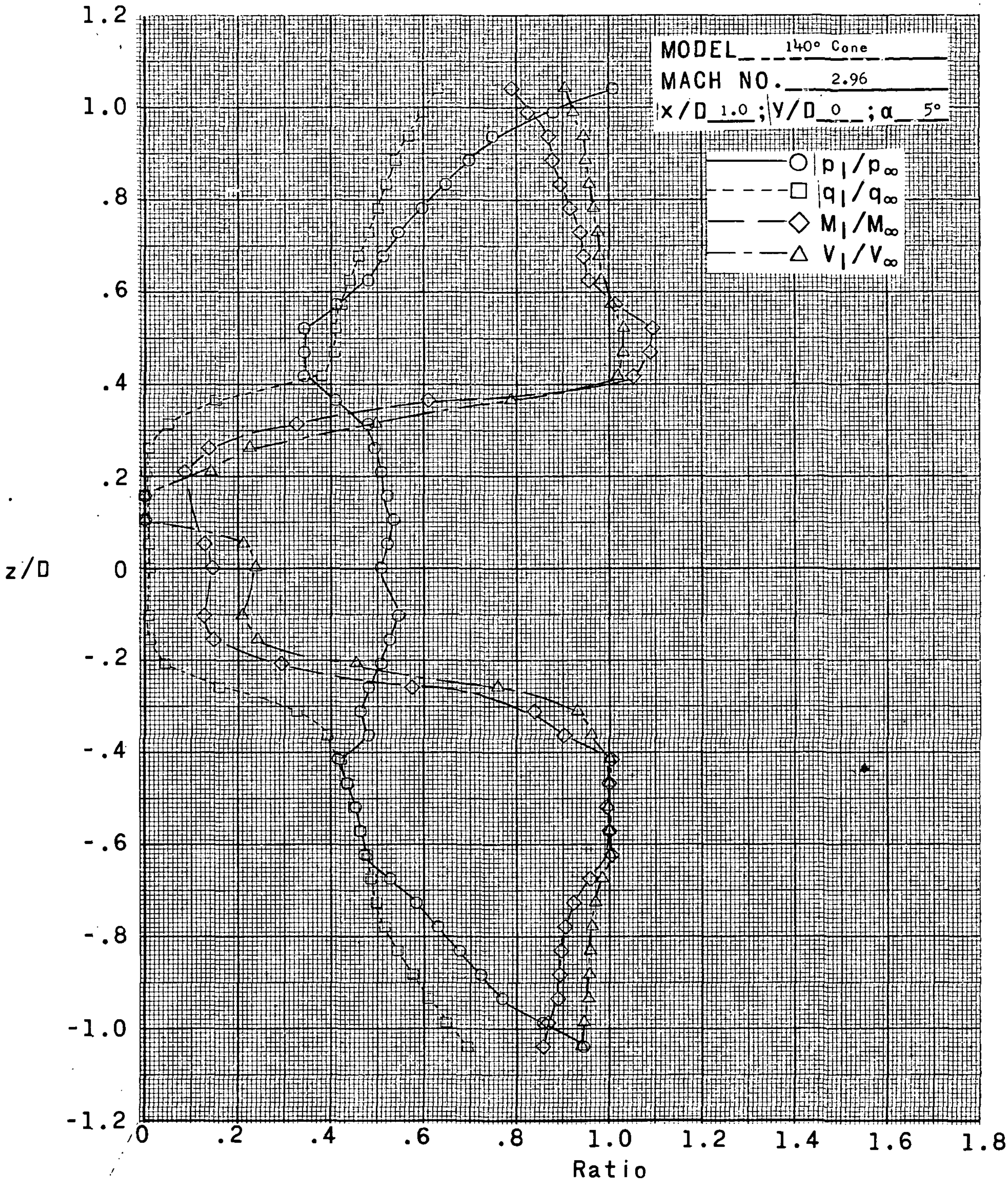
(j) x/D = 8.0; y/D = 0; α = 5°.

Figure 10.- Continued.



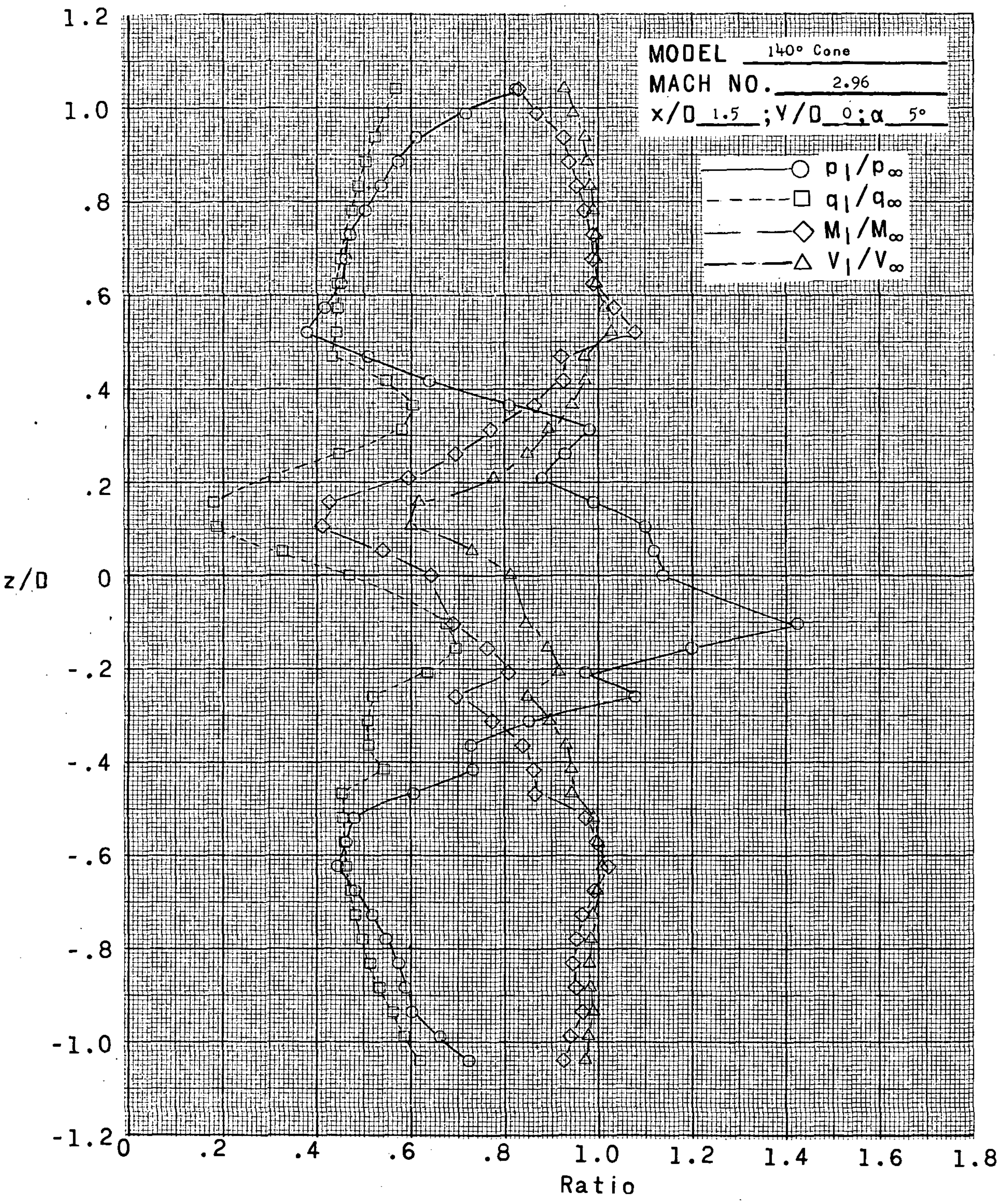
(k) $x/D = 8.39$; $y/D = 0$; $\alpha = 5^0$.

Figure 10.- Concluded.



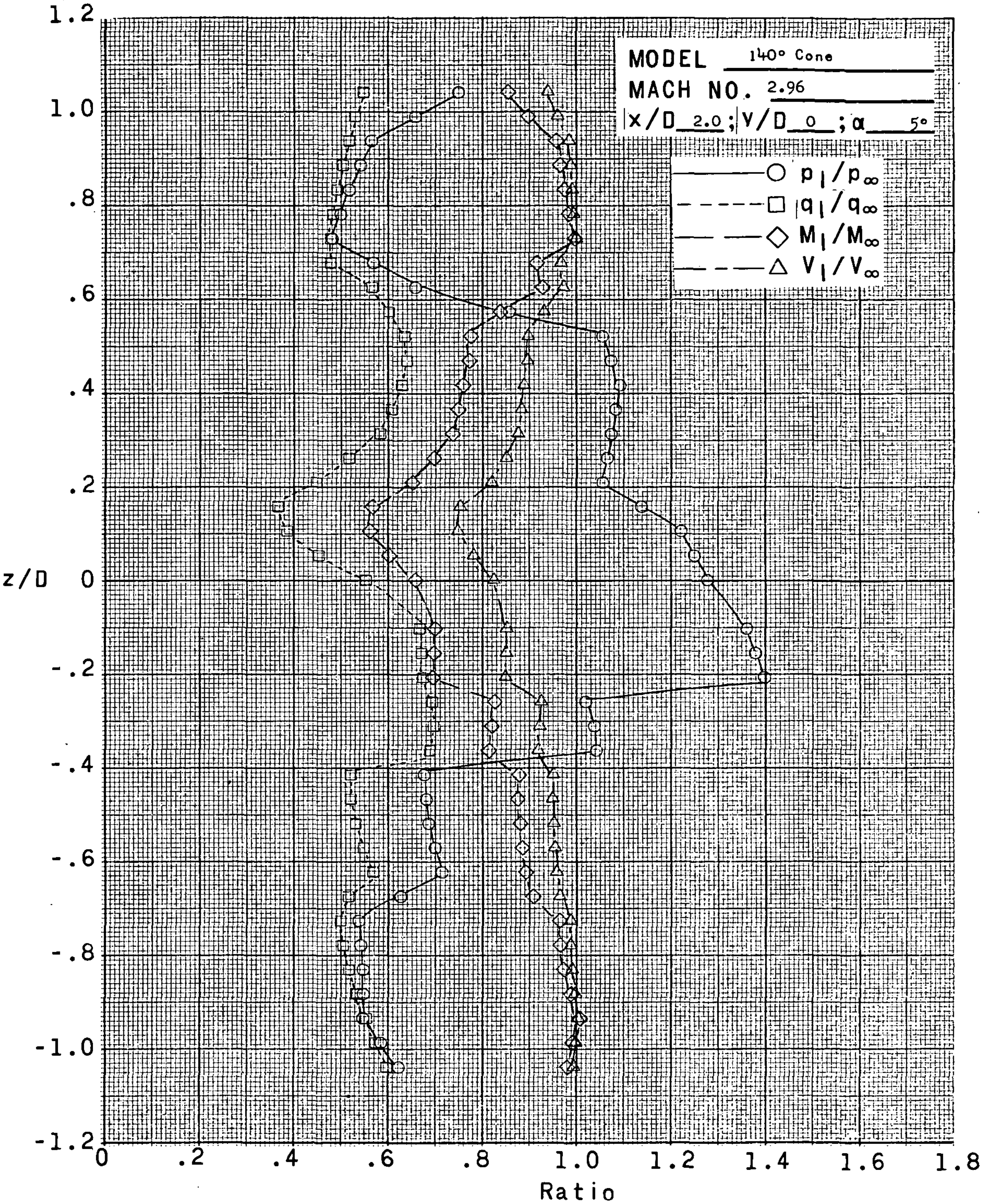
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 11.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D at center of wake of 140^0-included-angle cone at Mach number of 2.96 and Reynolds number of 5.42×10^6 per meter (1.65×10^6 per foot).



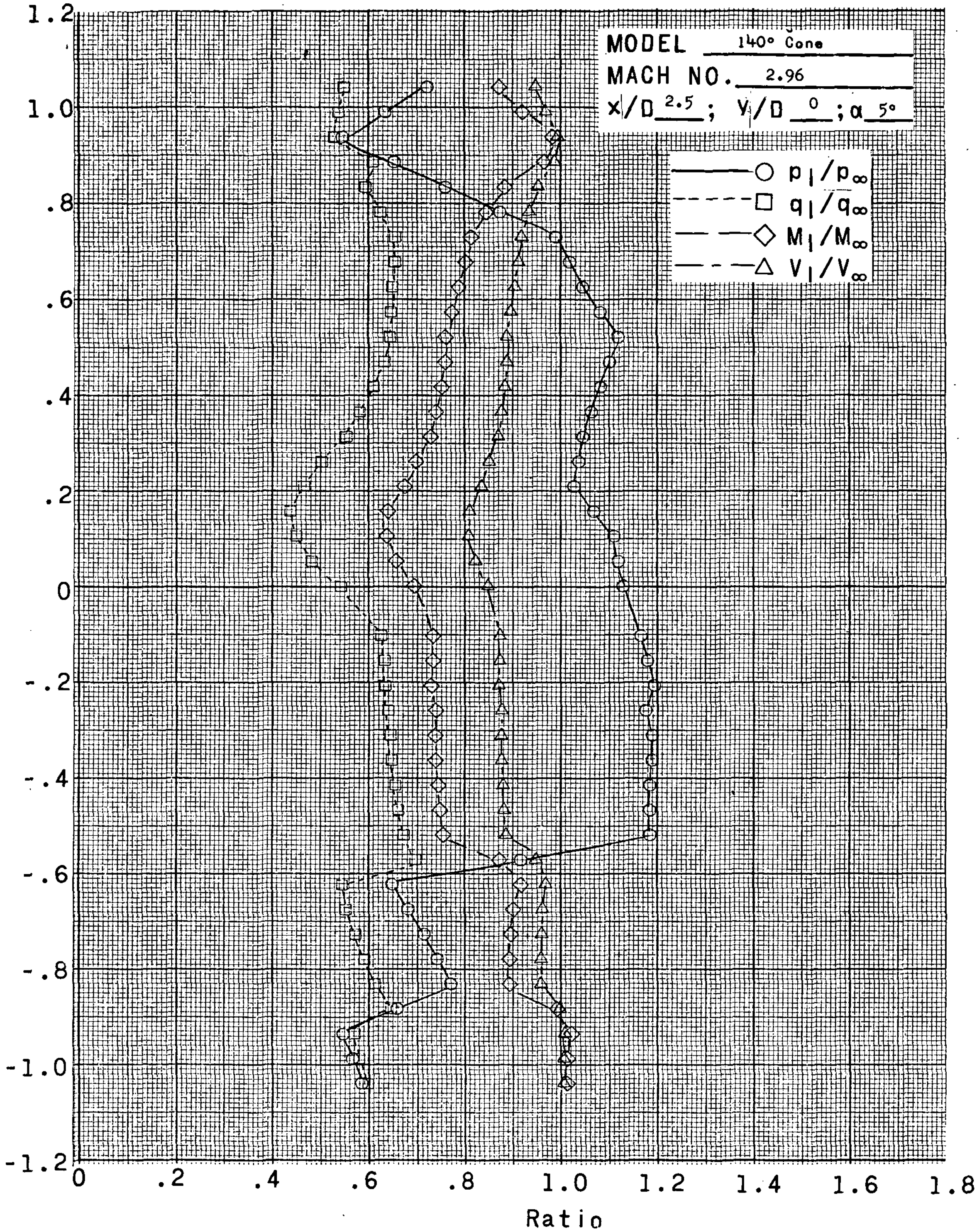
(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 5^0$.

Figure 11.- Continued.



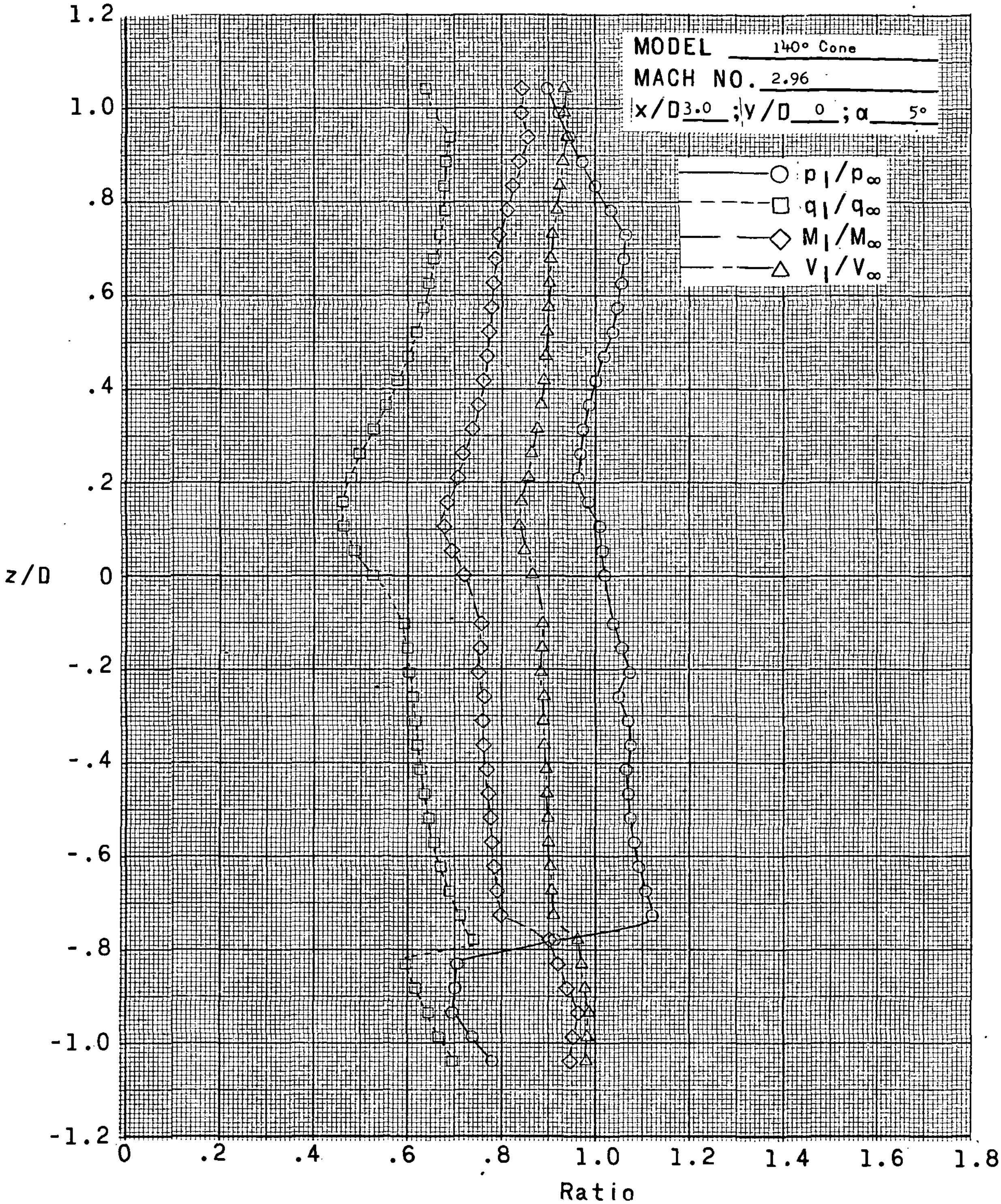
(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 11.- Continued.



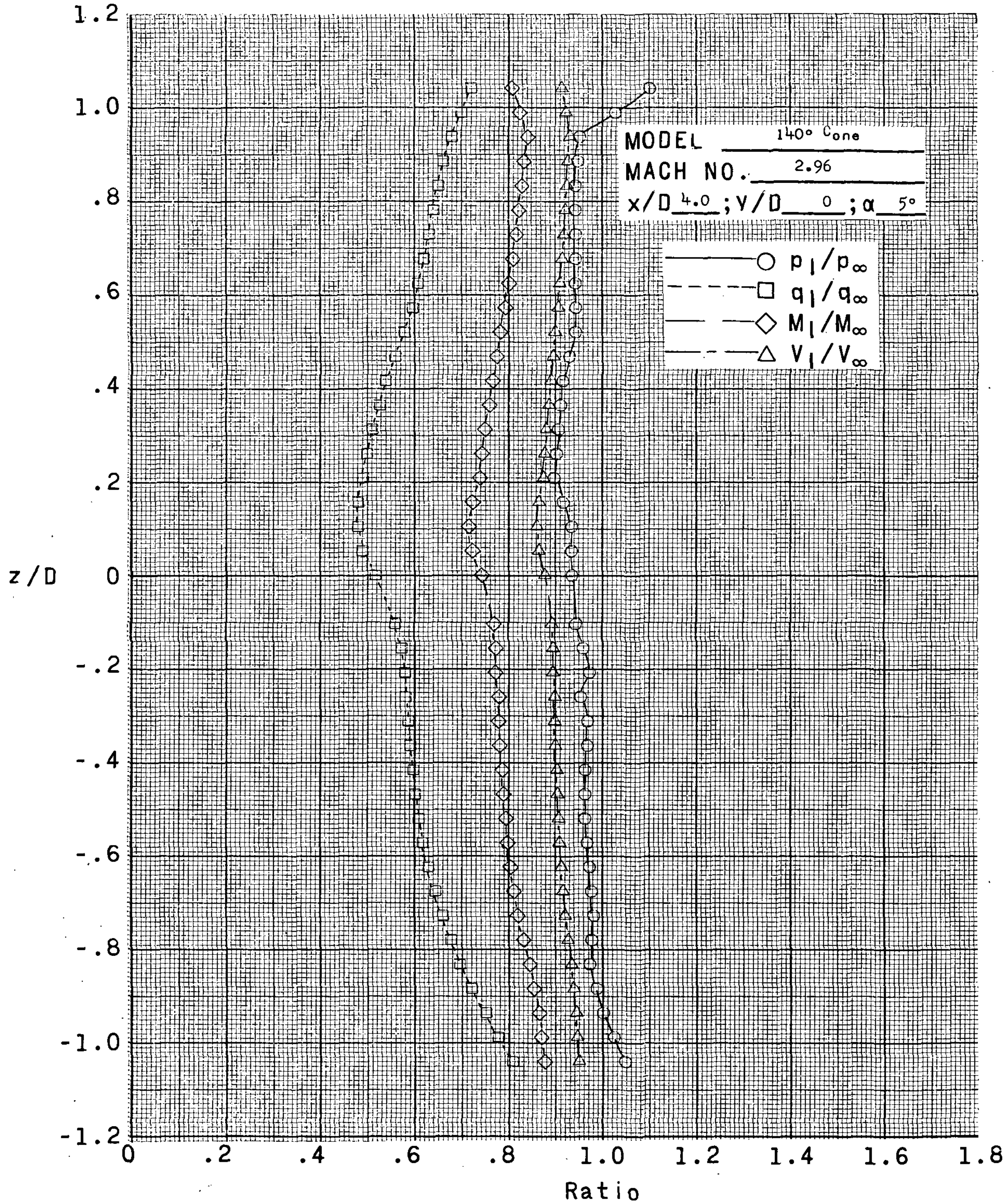
(d) $x/D = 2.5$; $y/D = 0$; $\alpha = 5^0$.

Figure 11.- Continued.



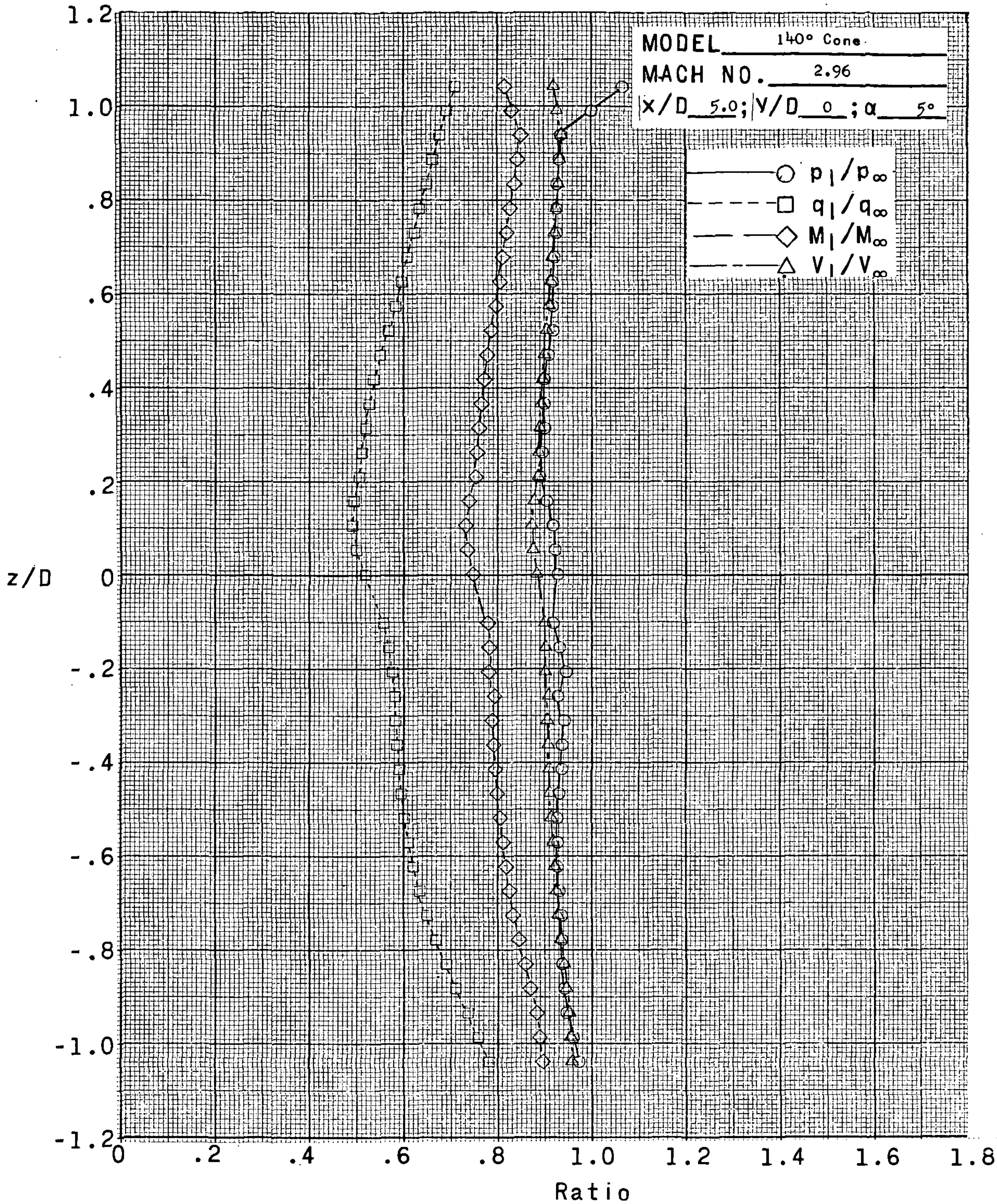
(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 11.- Continued.



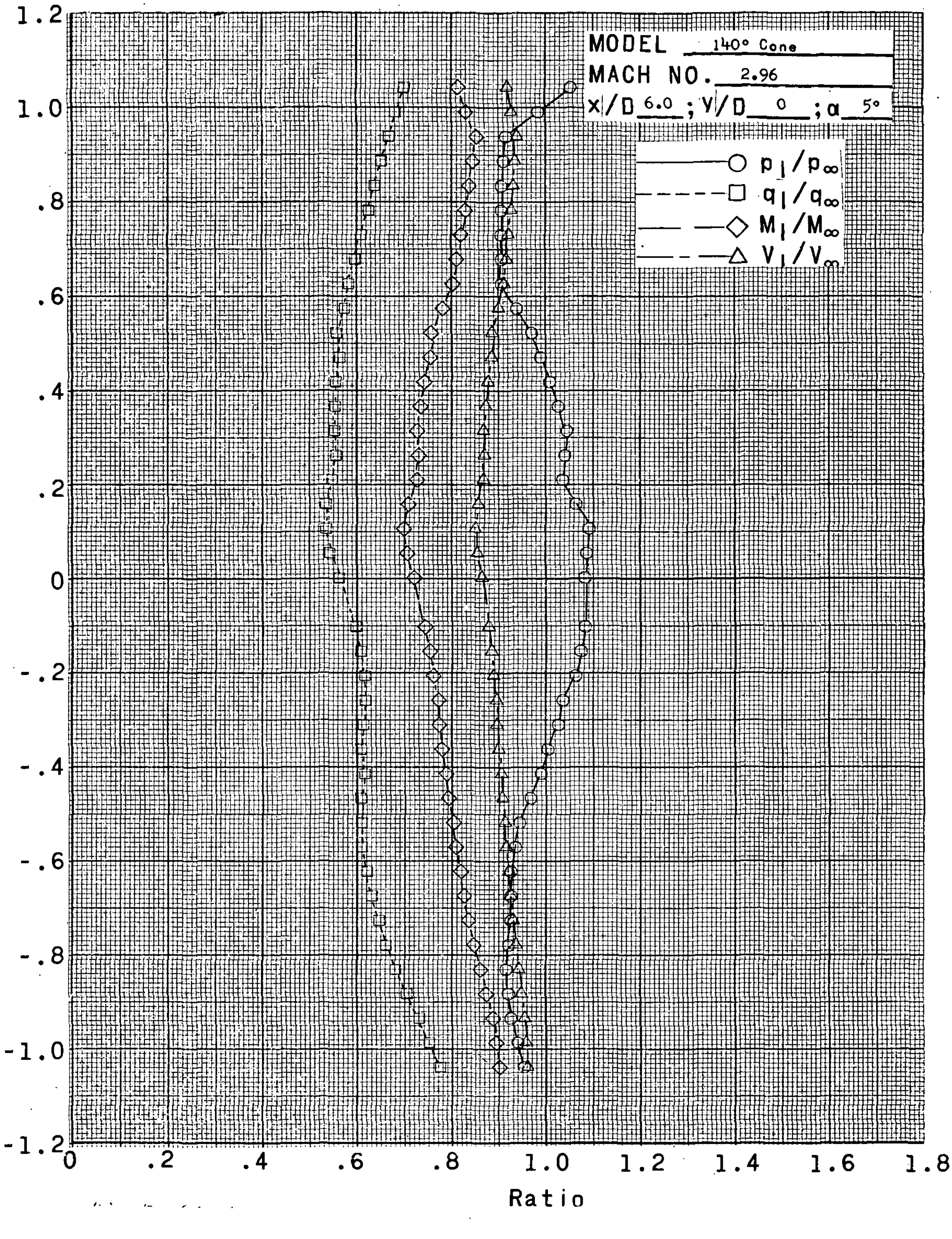
(f) x/D = 4.0; y/D = 0; α = 5°.

Figure 11.- Continued.



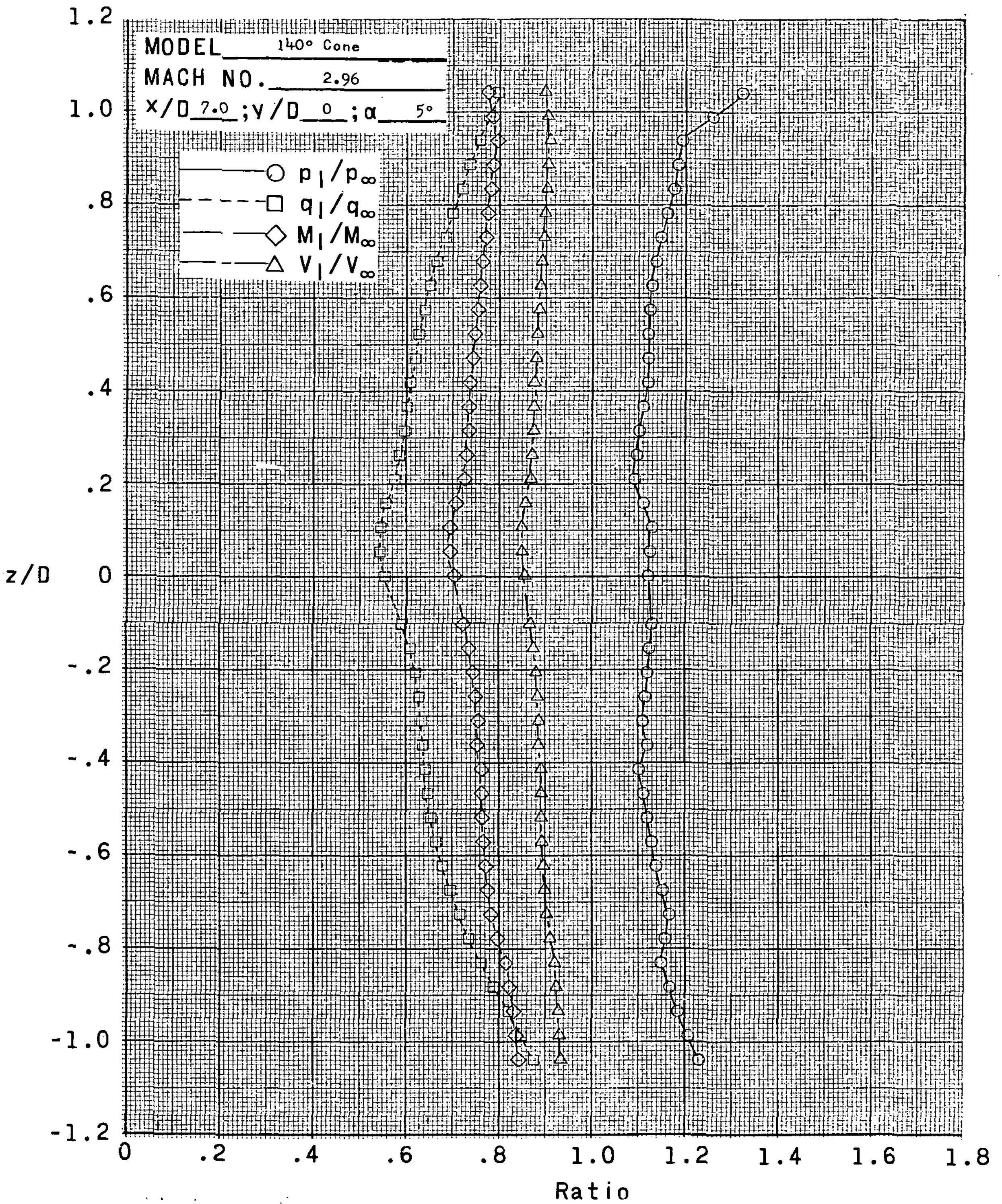
(g) x/D = 5.0; y/D = 0; α = 5°.

Figure 11.- Continued.



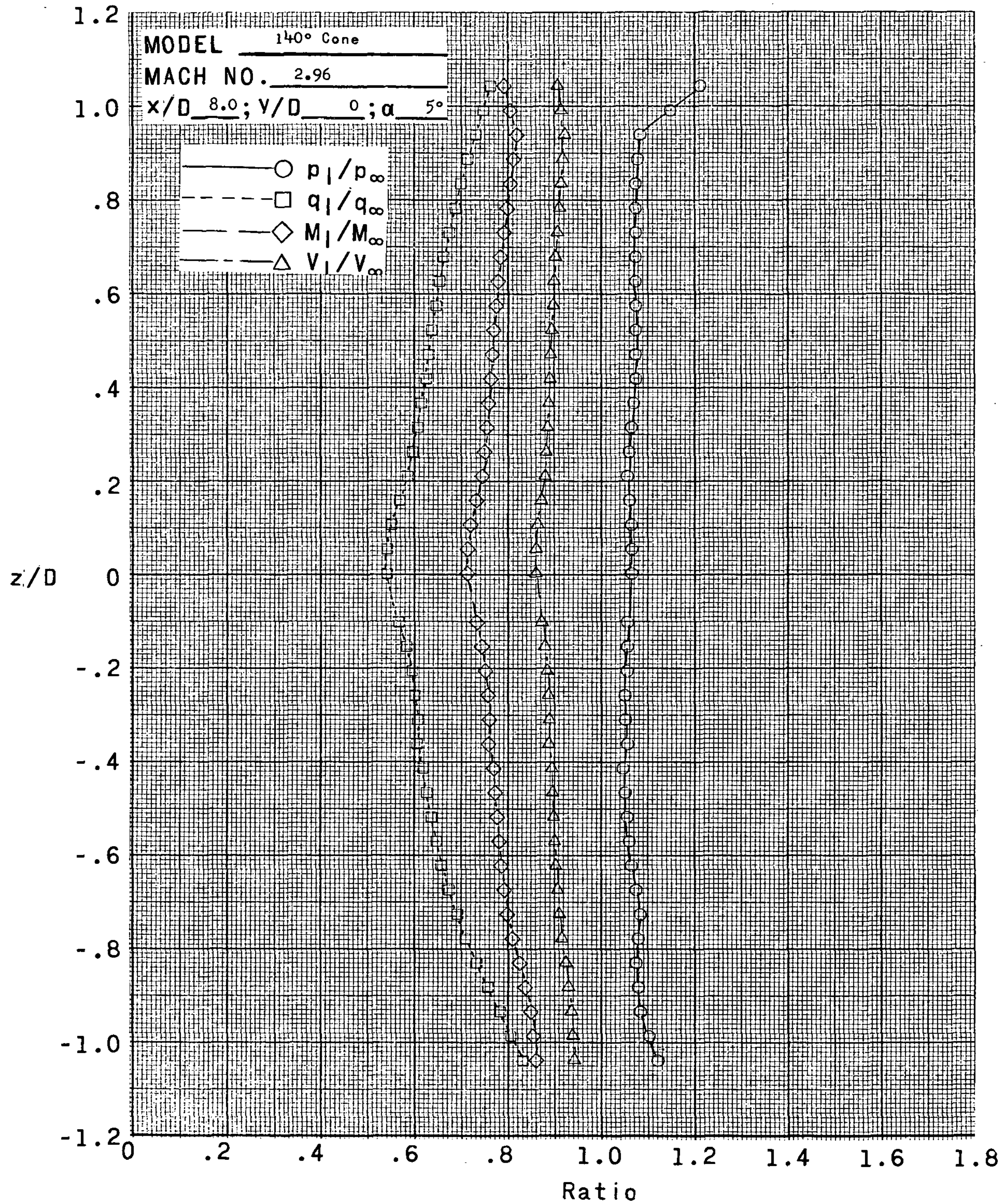
(h) x/D = 6.0; y/D = 0; α = 5°.

Figure 11.- Continued.



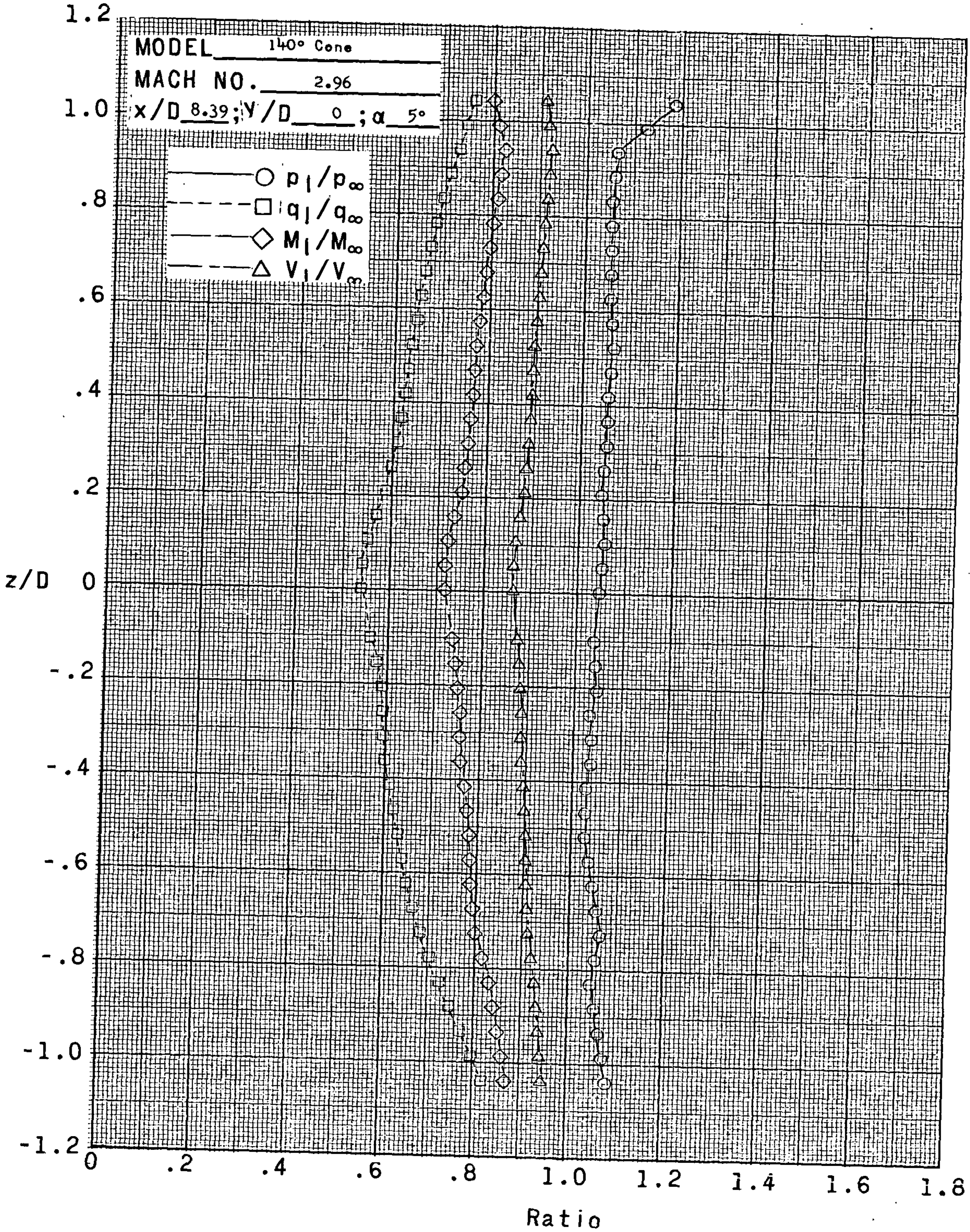
(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 11.- Continued.



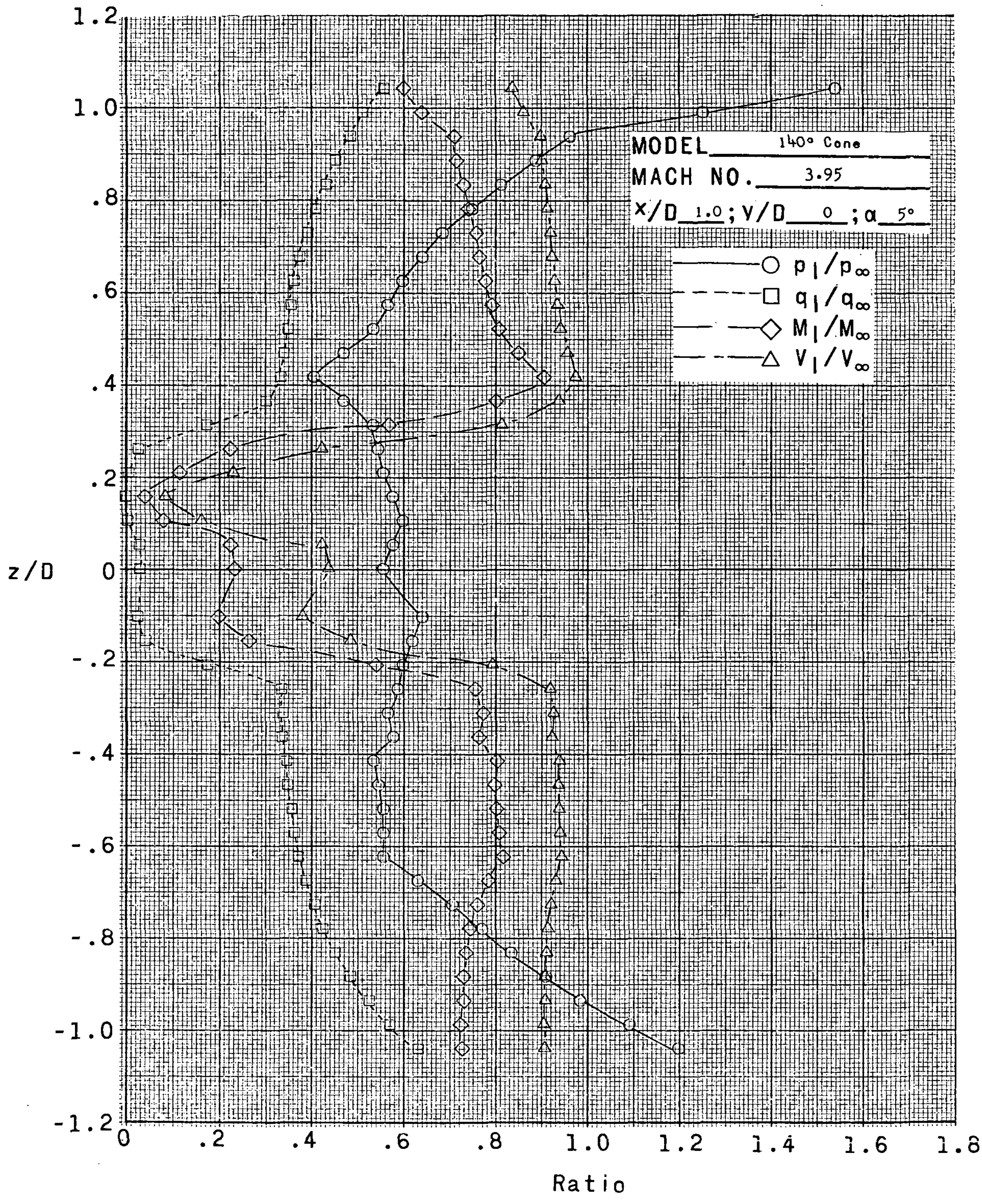
(j) $x/D = 8.0$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 11.- Continued.



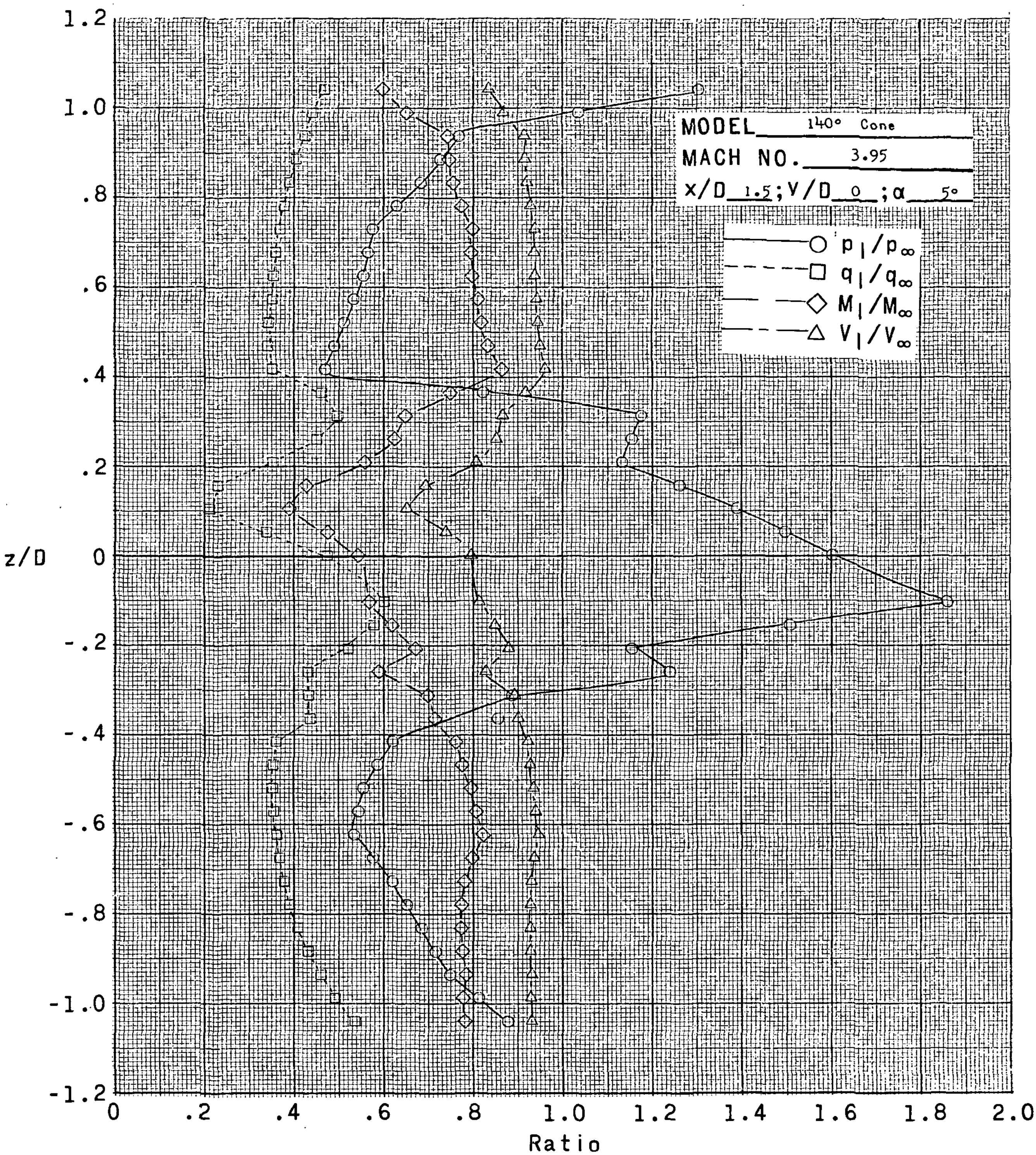
(k) $x/D = 8.39$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 11.- Concluded.



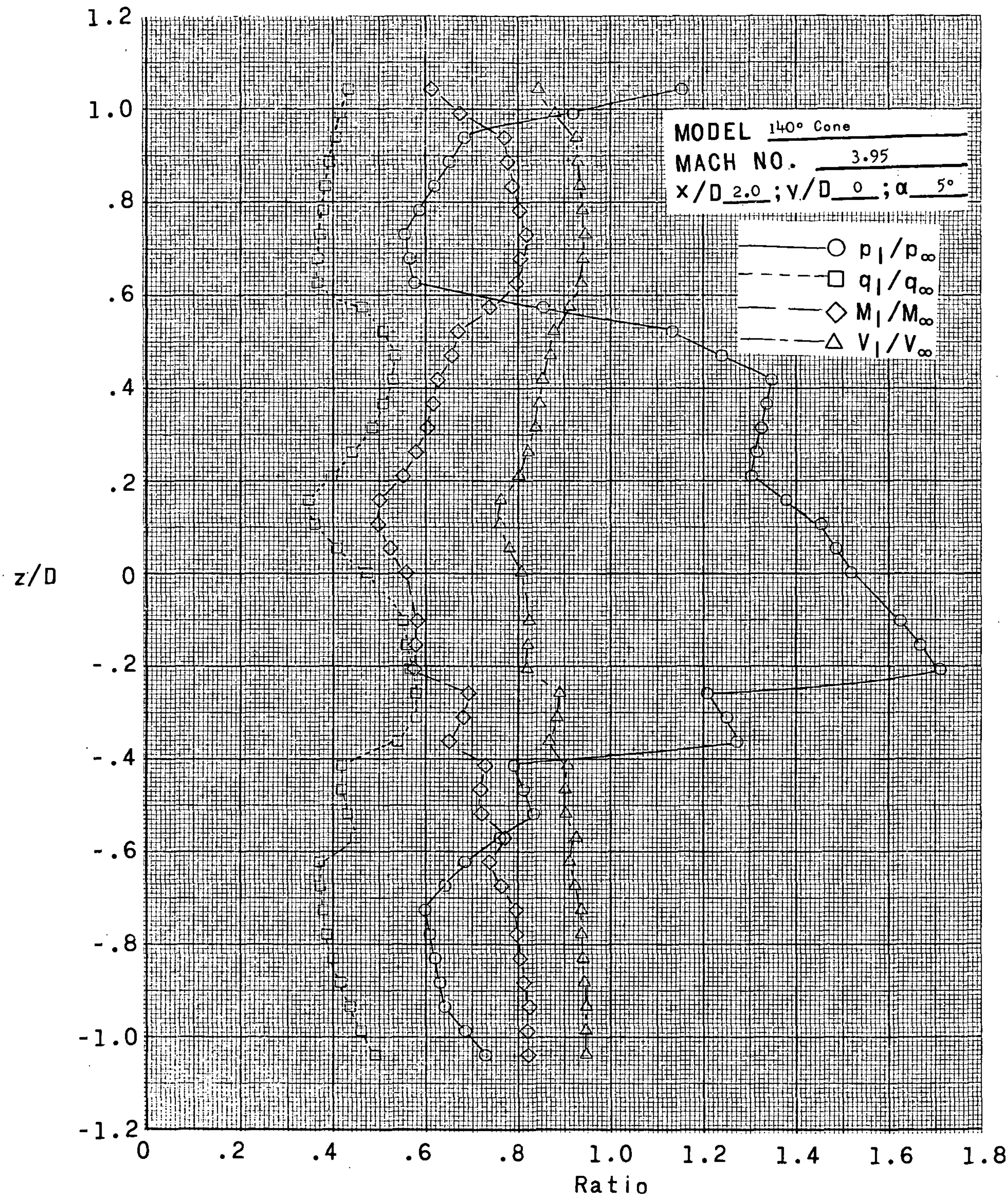
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 12.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D at center of wake of 140^0-included-angle cone at Mach number of 3.95 and Reynolds number of 5.42×10^6 per meter $(1.65 \times 10^6$ per foot).



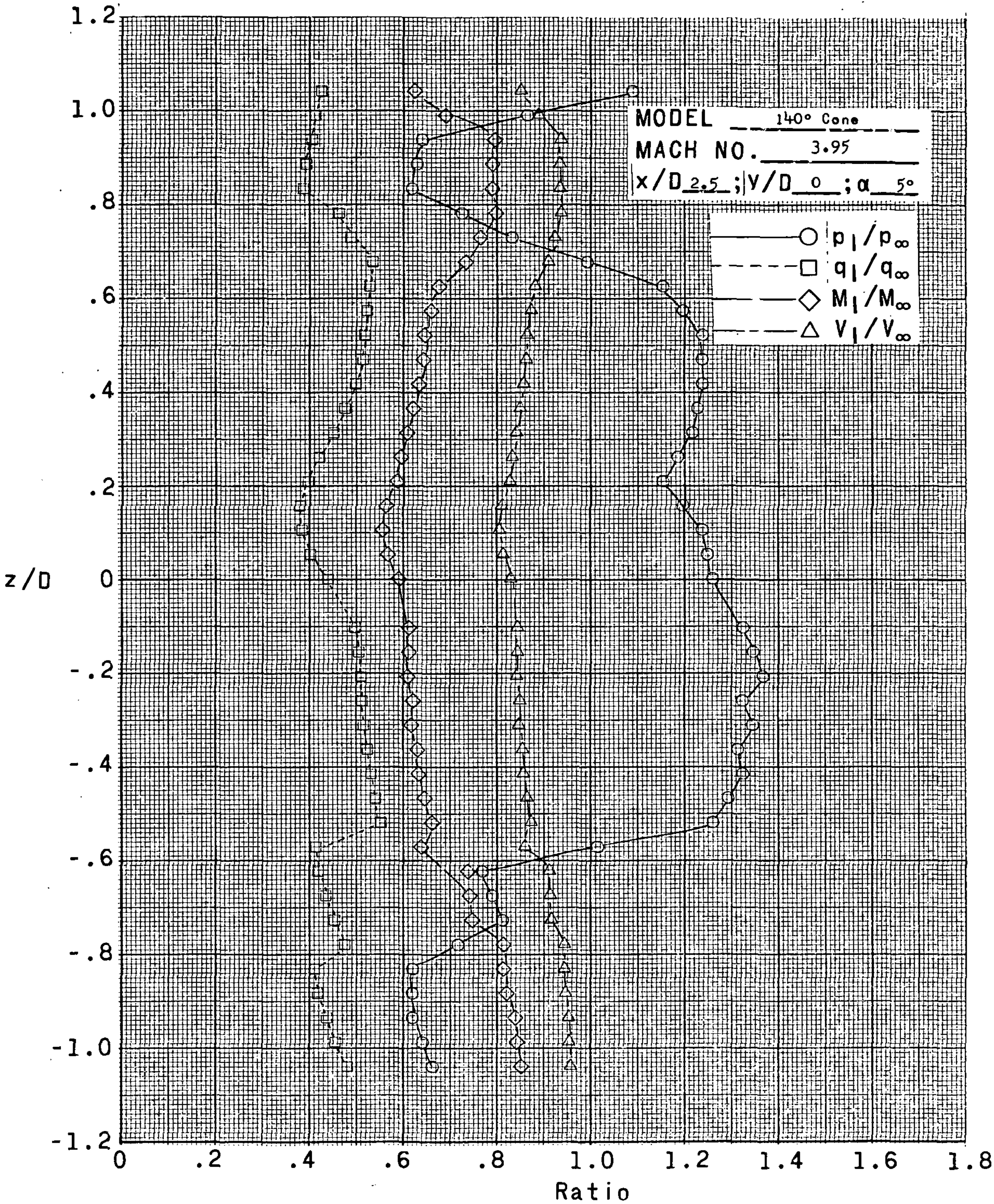
(b) x/D = 1.5; y/D = 0; α = 5°.

Figure 12.- Continued.



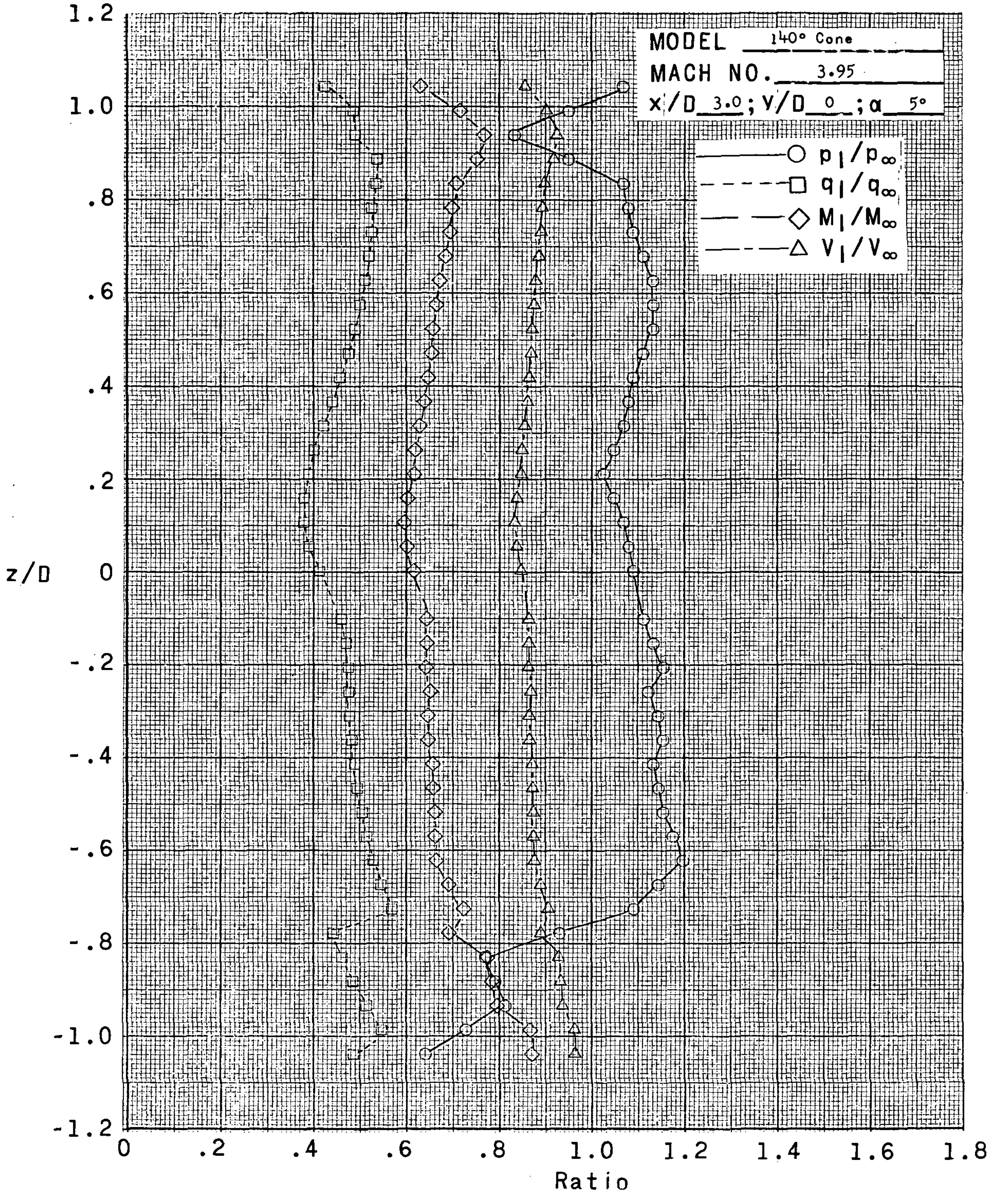
(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 5^{0}$.

Figure 12.- Continued.



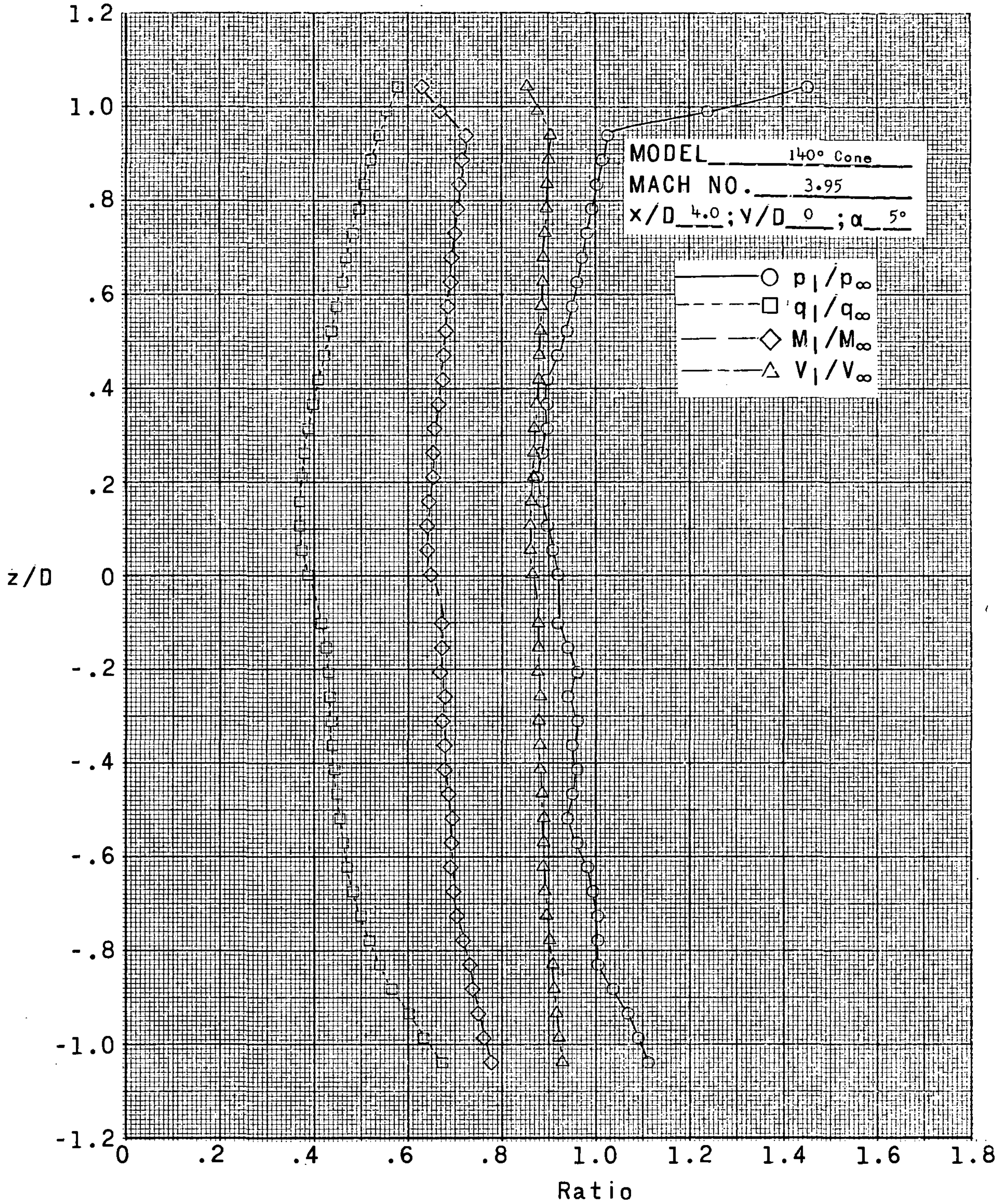
(d) $x/D = 2.5$; $y/D = 0$; $\alpha = 5^{0}$.

Figure 12.- Continued.



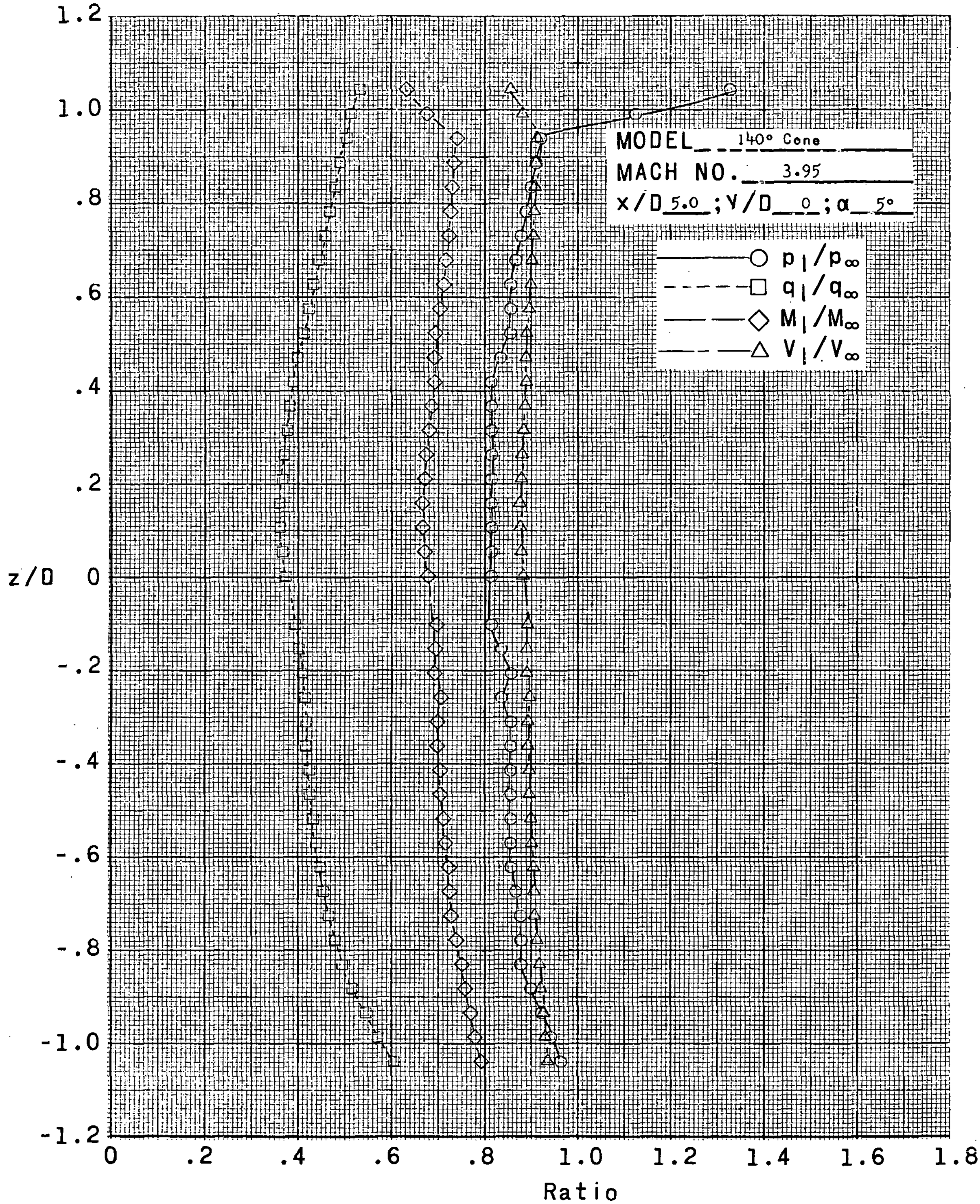
(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 12.- Continued.



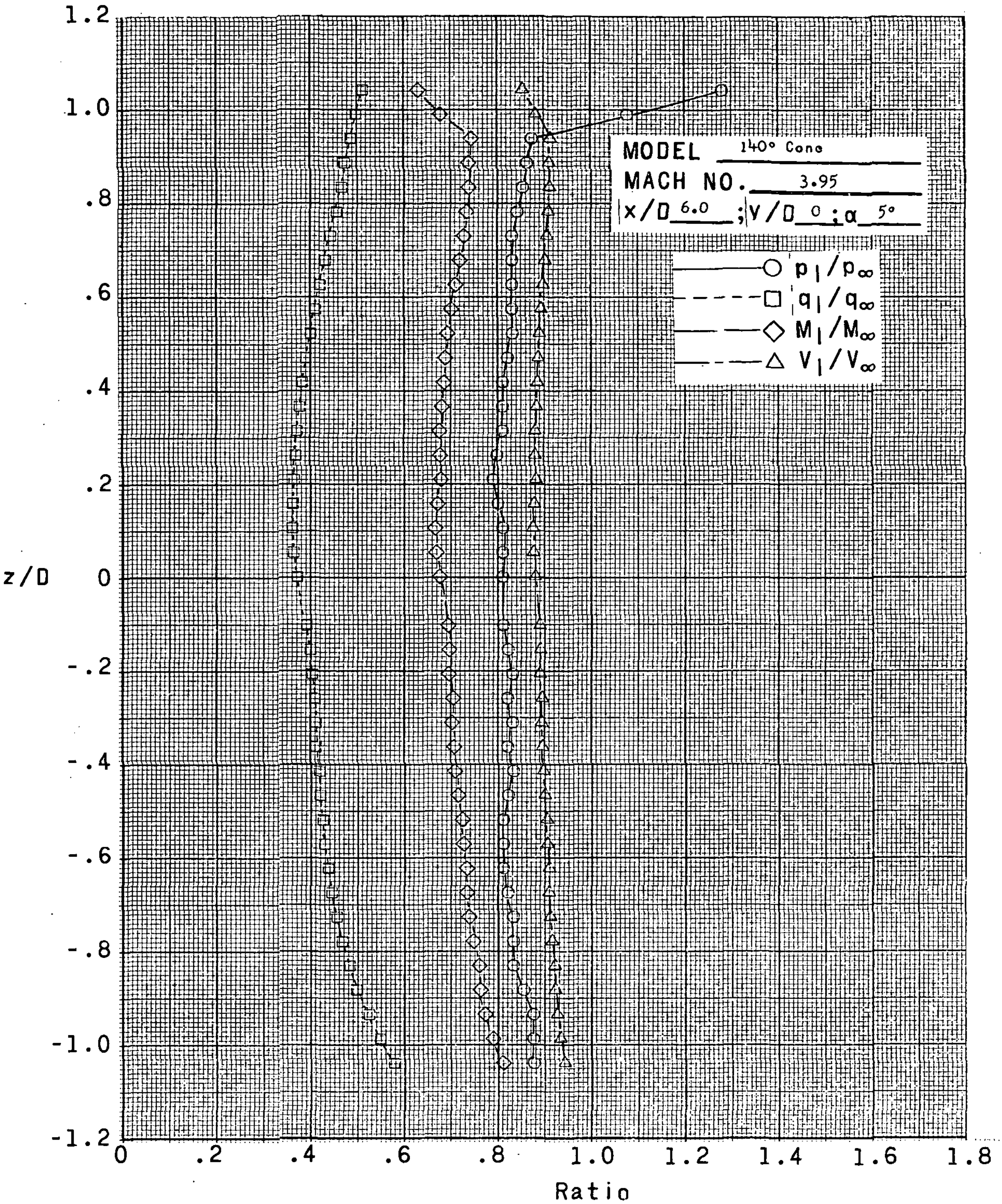
(f) x/D = 4.0; y/D = 0; α = 5°.

Figure 12.- Continued.



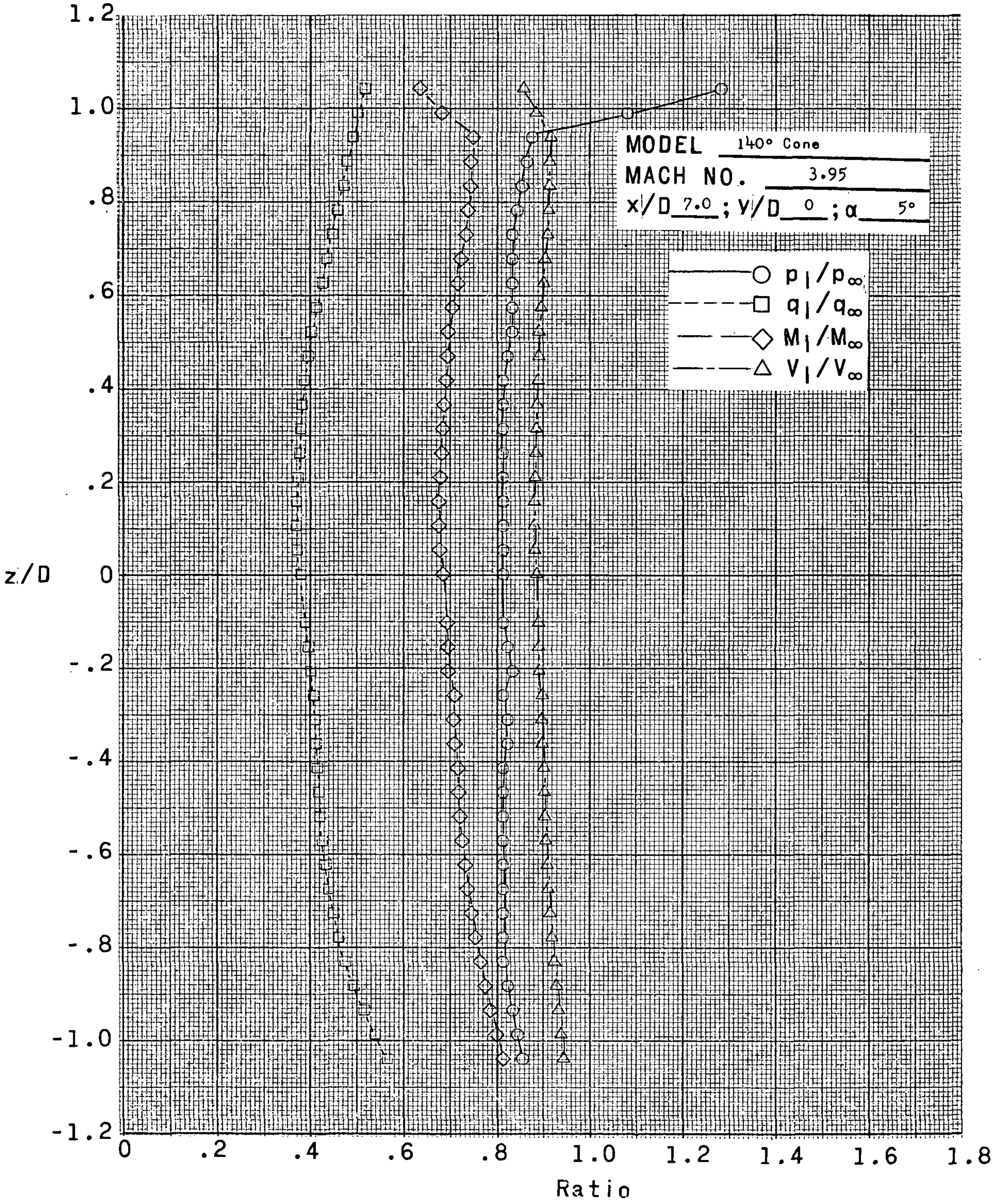
(g) $x/D = 5.0$; $y/D = 0$; $\alpha = 5^{0}$.

Figure 12.- Continued.



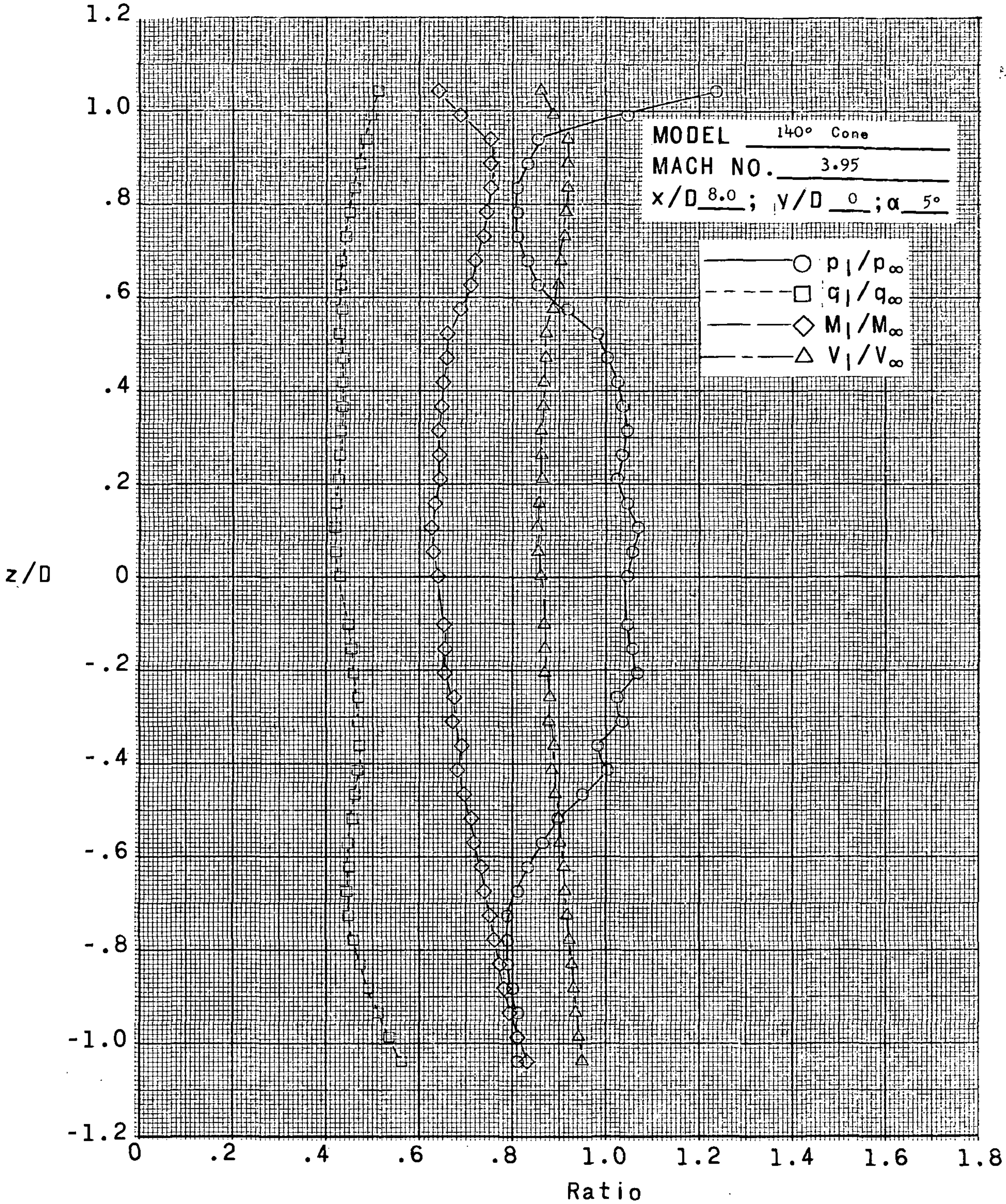
(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 5^{0}$.

Figure 12.- Continued.



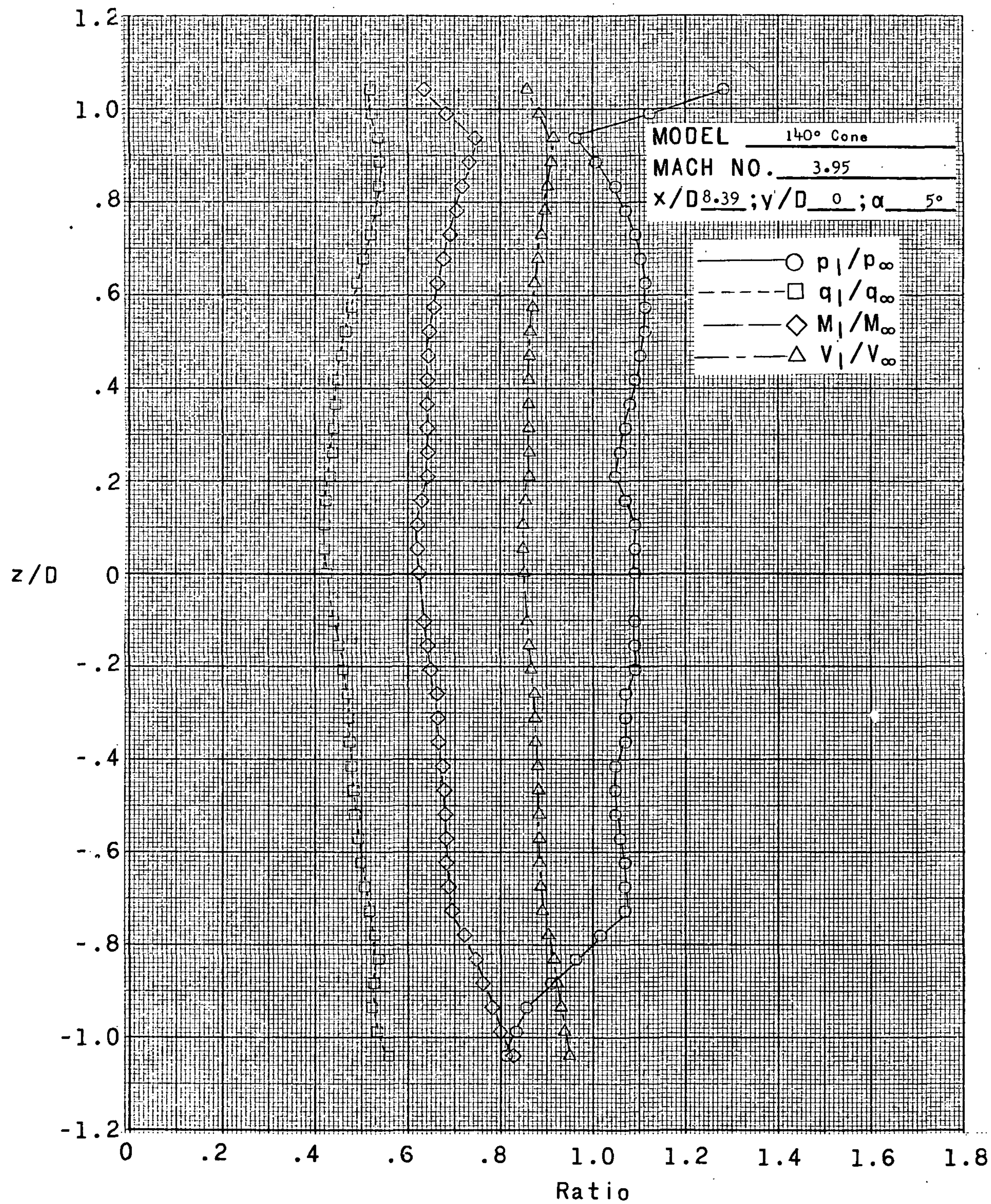
(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 12.- Continued.



(j) $x/D = 8.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 12.- Continued.



(k) x/D = 8.39; y/D = 0; α = 5°.

Figure 12.- Concluded.

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